

1 **Hydrological soil behavior in areas with semi-arid vegetation (Beni Chougrane**  
2 **Mountains, Algeria)**

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19 **Running title:** Hydrological soil behavior in Beni Chougrane

20

21 **Abstract**

22 In northern Algeria, the physical degradation of land by water erosion is one of the most serious  
23 forms of degradation. As is well known, vegetation plays an important role against water  
24 erosion. In the mentioned area the potential vegetation called maquis is currently characterized  
25 by an advanced stated of degradation, often ranging between sparse cover and bare soil. In the  
26 Oued Fergoug watershed belonging to the Beni Chougrane Mountains (NW of Algeria), a trial

27 was carried out with a mini rainfall simulator designed by ORSTOM to evaluate the runoff rate  
28 and the sediment load at experimental plot scale and in a situation of bare soil. The experimental  
29 layout took into account two different surface slopes, three different rainfall intensities, and  
30 three levels of initial soil water content. The highest runoff values observed exceeded 0.50 mm  
31  $\text{min}^{-1}$  and the maximum sediment load yield was 94.2  $\text{g L}^{-1}$  per square meter. Summarizing, the  
32 intensity of rain is the main factor for runoff generation, independently of the slope and the  
33 initial soil water content values. Since vegetation cover is a crucial component in maintaining  
34 stable slopes and limiting soil losses, the most effective practice to protect bare soil against  
35 erosion is to provide a protective ground plant cover in this area.

36

37 **Key words:** ORSTOM rainfall simulator; Algeria; slope; rainfall intensity; initial soil water  
38 content

39

## 40 **Introduction**

41 Land degradation is recognized as the main outcome of desertification (Puigdefabregas et al.  
42 2009). In particular, the mentioned authors highlight the importance of hydrological ratios,  
43 energy ratios, biomass, productivity and spatial patterns between the ecosystem attributes  
44 associated with land condition. Ecosystem degradation notably entails the incapacity to  
45 preserve, use and recycle local resources such as water, energy and nutrients. Koulouri &  
46 Giourga (2007) consider land abandonment and slope gradient as key factors for soil erosion in  
47 the Mediterranean region. In northern Algeria, the physical degradation of land due to water  
48 erosion is one of the most serious forms of degradation (Souidi et al. 2014).

49 Soil erosion is a two-phase process consisting of the detachment of individual soil particles  
50 from the soil mass and their transport by erosive agents as surface runoff. Runoff refers to the  
51 portion of rainwater that is not lost due to interception, infiltration, evapotranspiration or surface

52 storage, and flows over the land surface to a stream channel. Interrill erosion is induced by a  
53 moving sheet of water over the soil surface. The rate at which water passes into the soil is  
54 known as the infiltration rate and this exerts a major control over the generation of surface  
55 runoff (Rickson & Morgan 1995). In the case of bare soil, rainfall is distributed between  
56 infiltration and runoff, as direct evaporation is not taken into account.

57 Vegetation plays an important role against water erosion in two main ways: by preventing loss  
58 of substrate and by favoring sedimentation (Rey et al. 2004). Gray & Sotir (1996) point out the  
59 beneficial effects of herbaceous vegetation in preventing rainfall erosion. Martínez Raya et al.  
60 (2005) observed that plant cover with arbustive species reduced soil loss and runoff about 90%  
61 compared to bare soil. The risk of slope failures and erosion is **heightened** when the vegetation  
62 cover is removed (Rickson & Morgan 1995). Coppin & Richards (1990) distinguish between  
63 (i) bioengineering, the use of vegetation for slope stabilization and erosion control, and (ii)  
64 biotechnical engineering, techniques where vegetation is combined with inert structures, in  
65 which the engineering role of the vegetation is accentuated.

66 Among the various factors for controlling soil erosion related with the vegetation cover, the  
67 growth of the roots and their persistence play a significant role in semi-arid areas (Himmelbauer  
68 et al. 2013). Coppin & Richards (1990) underline the engineering role of vegetation and  
69 particularize water uptake by roots, reinforcement of soil by roots, and anchoring and  
70 buttressing by taproots.

71 Rainfall simulation, used for many years, is still one of the most used and most successful tools  
72 to study soil erosion by water (Martínez-Murillo et al. 2013).

73 One application of a rainfall simulator in Algeria concluded that soil tillage on marls in a semi-  
74 arid condition could be an excellent tool to diminish runoff and control soil erosion (Prinz et al.  
75 1994).

76 Therefore, the main objective of this paper is to characterize the runoff and sediment load yield  
77 on bare soils of a region located in Beni Chougrane Mountains (one of the most erodible  
78 countries in the world) by means of small-scale rainfall simulation. This information would be  
79 useful to assess future restoration projects using vegetation for the area understudied.

## 80 **Material and methods**

81 The experiment was carried out in the Oued Fergoug watershed (122 km<sup>2</sup>) in the Beni  
82 Chougrane Mountains (NW of Algeria). This area forms part of the great Oran-Chott Chergui  
83 watershed belonging to the Oran Tell, which in turn covers an area of 2860 km<sup>2</sup>. The UTM  
84 coordinates of the mouth of Oued Fergoug are: 31S 232440 mE 39394850 mN.

85 Average monthly temperatures (series from 1993 to 2012) show two different seasons: a cold  
86 season (from November to April) with an absolute minimum of 3°C recorded in January, and a  
87 hot season (from May to October). The absolute maximum temperature in this period was 41°C  
88 (August). Average annual rainfall at three stations located around the study area- Mascara, Ain  
89 Farès and Bouhanifia- were 402, 428 and 281 mm respectively. The maximum and minimum  
90 mean monthly rainfalls recorded between 1980 and 2000 were 62.8 mm (December) and 2.4  
91 mm (August). The rainfall distribution throughout the year is highly variable and it is  
92 concentrated during the cold season (Bouchetata & Bouchetata 2006). It should be noted that  
93 the rainiest season is between October and December and the wettest months are December and  
94 January. Rainfall intensity is also very variable and heavy rainfalls occur from late November  
95 to February, but secondary maximums are obtained in September or October and in April or  
96 May. Extreme values of rainfall intensity reach 900 mm h<sup>-1</sup> (December or January) for periods  
97 of 5 to 10 minutes.

98 The Beni Chougrane Mountains are characterized by an extremely abrupt relief (peaks from  
99 300 to 800 m) and large hills alternate with high plateaus and deep valleys. Slopes are very

100 variable. Nearly 20% of the soil surface has a slope of more than 50%, and 26% of the soil  
101 surface has a slope of between 25% and 12.5%.

102 The soils of the experimental area are developed on marl and sandstone and colluviums.  
103 Climatic aridity and soil erosion prevent soil development and poorly developed soils are  
104 common. Very often the soils retain characteristics of the bedrock. Inceptisols and entisols are  
105 the main soil orders in the region. Analytical data of the topsoil in the experimental area show  
106 60.2% clay, 22.1% fine silt, 7.5% coarse silt, 5.5% fine sand, 3.1% coarse sand, and 1.7%  
107 organic matter. Calcium carbonate is present in large proportions.

108 In accordance with the semi-arid Mediterranean bioclimate of the area, the maximum  
109 expression of the potential vegetation in the area is a particular maquis dominated by *Callitris*  
110 *articulata* (Vahl.) Link. (called *thuya de Barbarie* in French). This is a scrubland or shrubland  
111 of greater or lesser density depending on the conditions, with the presence of a diverse  
112 assortment of plant species sharing the common physical characteristic of dominance by shrubs  
113 (*Olea europaea* L., *Rosmarinus officinalis* L., *Calycotome spinosa* (L.) Lamk., *Artemisia*  
114 *herba-alba* Asso, etc.). Evergreen oak (*Quercus ilex* L.) and pine (*Pinus halepensis* Mill.)  
115 forests can appear in some specific sites forming sparse stands (Zahira et al. 2009; Haddouche  
116 et al. 2011; Tayeb & Kheloufi 2014).

117 In most of the area, due to several causes (erosion, fire and overgrazing), the vegetation is  
118 characterized by an advanced state of degradation. At best a sparse vegetation cover is observed  
119 and surfaces with bare soil in higher areas are common. In particular, we can see the rapid  
120 progress of land degradation by comparing the map provided by Benchetrit (1966) showing the  
121 situation of the vegetation of the Beni Chougrane area in 1953 (the author used a legend with 8  
122 categories: forest, degraded forest, maquis, scrublike matorral or garrigue, vineyards, European  
123 crops, Algerian crops, and bare soil) with the information obtained by remote sensing (Zahira  
124 et al. 2009; Haddouche et al. 2011; Tayeb & Kheloufi 2014). Nowadays Beni Chougrane is

125 included in the southern edge of the olive-growing area (Zdruli 2014), and is considered a good  
126 grazing area (FAO 2005).

127 A mini rainfall simulator designed by ORSTOM (Asseline 1981; Casenave 1982) was used in  
128 this experiment. A total of 18 rainfall simulations were carried out on regular square plots of 1  
129 m<sup>2</sup>. An adjustable lever system made it possible to vary the oscillation angle of the nozzle and  
130 the wet the surface of the soil. Consequently, the rainfall intensity in the plot ranged from 30 to  
131 150 mm h<sup>-1</sup>. The nozzle was supplied with water at constant pressure. It produced a flat stream  
132 of water in a fan shape.

133 An experimental area located on the same parent material, with similar soils and covers (bare  
134 soil), was selected on two different surface slopes. Nine plots were established in each area,  
135 distributed in a 3 by 3 matrix of plots, with the three different rainfall intensities, and three  
136 levels of initial soil water content (Table 1). Water runoff and sediment load were measured  
137 with a test tube at 1 minute intervals. Each rainfall simulation experiment was carried out until  
138 10 consecutive sediment samples were collected. The length of the simulations ranged between  
139 15 (moister plots) and 108 (dry plots) minutes.

140 The statistical analysis of data was first conducted using a set of exploratory techniques to  
141 investigate the relationship between time, runoffs and sediment loads of various groups of data  
142 according to the combinations of the three factors considered (Table 1). Row data and  
143 transformations of the data by logarithm function were investigated. Regression models were  
144 performed with the sediment load as the response variable to explain or predict, the runoff as a  
145 continuous predictor and the three factors as categorical predictors, jointly with their  
146 interactions. In order to establish comparisons between the runoffs when the stabilization took  
147 place, data were analyzed grouped into subsets according to the factors described above.  
148 General linear models (GLM) and variance tests (ANOVA) were used to evaluate the influence  
149 of the three factors (surface slope, initial soil water content and rain intensity) and their

150 interaction on the final stabilized runoff. In order to complete this data analysis, and taking into  
151 account the variability of the data and the small sample sizes, a nonparametric alternative to a  
152 one-way ANOVA, the Kruskal-Wallis test, was also used to rank data values. The separation  
153 of means was evaluated using the Tukey-Kramer procedure and Games-Howell pairwise  
154 comparisons. Data were analyzed using Minitab software (2007). The probability level of  
155 significance was set at 0.05.

156

## 157 **Results and discussion**

158 Fig. 1 shows the results of the evolution of the runoff ( $\text{mm min}^{-1}$ ) in the course of the experiment  
159 for the 18 simulations carried out. In the initial dry soil condition, water infiltrated across the  
160 soil surface and no runoff was observed independently of slope. Then the runoff rate stabilized  
161 (a maximum runoff rate was reached) over time. However, runoff acquired rising importance  
162 from the beginning of the simulation under more intense rainfall (RI-50 and RI-80). Runoff in  
163 moister soils (FC and SAT) started from the first moments of the simulation and increased until  
164 a stable rate was achieved. This maximum runoff rate was not assumed conclusively in the most  
165 favorable set of conditions to erosion (RI-50 or RI-80 and 25% slope), but we can consider the  
166 runoff values to be very near to stability.

167 Fig. 2 depicts the relationships between stable runoff rate ( $\text{mm h}^{-1}$ ) and sediment load yield ( $\text{g}$   
168  $\text{L}^{-1}$ ) per square meter. This figure shows that when the soil is dry (DS) the sediment load  
169 concentration does not increase when maximum runoff increases; our interpretation of this is  
170 that the soil mass susceptible to erosion tends to be exhausted during the experiment. This does  
171 not mean that the total (per square meter) quantity of sediment exported was the same over both  
172 slopes (12.5% and 25%). A similar behavior can be observed in the case of the rainfall  
173 simulations with  $\text{RI-30 mm h}^{-1}$ . In this case the largest quantity of exported soil (in terms of  
174 sediment load yield) would correspond to dry soil (DS). In other combinations of factors, the

175 regression model suggests that the maximum concentration of sediment exported was not  
176 reached. When the intensity of rainfall is maximum, the behavior varies according to slope. An  
177 overall view of all the graphs suggests a complex relationship between these variables, possibly  
178 related to the energy balance (Chaplot & Le Bissonnais 2003). The maximum value of sediment  
179 load yield, which reached  $94.2 \text{ g L}^{-1} \text{ m}^{-2}$ , was generated by interrill erosion. The stable  
180 (maximum) runoff values obtained with the rainfall simulator should be considered only as  
181 indicative of soil behavior in actual field conditions, among other reasons due to the large  
182 variety of simulators that can be used (Martínez-Murillo et al. 2013) and the wide variety of  
183 environmental factors that may be involved (Casenave 1982). Consequently, the interpretation  
184 should be considered in relative terms and in relation to the trends suggested by the results.

185 Table 2 shows the maximum runoff values of the 18 treatments arranged in descending order  
186 and significant differences have been stated for medians and means with the two statistical tests  
187 (Kruskal-Wallis and one-way ANOVA tests).

188 In each of the three data sets corresponding to each level of initial soil conditions, for the  
189 stabilized runoff variable, the two-way ANOVA tests performed with the factors slope and rain  
190 intensity revealed that their interaction was significant (the three p-values  $< 0.01$ ). For the three  
191 initial soil conditions, according to the Tukey-Kramer procedure, the higher means of runoff  
192 corresponding to the combinations 25%\_RI-80 and 12.5%\_RI-80 were significantly different,  
193 but no significant differences were detected between the pairs 12.5%\_RI-50 and 25%\_RI-50,  
194 or between 12.5%\_RI-30 and 25%\_RI-30. In turn, for each data set corresponding to the  
195 different levels of rain intensity, the two-way ANOVA tests carried out with the factors slope  
196 and initial soil water content for the runoff variable showed that the interaction of these two  
197 factors was not significant (p-values of 0.599, 0.755 and 0.825 for RI-30, RI-50 and RI-80  
198 respectively). Thus, the two main factors, the slope and the initial soil water content- showed  
199 an additive effect on runoff. Both factors were significant in each of the three rain intensities



200 (all p-values<0.01). According to the Tukey-Kramer procedure, in the case of the lowest rain  
201 intensity no significant difference was detected for the means corresponding to FC and DS,  
202 while for the other two rain intensities no significant differences were detected between the  
203 means of FC and SAT.

204 The results conclusively showed that the rainfall intensity is the main factor for runoff  
205 generation independently of slope value and initial soil water content. Both slope value and  
206 initial soil water content are factors that are uncontrollable by man, but their geographical  
207 distributions are usually known on different scales. The maximum concentration of sediment  
208 load yield tends to decrease with time over shallowly sloping surfaces and when rainfall  
209 intensity is low. In other cases the sediment load yield can increase with time. This suggests  
210 that it is necessary to protect the soil surface under any conditions of slope and initial moisture  
211 level in areas with more intense rainfall ( $> 80 \text{ mm h}^{-1}$ ). The most effective practice for  
212 protecting the soil against erosion is to implement an adequate vegetal cover, because  
213 vegetation is a critical component in maintaining stable slopes and thus limiting erosion.

214 The importance of the soil surface protective (vegetation) cover is well known. Subsequently,  
215 more field research and acquired knowledge would be necessary to design a detailed project for  
216 the bare soil areas in the Beni Chougrane Mountains favoring long-term restoration of  
217 spontaneous vegetation. The different factors involved in this land degradation and the present  
218 success of some bioengineering techniques to obtain ground cover vegetation should be taken  
219 into account in this context. Moreover, rainfall simulations would be an adequate technique to  
220 evaluate the abovementioned restoration work.

221

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## 276 **FIGURES AND TABLES**

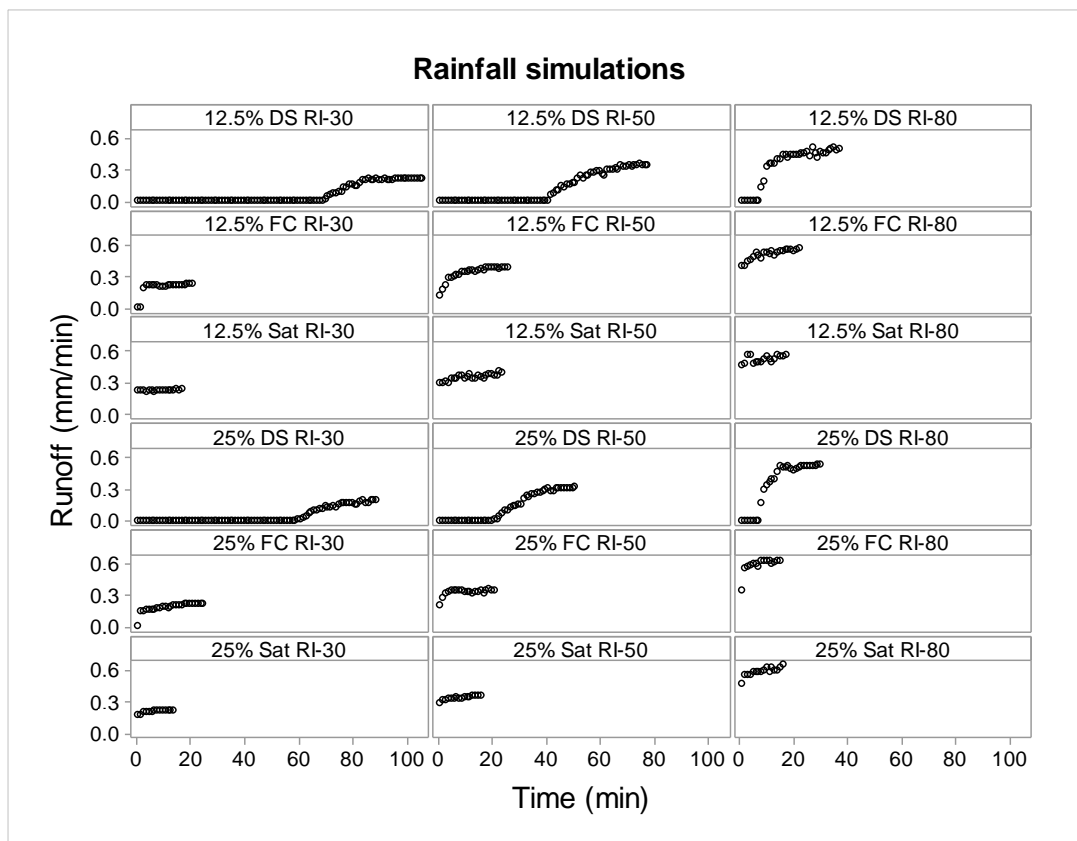
277 **Figure 1.** Runoff values obtained from the 18 rainfall simulations ( $\text{mm min}^{-1}$ ). Slopes (%): 12.5  
278 and 25; Initial soil water content: DS = dry soil, FC = near field capacity, Sat = near soil  
279 saturation. Rainfall intensity: RI-30,  $30 \text{ mm h}^{-1}$ ; RI-50,  $50 \text{ mm h}^{-1}$ , and RI-80,  $80 \text{ mm h}^{-1}$ .

280 **Figure 2.** Chart showing the relationship between sediment load ( $\text{g L}^{-1}$ ) and maximum runoff  
281 rate ( $\text{mm h}^{-1}$ ). Slopes (%): 12.5 and 25; Initial soil water content: DS = dry soil, FC = near field  
282 capacity, Sat = near soil saturation. Rainfall intensity: RI-30,  $30 \text{ mm h}^{-1}$ ; RI-50,  $50 \text{ mm h}^{-1}$ ; and  
283 RI-80,  $80 \text{ mm h}^{-1}$ .

284

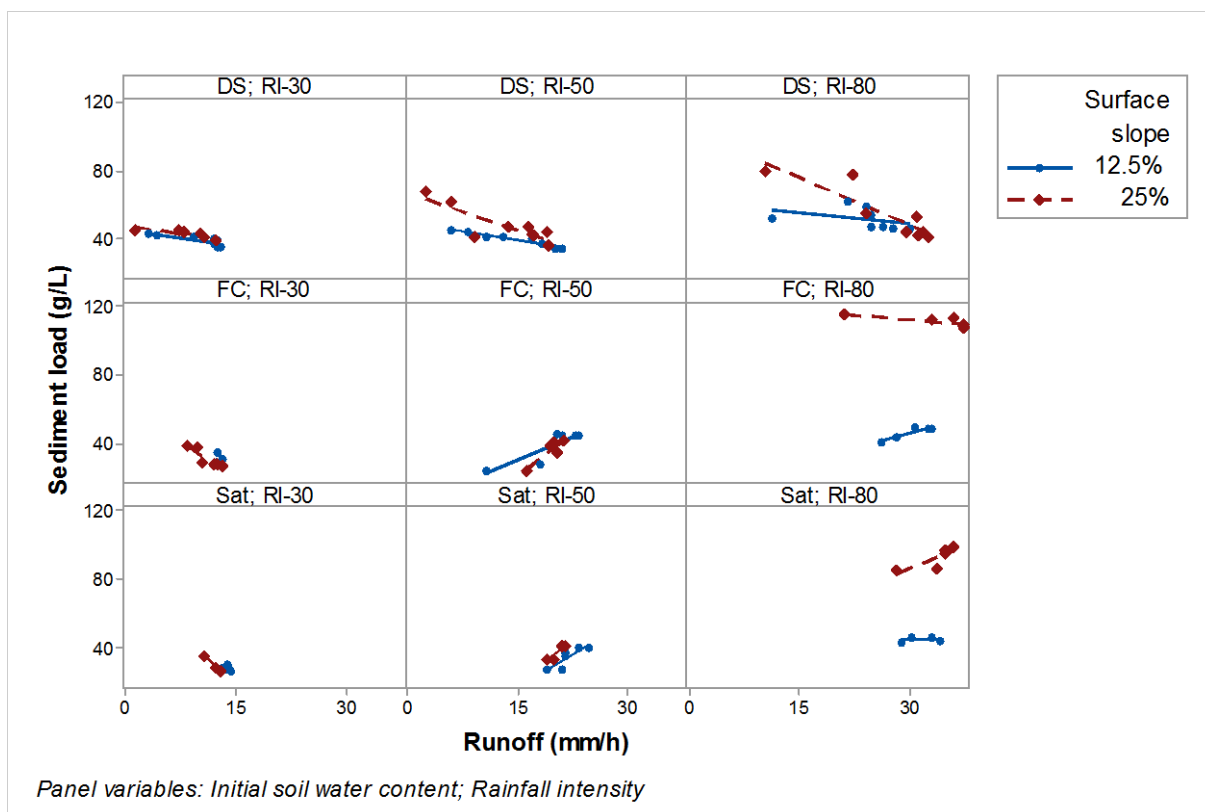
285

286 **Figure 1**



287

288 **Figure 2**



289

290

291 **Table 1.** Rainfall simulation experimental conditions.

Rainfall intensity mm h <sup>-1</sup>	Slope		Initial soil water content	
	%	°	w w <sup>-1</sup>	Last rain
RI-30	12.5	≈7	0.03 (DS)	25 days ago
RI-50	25	≈14	0.29 (FC)	24 h ago, 10 mm h <sup>-1</sup>
RI-80			0.33 (SAT)	15 min ago, 10 mm h <sup>-1</sup>

292

293 **Table 2.** Sample sizes, medians, average ranks and standardized values of these ranks given  
 294 by the nonparametric Kruskal-Wallis test, for each combination of the three factors, slope  
 295 (12.5%, 25%), initial soil water content (DS-dry soil, FC-near field capacity, SAT-near soil  
 296 saturation) and rain intensity (RI-80 mm h<sup>-1</sup>, RI-50 mm h<sup>-1</sup>, and RI-30 mm h<sup>-1</sup>). Means and  
 297 grouping information using the Games-Howell method and 95% confidence (means that do  
 298 not share a letter are significantly different).

Treatment	N	Kruskal-Wallis test			Games-Howell pairwise comparisons																
		Median	Ave Rank	Z	Mean	SE Mean															
25% FC RI-80	5	37.2	74.7	3.6	36.12	0.81	a														
25% Sat RI-80	4	34.8	72.4	3.0	34.80	0.49	a														
12.5% Sat RI-80	5	30.3	62.8	2.4	31.30	0.97	a	b													
25% DS RI-80	5	31.2	62.3	2.3	31.14	0.51		b													
12.5% FC RI-80	3	32.4	64.8	2.0	32.00	0.72	a	b													
12.5% DS RI-80	5	26.4	54.2	1.5	26.64	1.01		b c													
12.5% Sat RI-50	5	21.6	46.4	0.7	22.44	0.67			c d												
12.5% FC RI-50	5	22.8	44.5	0.5	22.08	0.58			c d												
25% Sat RI-50	4	20.4	37.6	-0.2	20.33	0.61			d												
25% FC RI-50	4	20.1	37.0	-0.2	20.25	0.40			d												
12.5% DS RI-50	4	19.2	33.1	-0.6	19.05	0.94			d	e	f	g	h	i	j						
25% DS RI-50	4	18.0	29.1	-0.9	17.93	0.66			d	e											
12.5% Sat RI-30	5	13.9	22.7	-1.7	13.87	0.20				e		g	i	k							
25% Sat RI-30	3	12.9	13.7	-2.0	12.72	0.18						g	h	i	j	k	l				
12.5% FC RI-30	5	12.6	14.1	-2.6	12.77	0.16								i	j	k	l				
25% FC RI-30	4	12.3	9.5	-2.7	12.08	0.58										k	l				
25% DS RI-30	3	10.8	3.7	-2.8	11.10	0.62										k	l				
12.5% DS RI-30	5	12.6	10.2	-3.0	12.44	0.17						f		h	j		l				

299

300