Application of the Tensegrity Principles on Tensile Textile Constructions

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ABSTRACT: The purpose of this document is to study the application of Tensegrity principles on tensile textile constructions, which is one of points of the PhD Thesis that the author is writing under the tutorship of Prof. Josep Ignasi Llorens and Prof. Ramon Sastre, professors at the Polytechnic University of Catalunia. This work studies the basic concept of Tensegrity unit, its classification according a previous researcher (Anthony Pugh) and the author's contribution, focused on new generations of forms. Through the geometry and computer software, another typology and a constructive simple method is developed, bearing in mind, some aspects as important as system pretension to find its balance.

The objective principal is to contribute in a particular way to the application of the tensegrity in architectural spaces, in this case sports spaces through a new proposal that generates an external ring in tensegrity with a central dome, free of any interior support, by formfinding a diamond membrane pattern with discontinuous struts in a double layer that find their equilibrium through the tension of the membrane.

In the following examples one can observe that traditional tensegrity tendons are replaced by membranes $Fig\ 1$, which is the main contribution of this work that finds geometry and its constructive method of the different prototypes with the help of software like AutoCAD and WinTess (a software development by Ramon Sastre), which verifies the structural equilibrium.

Key Words: Tensegrity Unit, Formfinding, Continuous Membrane, Diamond Pattern, Single Layer, Double Layer, Constructive Method, Pretension.

1. DEFINITION OF TENSEGRITY

The tensegrity geometry is defined by the equilibrium of tensile and compressive forces. The tensegrity geometry is characterized for having discontinuous compression bars, which remain in equilibrium by tensed cables. The balance is achieved because all the compression and tension forces are perfectly distributed, that is to say work jointly, where the structural form is guaranteed because finally the system is closed and auto-balanced, as Fuller [1] had said "Islands of compression in an ocean of tensions".

"Tensegrity describes a closed structural system composed of a set of three or more elongate compression struts within a network of tension tendons, the combined parts mutually supportive in such a way that the struts do not touch one another,

but press outwardly against nodal points in the tension network to form a firm, triangulated, prestressed, tension and compression unit." [2]

"A tensegrity system is established when a set of discontinuous compressive components interacts with a set of continuous tensile components to define a stable volume in space" [3]

2. PRECEDENTS

Tensegrity is a developing and relatively new system (more than 50 years old). Three men have been considered the inventors of tensegrity: Richard Buckminster Fuller (USA-1962), David Georges Emmerich (France-1964) and Kenneth D. Snelson (USA-1948). Although all of the three have claimed to be the first inventor, R. Motro mentions that Emmerich

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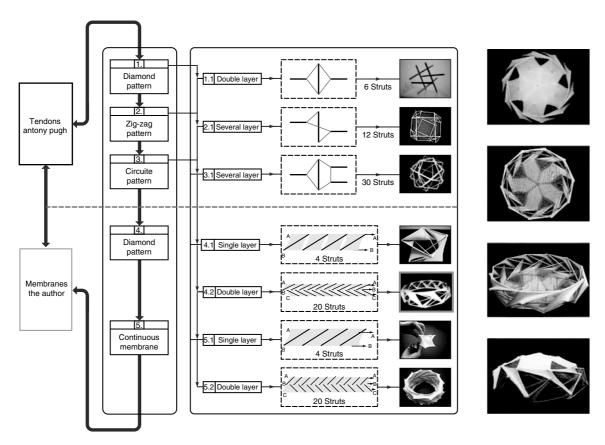


Figure 1. A comparision scheme between Anthony Pugh and a proposal by the author

reported that the first proto-tensegrity system, called "Gleichgewichtkonstruktion", was created by Karl Ioganson (Russia-1920). After in 1976 Anthony Pugh of the University of California (Berkeley) wrote his book "An Introduction to Tensegrity" where he showed and described different models; in addition he did a classification of the diverse existing typology [3]. He described three models, or basic patterns, with which the tensegrity structures can be constructed: a diamond pattern, a zigzag pattern and a circuit pattern. This classification originates from the relative position of the bars amongst themselves and the ends of the tendons [4]. This work rises from Anthony Pugh's classification of the diamond pattern and the position of the bars aligned in a single layer or a double layer, and proposes models using a continuous membrane and a diamond pattern.

3. FORMFINDING BY GEOMETRY

The tensegrity geometric construction of this study is based on:

- The conception of a basic module or tensegrity unit from polygons and polyhedrons (prisms and anti-prisms), Platonic and Archimedean solids. [5]
- The substitution of geometric components like edges and vertices by bars, cables and joints by faces in membranes.

 Forming more complex systems from groups and variations of the basic module.

Examples of different scales models in tensegrity with cables and membrane patterns. After we chose some of the models to define a classification and to do the structural analysis:



Figure 2. Examples of sixty scales models in tensegrity. Models constructed with an intuitive and experimental method based on the geometry. (Test with different materials)

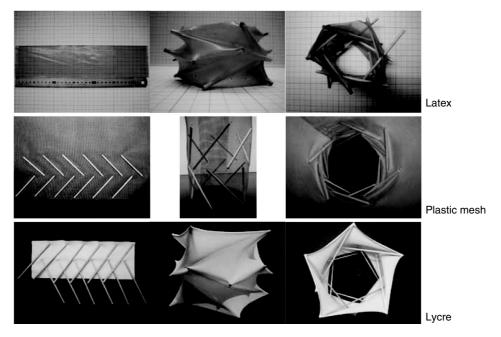


Figure 3. Models examples in different materials. The membrane in lycre is the material chosen to construct the scale models

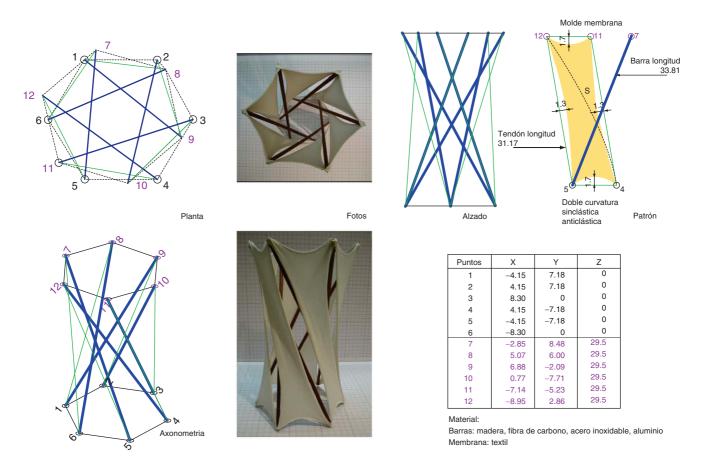


Figure 4. A tensegrity unit with 6 struts in a single layer - Geometric description

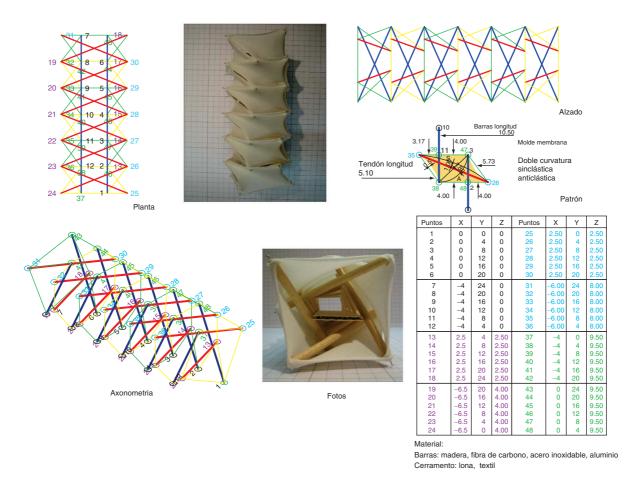


Figure 5. Six tensegrity units each one with 4 struts in a single layer - Geometric description. This example can be used like a path way or bridge

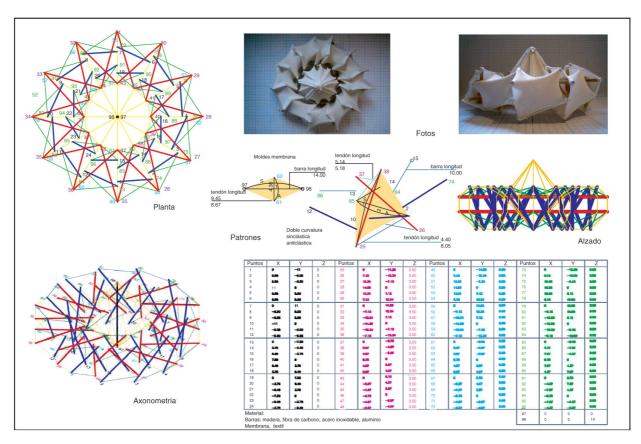


Figure 6. Twelve tensegrity units each one with 4 struts in a single layer (Torus with central mast) - Geometric description

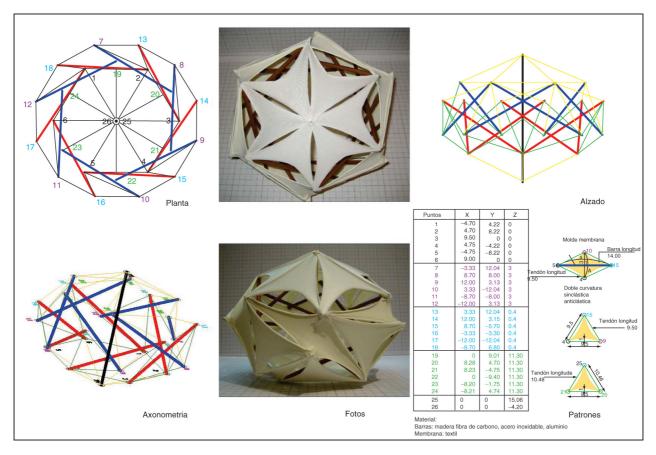


Figure 7. Tensegrity dome with twelve bars in a single layer with central mast - Geometric description

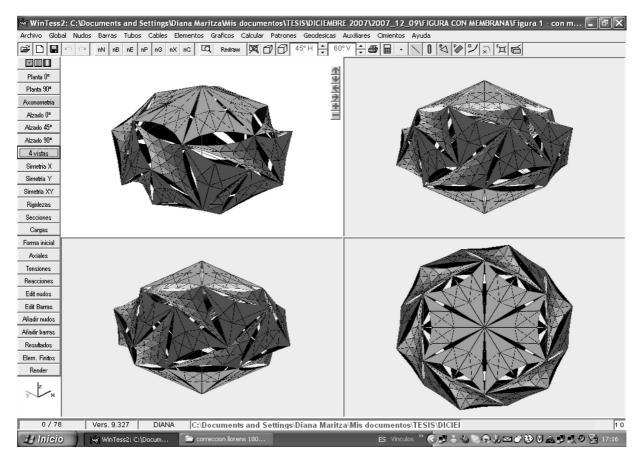


Figure 8. The structural analysis with WinTess considering self weight - The structure is in equilibrium

3.1. Classification

Model Types – Membrane patterns (contribution of the author)

The process is generated by cutting textile membranes, rhombus or diamond shape patterns (rhombus = major axis 17 cm, minor axis 12 cm), for the basic anti-prism

unit of four bars ($L = 22 \, cm$), which are arranged in an oblique direction or diagonal position. The bars are joined to the end points of the membrane as shown in Fig 9. The bars are tied to the adjacent pattern on one of its vertexes, and so on. The tied up units can be closed by joining the first bar and the last membrane

(a) Diamond membrane pattern and struts in a single layer

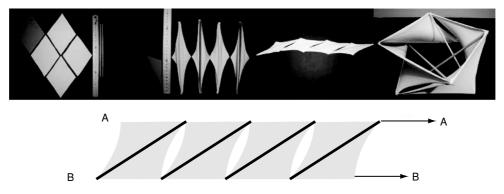


Figure 9. A tensegrity unit in a diamond pattern (an anti-prism of 4 struts)

pattern. The final anti-prism form has four paraboloids surfaces constructed from a flat rhombus. The initial position of the bars in this case is a single layer.

One can depart from the previously described process, and use a continuous rectangular membrane pattern ($15 cm \times 3.75 cm$) to find the form. The bars (L = 10 cm) arranged in a single layer and joined to the end points of the membrane as shown in *Fig 10*. Finally the system is closed by joining the first bar and the last corner of the membrane. The initial location of the bars was determined by an orthogonal single mesh ($3.5 cm \times 3.5 cm$).

The equilibrium of this unit tensegrity anti-prism with four bars and continuous membrane pattern is achieved through the tension of the membrane. The final form is a continuum of four paraboloids.

In this tensegrity ring, formfinding is generated by means of a continuous membrane pattern $(7.00 \, cm \times 36.75 \, cm)$, which has an initial rectangular form. For this model of twenty bars (L = $10 \, cm$) in a double layer, the bars are arranged in an oblique direction or diagonal position, in alternate form and are joined to the end points of the membrane like shown in *Fig 11*, and resemble the veins of a leaf. Finally the system is

(b) Continuous membrane pattern and struts in a single layer

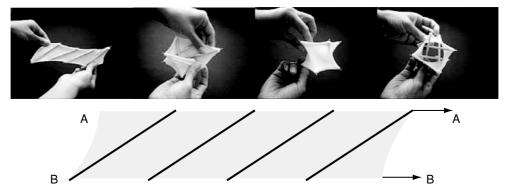


Figure 10. A tensegrity unit formed by continuous membrane pattern (an anti-prism of 4 struts)

(c) Continuous membrane pattern with twenty struts in a double layer

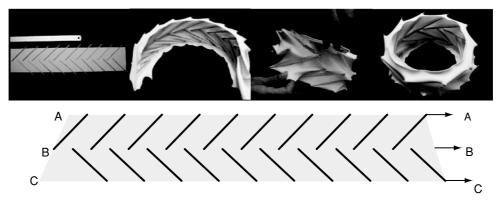


Figure 11. A tensegrity ring with continuous membrane pattern and 20 struts

closed by joining the first bars and the last corners of the membrane. The initial location of the bars was determined by an orthogonal double mesh $(3.5\,cm \times 3.5\,cm)$, whose distance was defined by the elasticity of the membrane regarding the length of the diagonal bar. The final form is a continuum of ten paraboloids above and ten paraboloids below.

Formfinding is generated by means of a diamond membrane pattern (rhombus = major axis 11.5 cm, minor axis 4 cm). This model is formed by two layers of twenty bars (L = 20 cm), which are arranged in an oblique direction or diagonal position. The bars are tied to the end points of the membrane as shown in Fig 12. Then the bars are joined to the adjacent pattern at one

of the remaining free end points. The procedure is repeated with the adjacent pieces, which include the alternate ones of the lower level that are joined to the top bars at the adequate place of the pattern continuum. The last two bars close the system.

The final ring form is a continuum of ten paraboloids (on the upper level) and ten paraboloids (on the lower level). To cover the upper ring a supported central dome is proposed that creates an internal free space. The central dome is formed by a central mast ($L = 9\,cm$) and several minor masts ($L = 6.5\,cm$) placed in a circular form, which are held by the tension of the membrane. At the same time, the membrane helps to balance the system and joins the top dome with the tensegrity ring.

(d) Diamond membrane pattern and mesh with twenty struts in a double layer

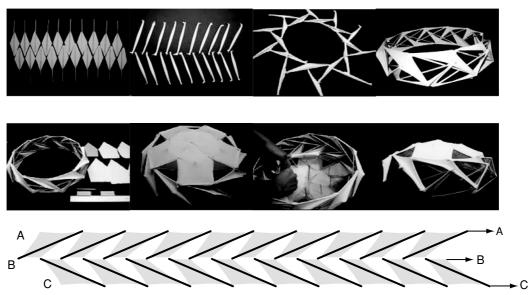


Figure 12. A tensegrity ring with a central dome and a diamond membrane pattern with 20 struts

In this case, the top part of the model uses a textile membrane and the lower part uses a mesh with which it is possible to observe the location of the masts and the bars inside the structure.

Finally a $40\,cm$ in diameter tensegrity structure has been completely constructed. To achieve a larger diameter, the number of bars would have to increase, but this must be proportional to the elasticity of the used membrane. Several models were constructed with major number of bars (24 - 30 struts). The material used (lycre) was not giving the sufficient stiffness when use more than 20 bars and for this reason there was chosen a scale model of 20 bars. If we increase the measure of the bars it is possible increase the diameter of the ring. (This is in progress to build a major scale prototype. Example: with 20 struts in a double layer $L = 50\,cm$, then we obtain a tensegrity ring with $100\,cm$ of diameter. The proportion length of bar to diameter is 1:2)

If one compares the model in Fig 12 with the continuous membrane in Fig 11 it can be observed that

though they have the same number of bars, the diameter of model in *Fig 12* is larger, approximately double, and for this reason the diamond pattern model was selected to continue with the structural analysis by means of WinTess software.

3.2. Formfinding by WinTess software

Form finding is generated using WinTess software [6]. First, an orthogonal 40 point mesh was constructed where the coordinates (x, y, z) came from the chosen model (*Fig 12*). After introducing the coordinates and defining the elements like: membranes, border cables, external cables, tubes, etc. with their respective structural characteristics and proper weight; a static equilibrium analysis of the prestressed membrane structure was performed. The balance is achieved because all the compression and tension forces are perfectly distributed, that is to say they work jointly, where the structural form is guaranteed, because finally the system is closed and auto-balanced.

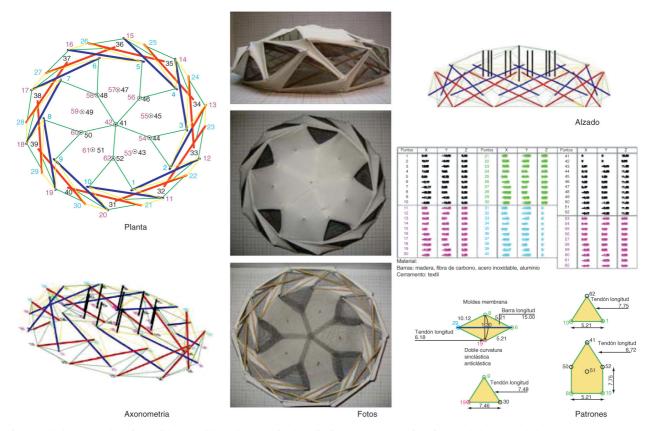


Figure 13. Stucture drawing with AutoCAD-Geometric description. The tensegrity ring and the central dome were represented with membrane and a net of cables

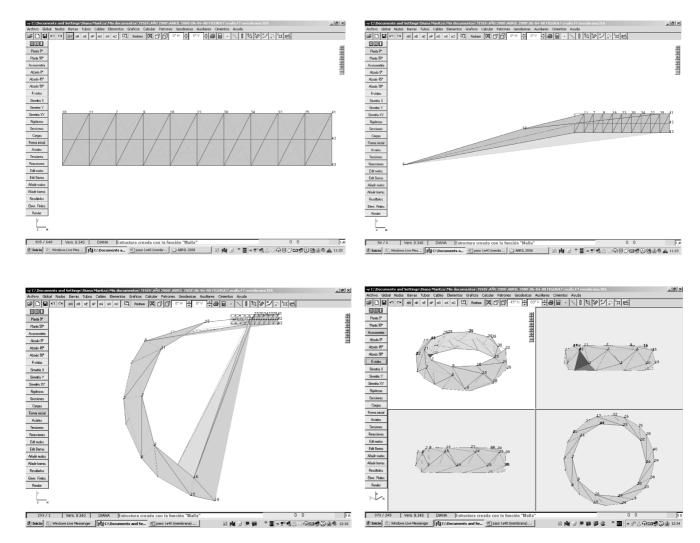


Figure 14. A tensegrity ring generated by WinTess. The tensegrity ring is represented with membrane and a net of cables to prevent the movements of the systems

4. STRUCTURAL ANALYSIS

Tensegrity structures are characterized because of their: [7]

- Discontinuous elements that work under compression,
- Prestressed structure.
- Auto-balanced structure.

In the following analysis the model is tested for external loads, first for wind at $170 \, km/h$, and then for $50 \, kg/m^2$ of snow. The tensegrity ring has sufficient stiffness to withstand the wind, however the major horizontal displacement is of $1143 \, mm$, therefore the central dome moves also, hence it is necessary to use

external elements to prevent the displacement and probably the collapse of the structure.

Pressure changes, depending on the direction of the wind over the membrane, and deforms and creates points of suction (dynamic pressure for $150 \, km/h$ wind over the membrane is $100 \, kg/m^2$ approximately). In case of snow, the central dome has a vertical displacement of $800 \, mm$ at the membrane where the maximum stress is located.

Exterior cables and tubes are proposed to prevent these exceptional displacements. The exterior tubes are placed surrounding the ring so that they continue in the direction of the forces coming from the top

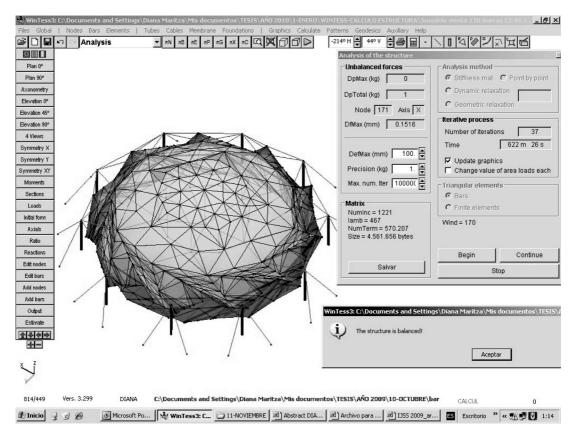


Figure 15. Structural analysis by WinTess–Wind 170 km/h - Structure is represented with membrane and a net of cables to prevent the movements of the system

membrane dome. The pretension cables can then increase the stiffness of the structure, and contribute to support the balance of the system.

Structural characteristics of the model elements:

- Membrane: Ferrari Fluotop T2 1202 Prestress
 1. % = 32.5 daN/5 cm = 650 kg/m Resistance
 Rk = 560/560 daN/5 cm = 11200,0 kg/m Safety
 factor (5) = Rd = Rk/5 = 112 daN/5 cm = 2240 kg/m
- **Border cables (Boltrope):** $1 \times 91 (36 mm)$ Inox 36 - **Section** 753 mm^2 - **Elasticity modulus** $1.380 t/cm^2 = 138 kN/mm^2$ - **Q** = 87,21 t = 872,1 kN
- External cables (Guyrope): WS-2 (36 mm) Galv 36 Section 855 mm² Elasticity modulus 1.635 $t/cm^2 = 163,5 \ kN/mm^2$ Q = 125,46 t = 1.254,6 kN
- Tubes of the ring: L = 20 m $400-10_{S235}$ Section $122,522 cm^2$ Elasticity modulus $2.100 \ t/cm^2 = 210 \ kN/mm^2$ Density $7,85 \ t/m^3 = 78,5 \ kN/m^3$
- Central mast of the dome: $L = 9 m 110-5_$S235 Section 16,493 cm^2 Elasticity modulus <math>2.100 t/cm^2 = 210 kN/mm^2 Density 7,85 t/m^3 = 78,5 kN/m^3$

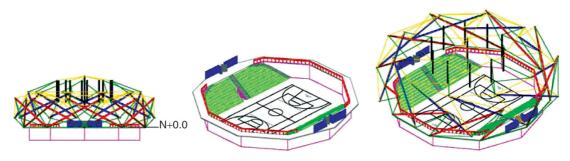


Figure 16. Application of the tensegrity ring to cover a sports arena

- Minor masts of the dome: L = 6.5 m $90-4_S235$ Section $10.807 cm^2$ Elasticity modulus $2.100 t/cm^2 = 210 kN/mm^2$ Density $7.85 t/m^3 = 78.5 kN/m^3$
- External tubes: $L = 8 m 250-8_S235$ Section 60,821 cm^2 Elasticity modulus 2.100 t/cm^2 = 210 kN/mm^2 Density 7,85 t/m^3 = 78,5 kN/m^3

Table 1. General data

Structure general data	
Number of nods	447
Number of bars	1296
Number of tubs	41
Number of elements	709
Number of cables	305
Covered surface	1.177,08 m ²
Volume (between membrane	
and plane $Z = 0$)	15.818 m^3
Membrane surface	2.959,96 m ²
Weight of the bars	53.807,38 kg
Weight of the membrane	3.847,94 kg
Membrane elongation modulus	65 T/m

5. APPLICATION

There exists a need for roof structures that can cover big surfaces and spaces, but free of any interior supports. After doing the pertinent calculations, a tensegrity ring is proposed with a central dome, using diamond membrane patterns with twenty struts in a double layer, to cover a 40 m diameter sports arena, which has a surface of $1.200 m^2$ and may be occupied by 626 persons, approximately.

6. CONCLUSIONS

This methodology allows these conclusions:

- Tensegrity is not a conventional structure.
- The balance is solved by formfinding, constructive methods and pretension possibilities, where models of continuous membranes and diamond patterns, with bars in a single layer or double layer are proposed.
- It is essential to know the initial state system (pretension and stiffness of the elements that compose it) and its behaviour when it is subjected to external actions.
- Tensegrity structures are kinematically weak and need geometrical stiffening elements, such as tension elements. [8]

- The analysis of the forces in the components is important, considering endogenous factors, like the internal prestress of the structure and exogenous factors, such as external loads, points of support, anchorages, etc.
- The major stress distribution given by the WinTess software shows the importance of property selection in the elements (to define dimensions). In addition it is observed that a safety coefficient is important to take account for the calculation.
- The difficulty of these systems lies in the fact that though they are auto-balanced, with external loads such as wind and snow, it is necessary to increase the stiffness of the elements and moreover they should be reinforced by external tubes, which help to prevent a collapse of the system in particular conditions.
- The system stiffness is achieved through the membrane prestress and auxiliary external elements such as tubes and cables.
- These systems are flexible in the Z axis, which makes them useful as elements or folding and unfolding systems. [9]
- To verify the hypotheses that are propose here, a major scale prototype will be constructed and a wind tunnel test will be performed also.

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