1	Intrinsic correlation between the fraction of liquid-like zones and the
2	β-relaxation in high-entropy metallic glasses
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29 Abstract

Lacking the structural information of crystalline solids, the origin of the relaxation 30 dynamics of metallic glasses is unclear. Here we report the evolution of stress relaxation 31 of high-entropy metallic glasses with distinct β -relaxation behavior. The fraction of 32 liquid-like zones, determined at each temperature by the intensity of stress decay, is 33 shown to be directly related to both the aging process and the spectrum of relaxation 34 modes obtained by mechanical spectroscopy. The results shed new light on the intrinsic 35 correlation between the static and dynamic mechanical response in high-entropy and 36 conventional metallic glasses, pointing towards a sluggish diffusion high-entropy effect 37 38 in the liquid dynamics.

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41 Letter

Owing to the disordered atomic structure, metallic glasses (MGs) show unique 42 properties [1-4]. Besides, high-entropy alloys (HEAs), containing equimolar 43 concentrations of each component, have been developed recently [5-7]. Benefitting 44 from the high configurational entropy, large lattice distortion, sluggish diffusion and 45 the cocktail effect [8,9], HEAs exhibit distinctive physical and mechanical properties 46 [5,9,10]. With the aim of blending the properties of MGs and HEAs, high-entropy 47 metallic glasses (HEMGs) have been developed [11-13]. However, the existence of 48 specific properties of HEMGs as compared to other families of MGs, especially the 49 presence of a high entropy - sluggish diffusion effect [14] and its effects on the glass-50 to-liquid transition and the aging/rejuvenation processes, which are essential to control 51 52 the glassy configuration and adjust the materials properties [11,15], have not been 53 clearly demonstrated.

Dynamic mechanical analysis (DMA) [2], i.e. mechanical spectroscopy, and stress 54 relaxation [16,17] have been proven powerful tools to characterize the dynamics of 55 56 MGs [17,18]. Stress relaxation has been investigated at different length scales by experiments [16,19] and simulations [20]. Besides, secondary β -relaxation, preceding 57 in temperature the collective, large-scale α -relaxation, is observed by mechanical 58 spectroscopy and has been associated with local (nano-scale) atomic phenomena 59 [20,21]. Although stress relaxation and mechanical spectroscopy observations are, 60 respectively, the time and frequency domain responses of the same mechanical 61 relaxation phenomenon, a direct evidence of the intrinsic correlation between β -62 63 relaxation and stress relaxation in MGs is still missing.

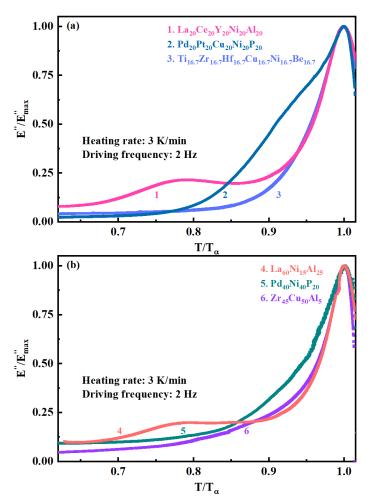
In this letter, we present a study over six different metallic glass formers. Three HEMGs and three 'conventional' MGs which are representative of the main compositional families of glass-forming alloys. By calorimetric and mechanical tests, we try to step forward in the solving of important questions, namely: What is the relation between the thermal activation of liquid like zones and the relaxation spectrum of metallic glasses? How the dynamical heterogeneity evolves during changes of the

glass state? And, finally, are there systematic dynamical differences between high-entropy and conventional metallic glass-formers?

72 For this purpose, we investigated the stress relaxation behavior of HEMGs and 73 MGs following the stress decay under a constant strain while heating in isothermal steps. The stress decay was monitored for 1800 s in each step from room temperature to the 74 75 glass transition. It is known that both stress and temperature are equally critical in controlling the stress relaxation dynamics of MGs [22-24], as the external stress reduces 76 77 the apparent flow activation energy [24]. Here, the applied strains are small and equal from room temperature to the glass transition, always within 0.3-0.6%. Within this 78 range the observed behaviors are basically produced by the temperature effects. The 79 80 selected compositions for this study are three representative HEMGs, $La_{20}Ce_{20}Y_{20}Ni_{20}Al_{20}$ (La-HEMG), $Pd_{20}Pt_{20}Cu_{20}Ni_{20}P_{20}$ (Pd-HEMG) [25] 81 and 82 Ti16.7Zr16.7Hf16.7Cu16.7Ni16.7Be16.7 (Zr-HEMG) and three representatives of 'conventional' MGs, La₆₀Ni₁₅Al₂₅ (La-MG), Pd₄₀Ni₄₀P₂₀ (Pd-MG), and Zr₄₅Cu₅₀Al₅ 83 (Zr-MG), with obvious different β -relaxation behaviors. As seen in the methods 84 85 section in supplementary materials (Figs. S1 (a,b)), all these MGs have a significant 86 supercooled liquid (SCL) region and excellent stability against crystallization. For each composition the tests were performed in both as-quenched samples (cooled from the 87 melt at ~ 10^5 - 10^6 K s⁻¹) and relaxed samples (cooled from the SCL at 1.67×10^{-3} K s⁻¹). 88

The temperature dependence of the normalized loss modulus $\frac{E''}{E''_{max}}$ obtained by 89 DMA is shown in Figs. 1 (a,b). With a driving frequency of 2 Hz, the maximum of loss 90 modulus E''_{max} , which corresponds to the α -relaxation peak, is observed at $T_{\alpha} = 504$, 91 588 and 708 K for La-HEMG, Pd-HEMG and Zr-HEMG and at 488, 602 and 730 K 92 for the La-MG, Pd-MG and Zr-MG, respectively. The β -relaxation is observed as a 93 distinct peak [18,26] for the La-based glasses, a shoulder [17,18] for the Pd-based and 94 an excess wing [27,28], almost merged into the α -relaxation, for the two glasses of the 95 Zr family. 96

97 While crystalline defects and grain boundaries are crucial for the internal friction 98 of crystalline metals [29], the heterogeneous nanoscale structure seems to be the main 99 factor in the case of MGs [30,31]. It has been accepted that MGs can be regarded as 100 viscous, weak-bond regions caged in an elastic, strong-bond matrix, as described by the 101 models based on flow units [32-34] or soft spots [33]. Within this picture, the β-102 relaxation is seen as a reversible process of local atomic rearrangement of these soft 103 spots and it is closely correlated to the mechanical properties of glasses, particularly 104 with the underlying mechanisms of plastic deformation [17,18].



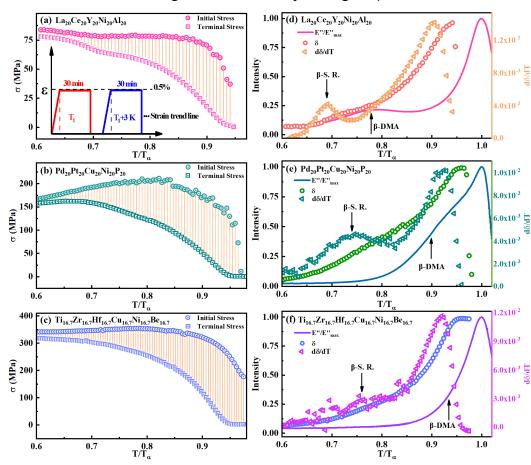
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106 Figure 1. Normalized loss modulus $\frac{E''}{E''_{max}}$ as a function of the normalized temperature T/T_{α} . 107 T_{α} stands for the peak temperatures of α relaxation probed at 2 Hz. (a) HEMGs (b) 108 'conventional' MGs.

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110 The stress drop of the HEMGs from room temperature to near T_{α} (for details see 111 the methods section in supplementary materials) is shown in Fig. 2 (a)-(c). After 112 applying a constant strain, the stress relaxes with time. We define $\delta = \frac{\sigma_0 - \sigma_r}{\sigma_0}$ as the

intensity of stress relaxation, where σ_0 and σ_r are the initial and terminal stresses of 113 each 30 min relaxation curve. The intensity of stress drop δ can be associated to the 114 fraction of liquid-like activated flow units and to viscosity [19,35]. The σ_0 and σ_r of 115 each relaxation curve are depicted as open circles and squares, respectively. One can 116 notice that the decay of σ_0 is not prominent until close to T_g , whereas the decay of σ_r 117 accelerates near T_{β} (the temperature of the β -relaxation) and then drops to zero near 118 T_q . In order to more clearly reveal the influence of the distinct β -relaxation behaviors, 119 in Figs. 2 (d)-(f) we depict together the evolution of δ (for 30 min of stress relaxation 120 each 3 K step) and the normalized loss modulus $\frac{E''}{E''_{max}}$ (driving frequency of 2 Hz and 121 a heating rate of 3 K min⁻¹). With the increase of temperature near T_{β} , both of these 122 magnitudes accelerate their rising reaching a maximum around T_g . The evolution of δ 123 in the different HEMGs exhibits a hint of a peak for the La-HEMG a shoulder for Pd-124 HEMG and an excess wing for Zr-HEMG, replicating the β -relaxations. 125



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127 Figure 2. Stress relaxation measured at stepping temperature from room temperature to T_{α} for

128 (a) La-HEMG, (b) Pd-HEMG, and (c) Zr-HEMG. Evolution with temperature of stress drop δ , 129 stress drop change rate $\frac{d\delta}{dT}$ and normalized loss modulus $\frac{E''}{E''_{max}}$ of (d) La-HEMG, (e) Pd-130 HEMG, and (f) Zr-HEMG.

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Interpreting δ as the fraction of liquid-like activated flow units [19][48], the 132 increase of δ indicates that a higher fraction of atoms are unfrozen to undergo inelastic 133 deformation [36,37]. This fact can be viewed as the increase of atomic/molecular 134 135 mobility caused by the thermal activation of microscopic movements. It is interesting to discuss the similarity between the loss modulus and the intensity of stress relaxation. 136 $\delta(T)$ shows the same features as $\frac{E''(T)}{E''_{max}}$, but shifted to lower temperatures. In this work, 137 the driving frequency of DMA experiments was 2 Hz, while the "effective driving 138 frequency" of the stress relaxation tests can be estimated as $f \sim \frac{1}{30 \text{ min}} = 6 \times 10^{-4} \text{ Hz}$. It 139 is well known that the loss modulus is shifted to low temperatures as frequency 140 decreases [38]. Following ref. [19], $\delta(T)$ can be interpreted as the fraction of liquid-141 142 like zones, i.e. zones that can relax stress within the duration of the test. Similarly, the integration of the relaxation spectrum obtained by DMA, $\int_0^T \frac{E''(T)}{E''_{max}} dT$, is proportional 143 to the fraction of relaxation modes faster than $\sim f^{-1}$. Therefore, the derivative 144 $d\delta(T)/dT$ should be proportional to $E''(T)/E''_{\text{max}}$ at a frequency of $f \sim 6 \times 10^{-4}$ Hz. 145 Figs. 2 (d)-(f) shows the behavior of $d\delta(T)/dT$ with clear α and β peaks displaced 146 to lower temperatures, as expected for such a low driving frequency. For all the three 147 materials, the position of the $d\delta(T)/dT$ maximum is found at $\sim 0.9T_{\alpha,2\text{Hz}}$, in 148 agreement with the temperatures at which the slope of the $\tau_c(T)$ (see Fig 3 and 149 discussion below) is observed to change, indicating the onset of the dynamic glass 150 transition for this frequency. For Pd-HEMG, the α and β become well separated in 151 comparison with the 'shoulder' observed at f = 2 Hz. For Zr-HEMG, the excess wing 152 observed at f = 2 Hz is moved towards lower temperatures and starts to be similar to 153 a broad shoulder of low intensity. The same intrinsic correlation between loss modulus 154 and $d\delta(T)/dT$ can be found in the three 'conventional' La, Pd and Zr MGs (see Figs. 155

S2 of supplementary materials). This direct relationship between the fraction of liquid-156 like zones and the spectrum of relaxation modes is in agreement with the view of MGs 157 being composed by a spatial distribution of zones of different relaxation time [39] or, 158 in other words, more or less liquid-like in nature. The transition from inhomogeneous 159 to homogenous flow is associated to the fraction of liquid-like zones reaching a 160 percolation or threshold fraction of around 25% [19]. Therefore, the results presented 161 here suggest that one could establish a readily way of estimating the inhomogeneous to 162 homogeneous line in a strain rate – temperature map by integrating the $\frac{E''(T)}{E''_{max}}$ spectra 163 obtained at different frequencies. 164

The results in Figs. 2 correspond to as-quenched samples. In this samples, the 165 evolution of liquid-fraction zones is not only due to the activation of the β and α 166 relaxations as temperature increases, but also to the physical aging process (or structural 167 relaxation) occurring during the tests [40]. Physical aging drives the glass to more stable 168 and denser configurations, reducing the excess free volume in the structure and so also 169 170 reducing the intensity of the secondary relaxation and the fraction of liquid-like zones. Figs. S3 in supplementary materials show the results of DMA and stress relaxation tests 171 on relaxed samples. The secondary peak in $E''(T)/E''_{max}$ shows a reduced intensity as 172 expected for well relaxed materials, as now reflects the activation of the β relaxation in 173 174 a structure with comparatively much less liquid-like zones. For $d\delta(T)/dT$ the peak is clearly reduced, but still evident, for the Pd glasses while it becomes almost 175 indistinguishable for the La systems. The same effect is observed in calorimetry (see 176 177 **Figs.** S4) where the activation of the β relaxation shows a clear signature in Pd systems while it is negligible in La based. This suggests a different nature of the secondary 178 179 relaxation in Pd and La systems. It can be correlated to the increase of the liquid-like volume fraction in Pd, whereas in La systems it seems to be related to an isolated 180 mobility mechanism which remains too fast to contribute to the overall stress relaxation 181 at longer times. 182

183 In order to further characterize the relaxation behavior of the glasses, the stress 184 relaxation curves at each temperature step were fitted to the phenomenological 185 Kohlrausch-Williams-Watts (KWW) equation [19,41]

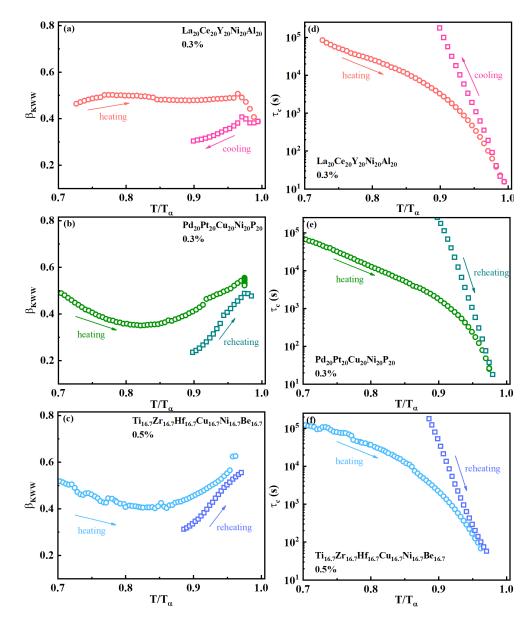
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$$\sigma(t) = \sigma_0 \exp\left(-\frac{t}{\tau_c}\right)^{\beta_{\rm KWW}}$$
(1)

where $\sigma(t)$ is the stress at time t, β_{KWW} is a stretching exponent, a parameter linked 187 to the dynamic heterogeneity, and τ_c is the stress relaxation timescale. Some selected 188 results are shown in Fig. 3. Figs. S5-S7 in supplementary materials show the relaxation 189 190 curves at various temperatures and details of the corresponding fittings with Eq. (1). Figs. S8, show the results for the La, Pd and Zr-MGs. The overall behavior is similar 191 192 for all the alloys. At $T/T_{\alpha} < 0.7$ the stress relaxation achieved during 30 min is small, less than 15%. This indicates that the relaxation timescale is much longer than the 193 experimental time window. For the relaxed samples, this happens until $T/T_{\alpha} \lesssim 0.85$ 194 195 due to the reduction of liquid-like zones in the more densified state. The results in this 196 low temperature range are not shown in Fig. 3 and will not be discussed here as a longer experimental relaxation step would be necessary to proper characterize τ_c and β_{KWW} . 197 In the temperature region 0.7 $< T/T_{\alpha} < 0.9$, $\tau_c(T)$ decreases with temperature, 198 going from values above 10^4 s towards a value of $\tau_c \sim 10^3$ s at $T/T_{\alpha} \sim 0.9$. The 199 parameter β_{KWW} varies within 0.35 to 0.6, which are typical values in the relaxation 200 201 of amorphous alloys [19,26,42,43].

The physical aging of the glasses during the tests seems reflected on the behavior 202 of $\beta_{KWW}(T)$. Although aging drives the system to a lower energy state with less overall 203 204 internal friction [38], various recent studies have shown that the underlying relaxation 205 time distribution becomes more heterogeneous during aging [16,43-45]. Thus, although the total intensity of stress relaxation is smaller in the aged samples, the different 206 207 timescales participating in it become more separated as indicated by a decrease of $\beta_{\rm KWW}(T)$. This phenomenon is also observed here in the temperature range going from 208 $T/T_{\alpha}=0.7$ to 0.8. The as-quenched samples start with a $\beta_{\rm KWW}(T) \sim 0.5$, a level of 209 dynamical heterogeneity similar to what is observed in the SCL [46]. As soon as the 210 fraction of activated liquid-like zones increases, the aging process is allowed to proceed, 211 and $\beta_{KWW}(T)$ decreases until values around 0.3, as it was also observed for very well 212 aged glassy states in other works [16,43,44]. At the higher temperatures, the transition 213

from a relaxed glass towards the liquid state shows, in parallel, the increase of the 214 fraction of liquid-like-zones and the $\beta_{KWW}(T)$ parameter, which returns to values in 215 216 the range 0.5-0.6 at the glass transition. The reason of the more constant behavior of $\beta_{\text{KWW}}(T)$ in the La-HEMG and MG (see Fig. S3) is not clear but may be related to the 217 presence of a distinct secondary process that dominates the atomic mobility at the 218 temperature range $T/T_{\alpha}=0.7$ - 0.8. It is worth noticing that the evolution of $\beta_{KWW}(T)$ 219 (shown in Figs. 3b and 3c) seems to be concave regardless of the material state. The 220 pre-annealed and well-relaxed samples show also a striking concave nature (see Fig. 221 **S9**). However, the duration of the isothermal steps of the experiments presented in this 222 work is not long enough to conclusively study the behavior of relaxed samples at low 223 224 temperatures.



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Figure 3. The fitted KWW parameters β_{KWW} of (a) La-HEMG, (b) Pd-HEMG and (c) Zr-HEMG and τ_c (d) La-HEMG, (e) Pd-HEMG and (f) Zr-HEMG with initial as-quenched state and with well relaxed state (second cycle of stress relaxation measurements after slowly cooling from T_g).

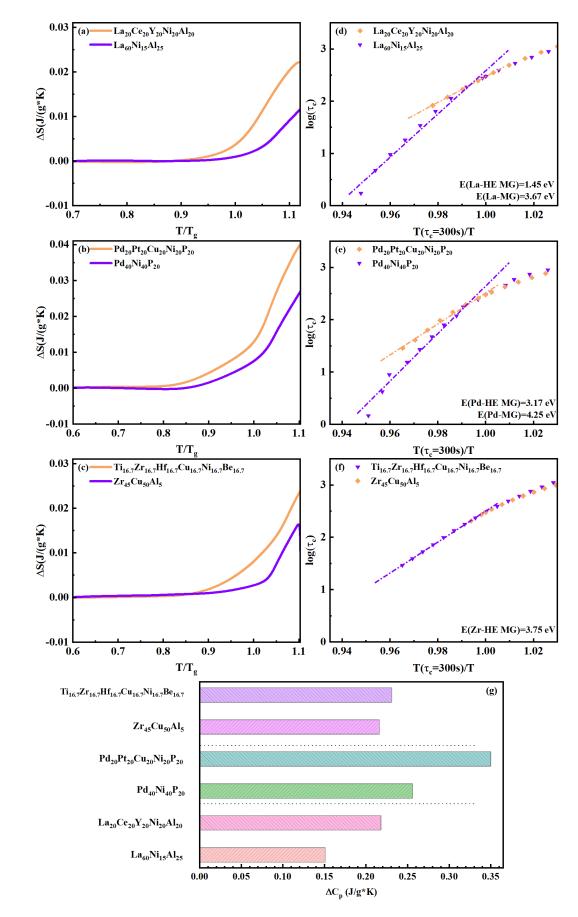
At $T/T_{\alpha} \sim 0.9$, the relaxation times of the six glasses are of the same timescale than the isothermal steps (2100 s), this allows the glasses to get closer to an ergodic state within each temperature step. This is observed by the progressive change of the slope of $\tau_c(T)$, which signals the transition from glass to SCL dynamics. Accordingly, between $0.9 < T/T_{\alpha} < 0.95$ the relaxation dynamics are more accelerated by the increase of temperature. At $T/T_{\alpha} \sim 0.93$ -0.94, all materials achieve full relaxation during the 30 min tests. Finally, above this temperature, the onset of crystallization is
clearly detected in the shape of the relaxation curves, thus also dictating the upper limit
of the validity of the KWW equation to describe the experimental data (see Figs. S5S7).

Finally, we will discuss the intrinsic effect of high entropy in the glass and liquid 240 dynamics. The difference of specific heat between the glassy alloys and the crystalline 241 baselines was measured by differential scanning calorimetry (DSC). The $c_p(T)$ curves 242 are given in Figs. S4 in supplementary materials. Fig. 4 (a)-(c) and (g) shows the step 243 $\Delta c_{p,T_g} = c_{p,l} - c_{p,g}$ at the glass transition and the integration $\Delta S_{lg-x} =$ 244 $\int_{T_1}^{T_2} \frac{c_{p,lg}(T) - c_{p,x}(T)}{T} dT$, which corresponds to the excess of entropy between the 245 amorphous (glass/liquid) and the crystallized samples. It can be observed that the 246 HEMGs systematically show higher glass transition steps, $\Delta c_{p,T_g}$, and configurational 247 entropies in comparison with the conventional MGs. 248

The mobility in the glass is determined by both the aging process and the fast part 249 of the relaxation spectrum, dominated by the β -relaxation and the high-frequency wing 250 of the α -process. The specific shape of this spectrum is primarily dependent on the kind 251 of metallic glass family, independently of the high-entropy or 'conventional' nature of 252 the alloys. Interestingly, the value $E_{\beta}/RT_g \approx 25 \pm 2$ (see Table S1) derived from stress 253 254 relaxation is consistent with the empirical relationship $E_{\beta}/RT_{q} \approx 26$ found in various MGs [17,18], in agreement with previous dynamic mechanical analyses [47] and 255 amplitude-modulation atomic force microscopy results [48]. On the other hand, the 256 relaxation tests performed in this work, allows us to study the temperature evolution of 257 258 the dynamics in the region of the glass transition, dominated by the α (or viscous) relaxation. Fig. 4 (d)-(f) shows the evolution with temperature of τ_c in the region 259 where it becomes shorter than 300 s. The fragility of the liquid, $m = \frac{d (\log \tau_c)}{d(T_g/T)}$, or 260 equivalently, the apparent activation energy of the relaxation, E_{α} , can be calculated in 261 this region. It is found that the HEMGs show always a stronger liquid behavior than 262

their MGs counterparts. At the same relative temperatures respect to the glass transition,
the Pd and La HEMGs show slower dynamics that their corresponding 'conventional'
counterparts.

Configurational and vibrational entropy contribute to the total entropy of metallic 266 glasses [49-51]. The vibrational entropy in MGs (and their undercooled liquids) is 267 approximately equal to that of the corresponding crystals, [49,52], and this implies that 268 the excess entropy of MGs can be mainly attributed to the configurational entropy 269 270 difference [50,52]. The rough correlation usually observed in glass formers between the Δc_p step at the glass transition and the liquid fragility is not fulfilled for the studied 271 alloys and this can be another trait related to the high-entropy effect. The larger Δc_p 272 of the HEMGs indicates that, in these alloys, the glass to liquid transition unfrozens the 273 274 possibility to explore a larger quantity of configurations [53]. However, this is not correlated to faster dynamics (or a more fragile liquid behavior) but to the high entropy 275 of mixing of these compositions. This points towards the sluggish diffusion high-276 entropy effect in the liquid dynamics as suggested in other works [14,54,55]. 277



280 Figure 4. The excess of entropy ΔS of (a) La-based, (b) Pd-based and (c) Zr-based HEMGs

and MGs. Stress relaxation time τ_c vs reciprocal temperature $T(\tau_c = 300s)/T$ and fitted Arrhenius plots for (d) La-based, (e) Pd-based and (f) Zr-based HEMGs and MGs. (g) The step Δc_p at the glass transition of well relaxed samples of HEMGs and MGs.

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In summary, the evolution of stress relaxation of high entropy and conventional 285 286 MGs with different types of β -processes was investigated. The study of the timescale and shape of the relaxation curves indicates that HE-MGs tend to have an enhanced 287 288 strong liquid behavior above the dynamic glass transition, and that aging of the glass increases the relative separation of the relaxation times contributing to the stress 289 290 relaxation, as reflected in the decrease of the β_{KWW} exponent. Importantly, this work shows that the fraction of zones that behave liquid-like during a fixed time interval is 291 proportional to the relaxation mode spectrum at the corresponding low frequency. Our 292 results shed new light on the intrinsic correlation between the static and dynamic 293 mechanical response in high-entropy and conventional metallic glasses, and they 294 provide a practical guideline for understanding, and subsequently controlling, the 295 296 mechanical behavior of HE-MGs.

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