

UNIVERSITAT POLITÈCNICA DE CATALUNYA



UNIVERSITAT POLITÈCNICA DE CATALUNYA
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**Escola Superior d'Enginyeries Industrial,
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MASTER THESIS

APPENDIXES

Study of stability control systems applied to a racing car

Author:

Albert INGLÉS NAVARRETE

Supervisor:

Dr. David GONZÀLEZ

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Declaration of Authorship

I, Albert INGLÉS NAVARRETE, declare that this thesis titled, 'Study of stability control systems applied to a racing car' and the work presented in it is my own. I confirm that this work submitted for assessment is my own and is expressed in my own words. Any uses made within it of the works of other authors in any form (e.g., ideas, equations, figures, text, tables, programs) are properly acknowledged at any point of their use. A list of the references employed is included.

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Appendix A

Tire Model: Magic Formula 6.1

In this appendix, the equations and description of the Magic Formula 6.1 tire model will be performed.

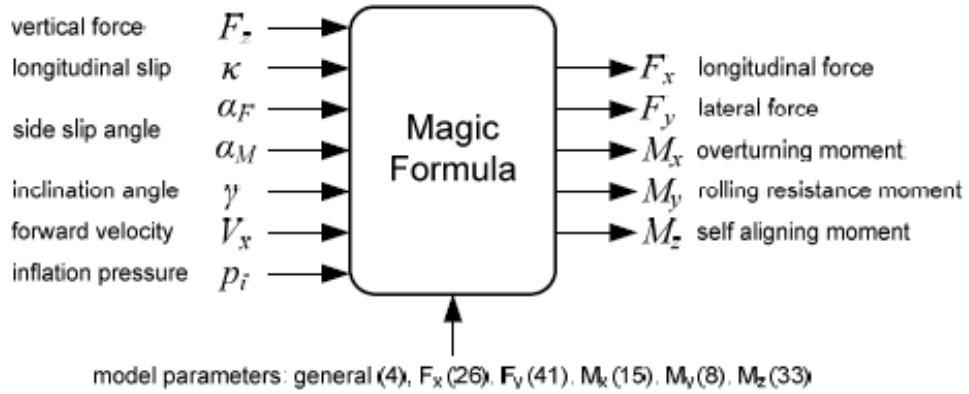


FIGURE A.1: Inputs and outputs of the Magic Formula. Source: [1], pag. 11

The first step is to dimensionless the vertical force and the pressure:

$$df_z = \frac{F_z - F_{z,0}}{F_{z,0}} \quad (\text{A.1})$$

$$dP_i = \frac{P_i - P_{i,0}}{P_{i,0}} \quad (\text{A.2})$$

A.1 Longitudinal force F_x

$$F_x = (D_x \sin [C_x \arctan\{B_x \kappa_x - E_x \arctan(B_x \kappa_x - \arctan(B_x \kappa_x))\}] + S_{V_x}) \cdot G_{x\alpha} \quad (\text{A.3})$$

Pure slip:

$$\kappa_x = \kappa + S_{H_x} \quad (\text{A.4})$$

$$C_x = P_{C_{x1}} \lambda_{C_x} \quad (\text{A.5})$$

$$D_x = \mu_x F_z \quad (\text{A.6})$$

$$\mu_x = (p_{D_{x1}} + p_{D_{x2}} df_z)(1 - p_{D_{x3}} \gamma^2)(1 + p_{p_{x3}} dp_i + p_{p_{x4}} dp_i^2) \lambda_{\mu_x} \quad (\text{A.7})$$

$$E_x = (p_{E_{x1}} + p_{E_{x2}} df_z + p_{E_{x3}} df_z^2)(1 - p_{E_{x4}} \text{sgn}(\kappa_x)) \lambda_{E_x} \quad (\text{A.8})$$

$$K_{x\kappa} = (p_{K_{x1}} + p_{K_{x2}} df_z) \exp(p_{K_{x3}} df_z)(1 + p_{p_{x1}} dp_i + p_{p_{x2}} dp_i^2) F_z \lambda_{K_{x\kappa}} \quad (\text{A.9})$$

$$B_x = \frac{K_{x\kappa}}{C_x D_x} \quad (\text{A.10})$$

$$S_{H_x} = (p_{H_{x1}} + p_{H_{x2}} df_z) \lambda_{H_x} \quad (\text{A.11})$$

$$S_{V_x} = (p_{V_{x1}} + p_{V_{x2}} df_z) F_z \lambda_{V_x} \lambda_{\mu_x} \quad (\text{A.12})$$

Combined longitudinal correction factor:

$$G_{x\alpha} = \frac{\cos[C_{x\alpha} \arctan\{B_{x\alpha} \alpha_s - E_{x\alpha} (B_{x\alpha} \alpha_s - \arctan(B_{x\alpha} \alpha_s))\}]}{\cos[C_{x\alpha} \arctan\{B_{x\alpha} S_{H_{x\alpha}} - E_{x\alpha} (B_{x\alpha} S_{H_{x\alpha}} - \arctan(B_{x\alpha} S_{H_{x\alpha}}))\}]} \quad (\text{A.13})$$

$$\alpha_s = \alpha_F + S_{H_{x\alpha}} \quad (\text{A.14})$$

$$B_{x\alpha} = (r_{B_{x1}} + r_{B_{x3}} \gamma^2) \cos(\arctan(r_{B_{x2}} \kappa)) \lambda_{x\alpha} \quad (\text{A.15})$$

$$C_{x\alpha} = r_{C_{x1}} \quad (\text{A.16})$$

$$C_{x\alpha} = r_{E_{x1}} + r_{E_{x2}} df_z \quad (\text{A.17})$$

$$S_{H_{x\alpha}} = r_{H_{x1}} \quad (\text{A.18})$$

A.2 Overturning moment M_x

$$\begin{aligned}
M_x = & R_0 F_z \lambda_{M_x} \{ q_{sx1} \lambda_{v_{M_x}} - q_{sx2} \gamma (1 + P_{p_{M_x1}} dp_i) - q_{sx12} \gamma |\gamma| + q_{sx3} \frac{F_y}{F_{z0}} \\
& + q_{sx4} \cos \left[q_{sx4} \arctan \left(\left(q_{sx6} \frac{F_z}{F_{z0}} \right)^2 \right) \right] \cdot \sin \left[q_{sx7} \gamma + q_{sx8} \arctan \left(\left(q_{sx9} \frac{F_y}{F_{z0}} \right)^2 \right) \right] \\
& + q_{sx10} \arctan \left(q_{sx11} \frac{F_z}{F_{z0}} \right) \gamma \} + R_0 F_y \lambda_{M_x} \{ q_{sx13} + q_{sx13} |\gamma| \} \quad (\text{A.19})
\end{aligned}$$

A.3 Rolling resistance moment M_y

$$\begin{aligned}
M_y = & -R_0 F_{z0} \lambda_{M_y} (q_{sy1} + q_{sy2} \frac{F_x}{F_{z0}} + q_{sy3} \left| \frac{V_x}{V_{ref}} \right| + q_{sy4} \left(\frac{V_x}{V_{ref}} \right)^4 + \\
& q_{sy5} \gamma^2 + q_{sy6} \frac{F_z}{F_{z0}} \gamma^2) \left(\frac{F_z}{F_{z0}} \right)^{q_{sy7}} \left(\frac{p}{p_0} \right)^{q_{sy8}} \quad (\text{A.20})
\end{aligned}$$

A.4 Lateral force F_y

$$F_y = G_{y\kappa} F_{yp} + S_{V_{y\kappa}} \quad (\text{A.21})$$

Pure slip:

$$F_{yp} = D_y \sin [C_y \arctan\{B_y \alpha_y - E_y (B_y \alpha_y - \arctan(B_y \alpha_y))\}] + S_{V_y} \quad (\text{A.22})$$

$$\alpha_y = \alpha + S_{Hy} \quad (\text{A.23})$$

$$C_y = P_{Cy1} \lambda_{Cy} \quad (\text{A.24})$$

$$D_y = \mu_y F_z \quad (\text{A.25})$$

$$\mu_y = (p_{Dy1} + p_{Dy2} df_z)(1 - p_{Dy3} \gamma^2)(1 + p_{py3} dp_i + p_{py4} dp_i^2) \lambda_{\mu y} \quad (\text{A.26})$$

$$E_y = (p_{Ey1} + p_{Ey2} df_z)(1 + p_{Ey5} \gamma^2 - (p_{Ey3} + p_{Ey4} \gamma) \text{sgn}(\alpha_y)) \lambda_{Ey} \quad (\text{A.27})$$

$$K_{y\alpha} = (p_{Ky1} F_{z0}(1 + p_{py1} dp_i) \sin \left[p_{Ky4} \arctan \left\{ \frac{F_z}{(p_{Ky2} + p_{Ky5} \gamma^2)(1 + p_{py2} dp_i) F_{z0}} \right\} \right] \\ (1 - p_{Ky3} |\gamma|) \lambda_{Ky\alpha} \quad (\text{A.28})$$

$$K_{y\gamma} = (p_{Ky6} + p_{Ky7} df_z)(1 + p_{py5} dp_i) F_z \lambda_{Ky\gamma} \quad (\text{A.29})$$

$$B_y = \frac{K_{y\alpha}}{C_y D_y} \quad (\text{A.30})$$

$$S_{Hy} = S_{Hy0} + S_{Hy\gamma} \quad (\text{A.31})$$

$$S_{Hy0} = (p_{Hy1} + p_{Hy2} df_z) \lambda_{Hy} \quad (\text{A.32})$$

$$S_{Hy\gamma} = \frac{K_{y\gamma} \gamma - S_{Vy\gamma}}{K_{y\alpha}} \quad (\text{A.33})$$

$$S_{Vy} = S_{Vy0} + S_{Vy\gamma} \quad (\text{A.34})$$

$$S_{Vy0} = (p_{Vy1} + p_{Vy2} df_z) F_z \lambda_{Vy} \lambda_{\mu y} \quad (\text{A.35})$$

$$S_{Vx} = (p_{Vy3} + p_{Vy4} df_z) F_z \gamma \lambda_{Ky\gamma} \lambda_{\mu y} \quad (\text{A.36})$$

Combined lateral correction factor:

$$S_{Vy\kappa} = D_{Vy\kappa} \sin(r_{Vy5} \arctan(r_{Vy6}\kappa)) \lambda_{Vy\kappa} \quad (\text{A.37})$$

$$D_{Vy\kappa} = \mu_y F_z (r_{Vy1} + r_{Vy2} df_z + r_{Vy3} \gamma) \cos(\arctan(r_{Vy4}\alpha)) \quad (\text{A.38})$$

$$G_{y\kappa} = \frac{\cos[C_{y\kappa} \arctan\{B_{y\kappa}\kappa_s - E_{y\kappa}(B_{y\kappa}\kappa_s - \arctan(B_{y\kappa}\kappa_s))\}]}{\cos[C_{y\kappa} \arctan\{B_{y\kappa}S_{Hy\kappa} - E_{y\kappa}(B_{y\kappa}S_{Hy\kappa} - \arctan(B_{y\kappa}S_{Hy\kappa}))\}]} \quad (\text{A.39})$$

$$\kappa_s = \kappa + S_{Hy\kappa} \quad (\text{A.40})$$

$$B_{y\kappa} = (r_{By1} + r_{By4}\gamma^2) \cos(\arctan(r_{By2}(\alpha - r_{By3}))) \lambda_{y\kappa} \quad (\text{A.41})$$

$$C_{y\kappa} = r_{Cy1} \quad (\text{A.42})$$

$$C_{y\kappa} = r_{Ey1} + r_{Ey2} df_z \quad (\text{A.43})$$

$$S_{Hy\kappa} = r_{Hy1} + r_{Hy2} df_z \quad (\text{A.44})$$

A.5 Self-aligning moment M_z

$$M_z = -t \cdot F_{yp0} \cdot G_{y\kappa 0} + M_{zr} + s \cdot F_x \quad (\text{A.45})$$

Where $F_{yp0} \cdot G_{y\kappa 0}$ is the combined slip side force with zero inclination angles $\gamma = 0$.

$$\alpha_t = \alpha + S_{Ht} \quad (\text{A.46})$$

$$S_{Ht} = q_{Hz1} + q_{Hz2} df_z + (q_{Hz3} + q_{Hz4} df_z) \gamma \quad (\text{A.47})$$

$$\alpha_r = \alpha + S_{Hy} + \frac{S_{Vy}}{K_{y\alpha}} \quad (\text{A.48})$$

$$\alpha_{t,eq} = \arctan\left(\sqrt{\tan^2(\alpha_t) + \left(\frac{K_{x\kappa}}{K_{y\alpha}}\right)^2 \kappa^2 \text{sgn}(\alpha_t)}\right) \quad (\text{A.49})$$

$$\alpha_{r,eq} = \arctan\left(\sqrt{\tan^2(\alpha_r) + \left(\frac{K_{x\kappa}}{K_{y\alpha}}\right)^2 \kappa^2 \text{sgn}(\alpha_r)}\right) \quad (\text{A.50})$$

$$s = \left(s_{sz1} + s_{sz1} \left(\frac{F_y}{f_{z0}} \right) + (s_{sz1} + s_{sz1} df_z) \gamma \right) R_0 \lambda_s \quad (\text{A.51})$$

Pneumatic trail t :

$$t = D_t \cos[C_t \arctan\{B_t \alpha_{t,eq} - E_t(B_t \alpha_{t,eq} - \arctan(B_t \alpha_{t,eq}))\}] \cos(\alpha) \quad (\text{A.52})$$

$$B_t = (q_{Bz1} + q_{Bz2} df_z + q_{Bz3} df_z^2) (1 + q_{Bz4} q_{Bz5} |\gamma|) \frac{\lambda_{Ky\alpha}}{\lambda_{\mu_y}} \quad (\text{A.53})$$

$$C_t = q_{Cz1} \quad (\text{A.54})$$

$$D_t = (q_{Dz1} + q_{Dz2}df_z)(1 - q_{Dz1}dp_i)(1 + q_{Dz3}\gamma + q_{Bz4}\gamma^2)F_z \frac{R_0}{F_{z0}} \lambda_t \quad (\text{A.55})$$

$$E_t = (q_{Ez1} + q_{Ez2}df_z + q_{Ez3}df_z^2) \left(1 + (q_{Ez4}q_{Bz5}\gamma) \left(\frac{2}{\pi} \right) \arctan(B_t C_t \alpha_t) \right) \quad (\text{A.56})$$

Residual moment M_{zr} :

$$M_{zr} = D_r \cos [\arctan\{B_r \alpha_{r,eq}\} \cos(\alpha)] \quad (\text{A.57})$$

$$B_r = q_{Bz9} \frac{\lambda_{Ky}\alpha}{\lambda_{\mu y}} + q_{Bz10} B_y C_y \quad (\text{A.58})$$

$$D_r = [(q_{Dz6} + (q_{Dz7}df_z)\lambda_r + ((q_{Dz8} + (q_{Dz9}df_z)(1 - p_{p22}dp_i)\gamma)\lambda_{Kz\gamma} + (q_{Dz10} + (q_{Dz11}df_z)\gamma|\gamma|\lambda_{Kz\gamma})F_z R_0 \lambda_{\mu y} \quad (\text{A.59})$$

A.6 Tire model Matlab code

```

1 function [Fx,Fy,Mx,My,Mz,cx,cy,cz,Rl]=Evaluate_Tyre_Model(inputs,coefficients,
2 scaling_factors,Tot)
3 %% Index
4     %Adimensionalization
5     %Fx calculation
6     %Fy calculation
7     %Mx calculation
8     %My calculation
9     %Mz calculation
10    %Radius calculation (Cancelled)
11    %Contact patch calculation (Cancelled)
12    %Stiffness calculation
13 %% Bibliography
14    % Using UPC ecoRacing Pacejka Model extractet from the paper:
15    % [4] An improved Magic Formula/Swift tyre model that can handle in ation
16    % pressure changes.
17    % In Vehicle System Dynamics, volume 48, pages 337–352, 2010.
18 %% Adimensionalization
19    dFz=(inputs(1)-coefficients(1))/coefficients(1);
20    dPi=(inputs(6)-coefficients(4))/coefficients(4);
21 %% Fx calculation
22    %Pure slip (34–42)
23    Kxk=(coefficients(40)+coefficients(41)*dFz)*exp(coefficients(42)*dFz)*(1+
24    coefficients(47)*dPi+coefficients(48)*dPi^2)*inputs(1)*scaling_factors(5);
25    SHx=(coefficients(43)+coefficients(44)*dFz)*scaling_factors(11);
26    SVx=(coefficients(45)+coefficients(46)*dFz)*inputs(1)*scaling_factors(2)*
27    scaling_factors(13);
28    kx=inputs(2)+SHx;
29    Mux=(coefficients(33)+coefficients(34)*dFz)*(1-coefficients(35)*inputs(4)^2)
30    *(1+coefficients(49)*dPi+coefficients(50)*dPi^2)*scaling_factors(2);
31    Cx=coefficients(32)*scaling_factors(7);
32    Dx=Mux*inputs(1);
33    Ex=(coefficients(36)+coefficients(37)*dFz+coefficients(38)*dFz^2)*(1-
34    coefficients(39)*sign(inputs(2)))*scaling_factors(9);
35    Bx=Kxk/Cx/Dx;
36
37    if Ex>1
38        Error=['Error in the value of E: Ex=' Ex]; %%ok<NASGU>
39        disp('Error')
40        display(inputs)
41        clear Error
42    end
43
44    %Combined slip (43–48)
45    SHxa=coefficients(100);
46    SAs=inputs(3)+SHxa;
47    Bxa=(coefficients(96)+coefficients(98)*inputs(4)^2)*cos(atan(coefficients(97)
48    *inputs(2)))*scaling_factors(19);
49    Cxa=coefficients(99);
50    Exa=coefficients(101)+coefficients(102)*dFz;

```

```

46     Gxa=cos(Cxa*atan(Bxa*SAs-Exa*(Bxa*SAs-atan(Bxa*SAs)))/cos(Cxa*atan(Bxa*SHxa-
47     Exa*(Bxa*SHxa-atan(Bxa*SHxa))));
48
49     if Exa>1
50         Error=['Error in the value of E: Exa=' Exa]; %%ok<NASGU>
51         disp('Error')
52         display(inputs)
53         clear Error
54     end
55
56     %%Pacejka formula (33)
57     Fx=(Dx*sin(Cx*atan(Bx*kx-Ex*(Bx*kx-atan(Bx*kx))))+SVx)*Gxa;
58     %% Fy calculation
59     %%Pure slip (53-66)
60     Kya=coefficients(14)*coefficients(1)*(1+coefficients(27)*dPi)*sin(
61     coefficients(17)*atan(inputs(1)/...
62     ((coefficients(15)+coefficients(18)*inputs(4)^2)*(1+coefficients(28)*dPi
63     *coefficients(1))))*(1-coefficients(16)*abs(inputs(4))*scaling_factors(6);
64     Kyia=(coefficients(19)+coefficients(20)*dFz)*(1+coefficients(31)*dPi)*inputs
65     (1)*scaling_factors(15);
66     SVy0=inputs(1)*(coefficients(23)+coefficients(24)*dFz)*scaling_factors(3)*
67     scaling_factors(14);
68     SVyia=inputs(1)*(coefficients(25)+coefficients(26)*dFz)*inputs(4)*
69     scaling_factors(3)*scaling_factors(15);
70     SHy0=(coefficients(21)+coefficients(22)*dFz)*scaling_factors(12);
71     SHyia=(Kyia*inputs(4)-SVyia)/Kya;
72     SHy=SHy0+SHyia;
73     SVy=SVy0+SVyia;
74     SAy=inputs(3)+SHy;
75     Muy=(coefficients(6)+coefficients(7)*dFz)*(1-coefficients(8)*inputs(4)^2)*(1+
76     coefficients(29)*dPi+coefficients(30)*dPi^2)*scaling_factors(3);
77     Cy=coefficients(5)*scaling_factors(8);
78     Dy=Muy*inputs(1);
79     Ey=(coefficients(9)+coefficients(10)*dFz)*(1+coefficients(13)*inputs(4)^2-(
80     coefficients(11)+coefficients(12)*inputs(4))*sign(SAy))*scaling_factors(10);
81     By=Kya/Cy/Dy;
82
83     if Ey>1
84         Error=['Error in the value of E: Ey=' Ey]; %%ok<NASGU>
85         disp('Error')
86         display(inputs)
87         clear Error
88     end
89
90     %%Combined slip (67-74)
91     SHyk=coefficients(88)+coefficients(89)*dFz;
92     ks=inputs(2)+SHyk;
93     Byk=(coefficients(81)+coefficients(84)*inputs(4)^2)*cos(atan(coefficients(82)
94     *(inputs(3)-coefficients(83))))*scaling_factors(20);
95     Cyk=coefficients(85);
96     Eyk=coefficients(86)+coefficients(87)*dFz;
97     DVyk=Muy*inputs(1)*(coefficients(90)+coefficients(91)*dFz+coefficients(92)*
98     inputs(4))*cos(atan(coefficients(93)*inputs(3)));
99     SVyk=DVy*sin(coefficients(94)*atan(coefficients(95)*inputs(2)))*
100     scaling_factors(21);

```

```

90
91 Gyk=cos (Cyk*atan (Byk*ks-Eyk*(Byk*ks-atan (Byk*ks)))/cos (Cyk*atan (Byk*SHyk-Eyk
92 *(Byk*SHyk-atan (Byk*SHyk))));
93
94 if Eyk>1
95     Error=['Error in the value of E: Eyk=' Eyk]; %%ok<NASGU>
96     disp ('Error ')
97     display (inputs)
98     clear Error
99
100 end
101
102 %%Pacejka formula (51-52)
103 Fy=Gyk*(Dy*sin (Cy*atan (By*SAy-Ey*(By*SAy-atan (By*SAy))))+SVy)+SVyk;
104
105 %% Mx calculation (49)
106 Mx=coefficients (2)*inputs (1)*scaling_factors (24)*(coefficients (107)*
107 scaling_factors (26)-coefficients (108)*inputs (4)*(1+coefficients (121)*dPi)...
108 -coefficients (118)*inputs (4)*abs (inputs (4))+coefficients (109)*Fy/
109 coefficients (1)...
110 +coefficients (110)*cos (coefficients (111)*atan ((coefficients (112)*inputs (1)
111 /coefficients (1))^2))*sin (coefficients (113)*inputs (4)...
112 +coefficients (114)*atan (coefficients (115)*Fy/coefficients (1))+
113 coefficients (116)*atan (coefficients (117)*inputs (1)/coefficients (1))*inputs (4)
114 )...
115 +coefficients (2)*Fy*scaling_factors (24)*(coefficients (119)+coefficients
116 (120)*abs (inputs (4)));
117
118 %% My calculation (50)
119 My=-coefficients (2)*coefficients (1)*scaling_factors (25)*(coefficients (122)+
120 coefficients (123)*Fx/coefficients (1)...
121 +coefficients (124)*abs (inputs (5)/coefficients (3))+coefficients (125)*
122 (inputs (5)/coefficients (3))^4+coefficients (126)*inputs (4)^2 ...
123 +coefficients (127)*inputs (1)/coefficients (1)*inputs (4)^2*(inputs (1)/
124 coefficients (1))^coefficients (128)*(inputs (6)/coefficients (4))^coefficients
125 (129);
126
127 %% Mz calculation
128 %%Combined slip force with zero inclination angle Fy@IA=0
129 if inputs (4)==0
130     Fy0=Fy;
131 else
132     %%Pure slip (53-66)
133     Kya=coefficients (14)*coefficients (1)*(1+coefficients (27)*dPi)*...
134         sin (coefficients (17)*atan (inputs (1)/(coefficients (15)*(1+coefficients
135 (28)*dPi)*coefficients (1))))*scaling_factors (6);
136     SVy=inputs (1)*(coefficients (23)+coefficients (24)*dFz)*scaling_factors (3)*
137 scaling_factors (14);
138     SHy=(coefficients (21)+coefficients (22)*dFz)*scaling_factors (12);
139     SAy=inputs (3)+SHy;
140     Muy=(coefficients (6)+coefficients (7)*dFz)*(1+coefficients (29)*dPi+
141 coefficients (30)*dPi^2)*scaling_factors (3);
142     Cy=coefficients (5)*scaling_factors (8);
143     Dy=Muy*inputs (1);
144     Ey=(coefficients (9)+coefficients (10)*dFz)*(1-coefficients (11)*sign (SAy))*
145 scaling_factors (10);

```

```

130     By=Kya/Cy/Dy;
131
132     if Ey>1
133         Error=['Error in the value of E: Ey=' Ey]; %%ok<NASGU>
134         disp('Error')
135         display(inputs)
136         clear Error
137     end
138
139     %Combined slip (67-74)
140     SHyk=coefficients(88)+coefficients(89)*dFz;
141     ks=inputs(2)+SHyk;
142     Byk=coefficients(81)*cos(atan(coefficients(82)*(inputs(3)-coefficients
(83))))*scaling_factors(20);
143     Cyk=coefficients(85);
144     Eyk=coefficients(86)+coefficients(87)*dFz;
145     DVyk=Muy*inputs(1)*(coefficients(90)+coefficients(91)*dFz)*cos(atan(
coefficients(93)*inputs(3)));
146     SVyk=DVy*sin(coefficients(94)*atan(coefficients(95)*inputs(2)))*
scaling_factors(21);
147
148     Gyk=cos(Cyk*atan(Byk*ks-Eyk*(Byk*ks-atan(Byk*ks)))/cos(Cyk*atan(Byk*SHyk
-Eyk*(Byk*SHyk-atan(Byk*SHyk))));
149
150     if Eyk>1
151         Error=['Error in the value of E: Eyk0=' Eyk]; %%ok<NASGU>
152         disp('Error')
153         display(inputs)
154         clear Error
155     end
156
157     %Pacejka formula (51-52)
158     Fy0=Gyk*(Dy*sin(Cy*atan(By*SAy-Ey*(By*SAy-atan(By*SAy))))+SVy)+SVyk;
159 end
160
161 %Equivalent slip (76-81)
162 SHt=coefficients(75)+coefficients(76)*dFz+(coefficients(77)+coefficients(78)*
dFz)*inputs(4);
163 SAt=inputs(3)+SHt;
164 SAR=inputs(3)+SHy+SVy/Kyia;
165 SAteq=atan(sqrt((tan(SAt))^2+(Kxk/Kya)^2*inputs(2)^2))*sign(SAt);
166 SAreq=atan(sqrt((tan(SAR))^2+(Kxk/Kya)^2*inputs(2)^2))*sign(SAR);
167
168 %Pneumatic scrub (82)
169 s=(coefficients(103)+coefficients(104)*(Fy/coefficients(1)))+(coefficients
(105)+coefficients(106)*dFz)*inputs(4)*coefficients(2)*scaling_factors(22);
170
171 %Pneumatic trail (83-87)
172 Bt=(coefficients(51)+coefficients(52)*dFz+coefficients(53)*dFz^2)*(1+
coefficients(54)+coefficients(55)*abs(inputs(4)))*scaling_factors(15)/
scaling_factors(3);
173 Ct=coefficients(59);
174 Dt=(coefficients(60)+coefficients(61)*dFz)*(1-coefficients(79)*dPi)*(1+
coefficients(62)*inputs(4)+coefficients(63)*inputs(4)^2)*inputs(1)*
coefficients(2)/...

```

```

175     coefficients(1)*scaling_factors(17);
176     Et=(coefficients(70)+coefficients(71)*dFz+coefficients(72)*dFz^2)*(1+(
coefficients(73)+coefficients(74)*inputs(4))*2/pi*atan(Bt*Ct*SA_t));
177     t=Dt*cos(Ct*atan(Bt*SA_teq-Et*(Bt*SA_teq-atan(Bt*SA_teq))))*cos(inputs(3));
178
179     %%Residual moment (88-90)
180     Br=coefficients(57)*scaling_factors(15)/scaling_factors(3)+coefficients(58)*
By*Cy;
181     Dr=((coefficients(64)+coefficients(65)*dFz)*scaling_factors(18)+(coefficients
(66)+coefficients(67)*dFz)*(1-coefficients(80)*dPi)*inputs(4)...
182     *scaling_factors(16)+(coefficients(68)+coefficients(69)*dFz)*inputs(4)*
abs(inputs(4))*scaling_factors(16))*inputs(1)*coefficients(2)*scaling_factors
(3);
183     Mzr=Dr*cos(atan(Br*SAreq))*cos(inputs(3));
184
185     %%Pacejka formula (75)
186     Mz=-t*Fy0+Mzr+s*Fx;
187     cx=0;
188     cy=0;
189     cz=0;
190     Rl=0;
191     if Tot==1
192         %% Radius calculation
193         c=coefficients(1)/coefficients(2)*sqrt(coefficients(133)^2+4*coefficients
(134))*(1+coefficients(138)*dPi); %Vertical stiffness [N/m] used in (5)
194         w=(1+inputs(2))*inputs(5)/coefficients(2); %Initial point of angular
speed [rad/s] (6) supposing Re=R0
195         for i=1:3 %Resolving of Rfr, Re and w
196             wo=w;
197             Rfr=coefficients(2)*(coefficients(130)+coefficients(131)*(wo*
coefficients(2)/coefficients(3))^2); %Free tyre radius [m] (1)
198             Re=Rfr-coefficients(1)/c*(coefficients(141)*atan(coefficients(142)*
inputs(1)/coefficients(1))+coefficients(143)*inputs(1)/coefficients(1));...
199             %Effective radius [m] (7)
200             w=(1+inputs(2))*inputs(5)/Re; %Angular speed [rad/s] (6)
201             if abs(w-wo)<0.1
202                 break;
203             end
204         end
205         if abs(w-wo)>0.1
206             Error=['Error in the convergence of the agular velocity. Last
iteration error of ',abs(w-wo),' rad/s.'];
207             disp(Error);
208             display(inputs);
209             clear Error
210         end
211
212         k3=(1+coefficients(132)*coefficients(2)/coefficients(3)*abs(w)-(
coefficients(136)*Fx/coefficients(1))^2-(coefficients(137)*Fy/coefficients(1)
)^2)...
213         *(1+coefficients(138)*dPi)*coefficients(1); %Terms part of (3)
214
215         deflection=(-coefficients(133)/coefficients(2)+sqrt(coefficients(133)^2/
coefficients(2)^2+4*coefficients(134)/coefficients(2)^2*inputs(1)/k3))...

```

```

216         /(2*coefficients(134)/coefficients(2)^2); %Deflection [m]
    resulting of solve (3)
217
218     Rl=min(Rfr ,Rfr-deflection); %Loaded radius [m] (2)
219 %% Contact patch calculation
220 %     a=coefficients(2)*(coefficients(145)*inputs(1)/c/coefficients(2)+
coefficients(144)*sqrt(inputs(1)/c/coefficients(2)));...
221 %     %Half of the contact patch length [m] (9)
222 %     b=coefficients(146)*(coefficients(148)*inputs(1)/c/coefficients(2)+
coefficients(147)*(inputs(1)/c/coefficients(2))^(1/3));...
223 %     %Half of the contact patch width [m] (10)
224 %% Stiffness calculation
225     cx=coefficients(153)*(1+coefficients(154)*dFz+coefficients(155)*dFz^2)
*(1+coefficients(156)*dPi); %Longitudinal stiffness [N/m] (17)
226     cy=coefficients(149)*(1+coefficients(150)*dFz+coefficients(151)*dFz^2)
*(1+coefficients(152)*dPi); %Lateral stiffness [N/m] (18)
227     cz=k3*(coefficients(133)/coefficients(2)+2*coefficients(134)/coefficients
(2)^2*deflection); %Vertical stiffness [N/m] resulting of dFz/dRl
(3)
228 end
229 end

```


Appendix B

Simulink vehicle model

In this appendix, Simulink vehicle model will be shown. Starting from the general overview of the Simulink blocks and, finally, entering in detail in each function of the model.

B.1 Simulink blocks and connections

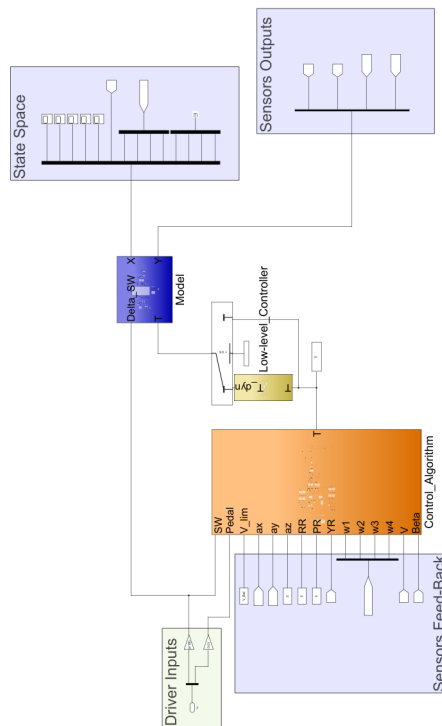


FIGURE B.1: Simulink model general overview.

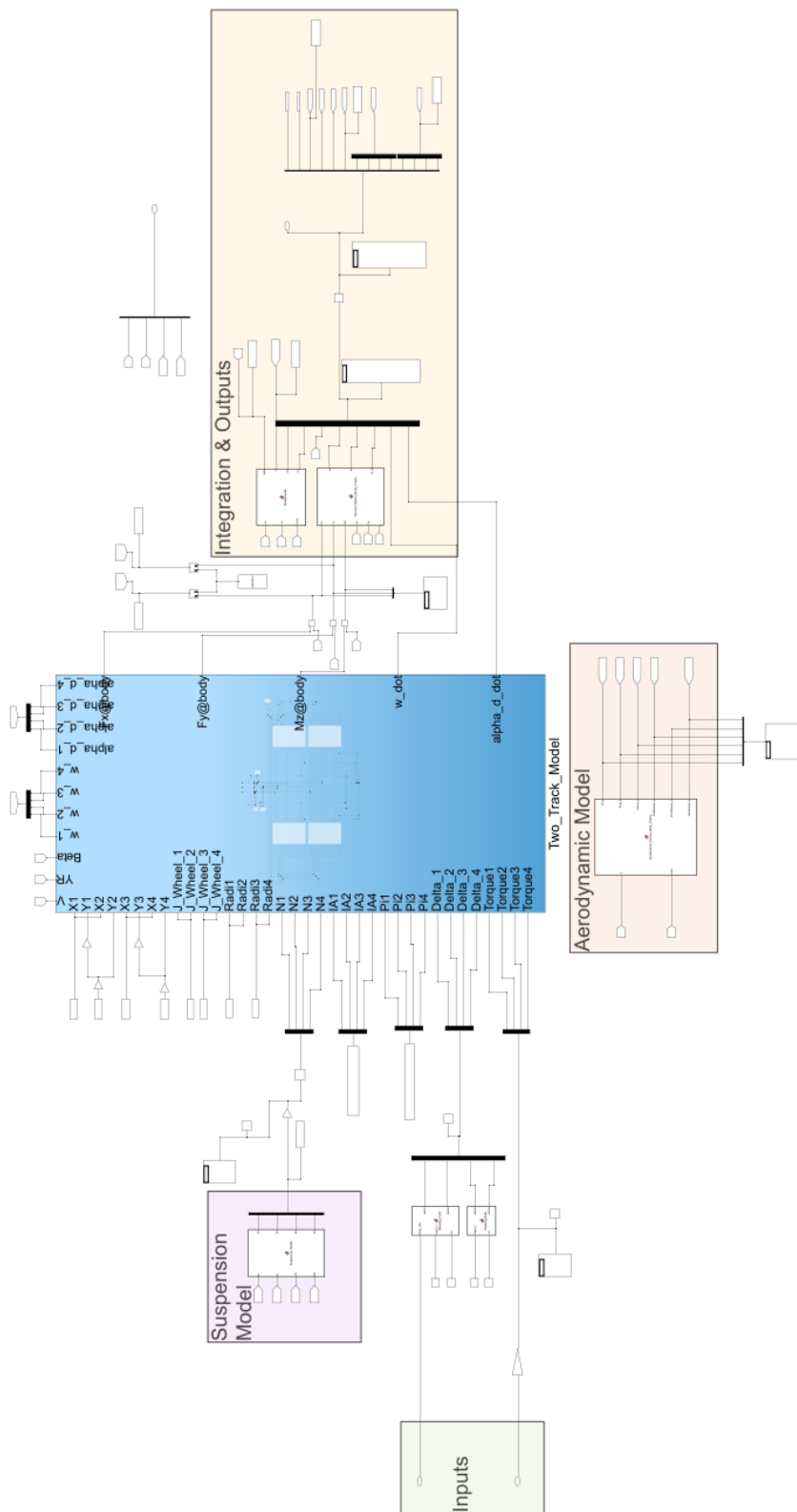


FIGURE B.2: Simulink vehicle physical model overview.

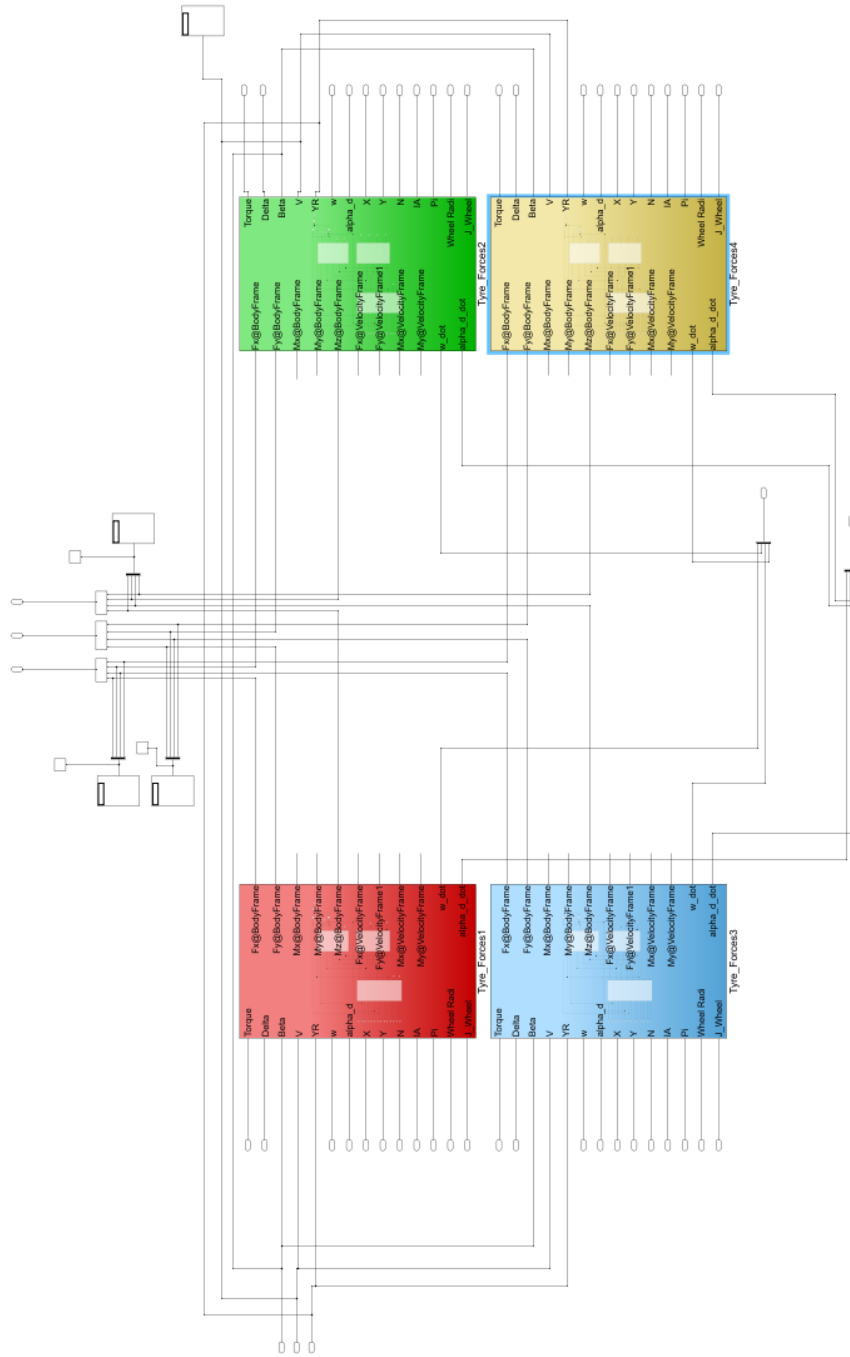


FIGURE B.3: Simulink two-track model overview.

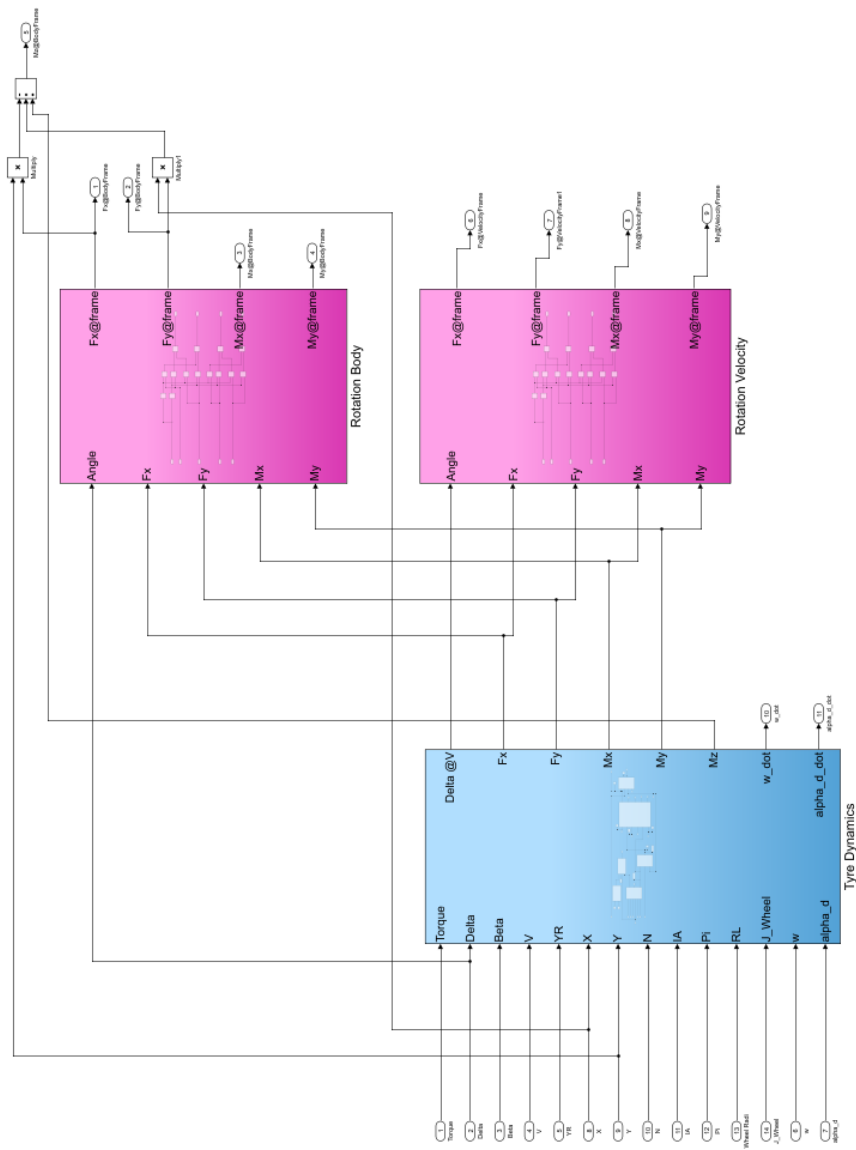


FIGURE B.4: Simulink tire dynamics and reference system projection.

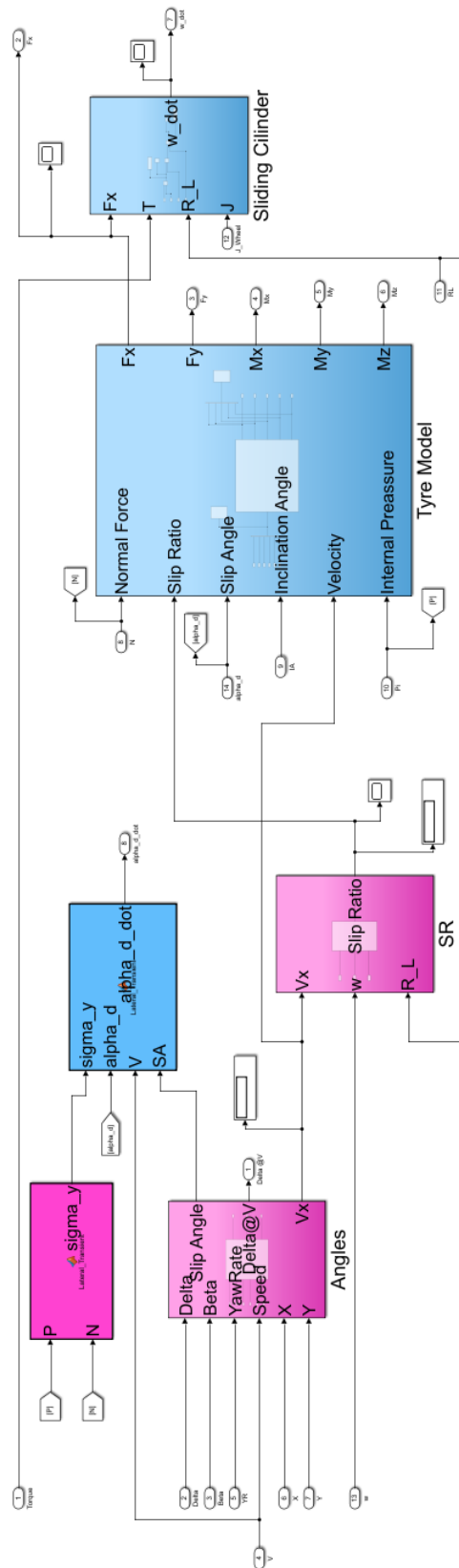


FIGURE B.5: Simulink tire dynamics and Magic Formula 6.1 tire model.

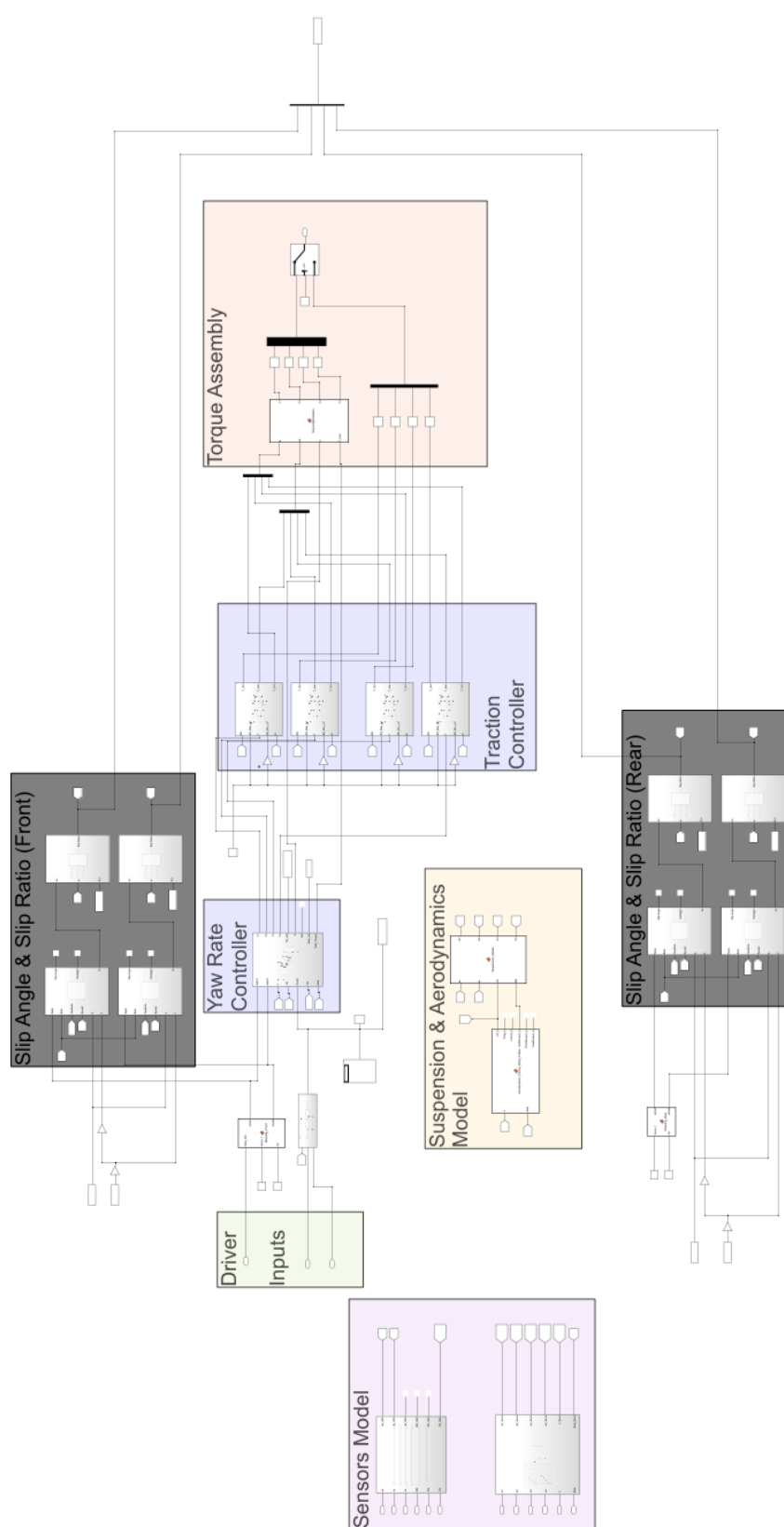


FIGURE B.6: Simulink control algorithm general overview.

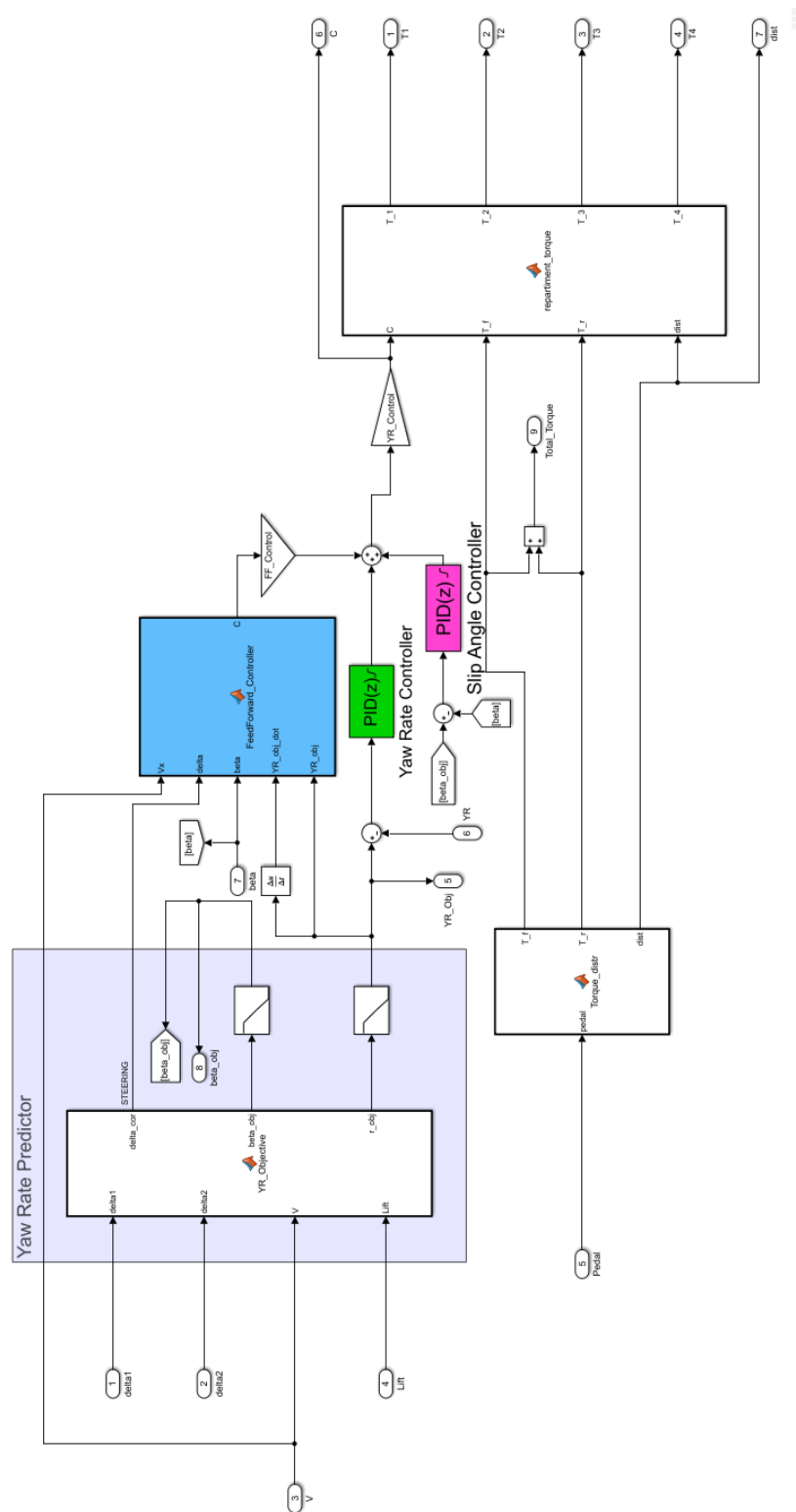


FIGURE B.7: Simulink yaw rate control algorithm general detailed.

B.2 Matlab and Simulink codes

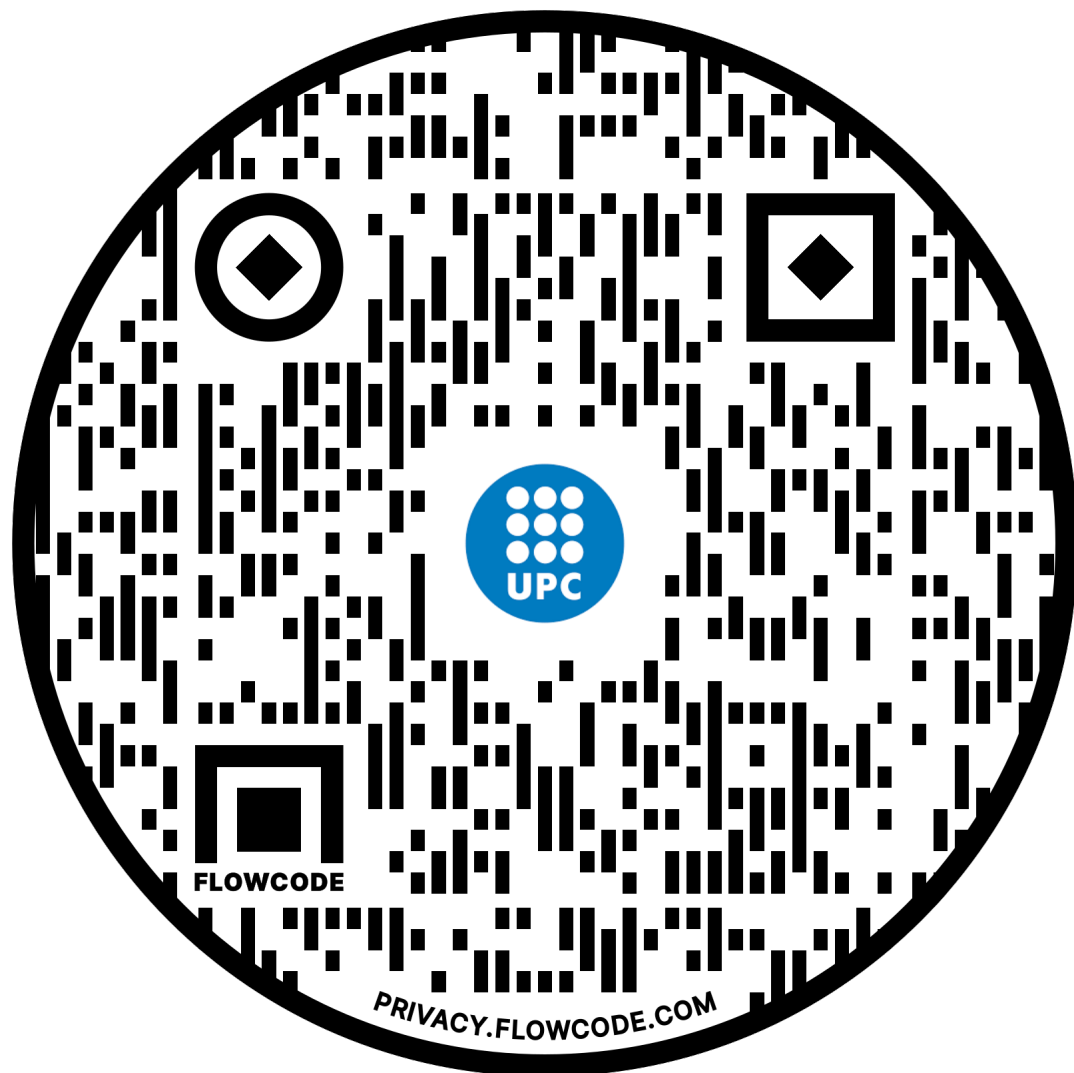


FIGURE B.8: QR that give access to the Matlab and Simulink codes.

References

- [1] I. J. M. Besselink, A. J. C. Schmeitz, and H. B. Pacejka. An improved Magic Formula/Swift tyre model that can handle inflation pressure changes. In *Vehicle System Dynamics*, volume 48, pages 337–352, 2010. ISBN 0042-3114. doi: 10.1080/00423111003748088.

