

1 Building-integrated agriculture: are we shifting environmental
2 impacts? An environmental and structural improvement
3 assessment of greenhouses structures.

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22 **Abstract:**

23 Urban and building systems are awash with materials. The incorporation of green
24 infrastructure such as rooftop greenhouses (RTG) has the potential to contribute to buildings
25 and cities circularity but, in turn, its higher sophistication compared to conventional
26 agriculture (CA) could lead to a shift of environmental impacts. One of the key elements for
27 greenhouse building-integrated agriculture (BIA) and CA to achieve high levels of
28 environmental performance is their structural design, which largely impacts the economic
29 and environmental life-cycle costs. In this context, this study assessed RTGs material and
30 energy flows and its environmental burdens at the structural level ($m^2 \cdot y$) within life cycle
31 assessment (LCA) based on a case study in Barcelona. An improvement structural assessment
32 following the European standards allowed to identify key design elements to minimize RTGs
33 environmental impacts within improvement scenarios. The assesment revealed that the steel
34 structure in the BAU scenario caused between 31.5 to 67.3% of the impact categories
35 analyzed, followed by the polycarbonate covering material (21.8 - 45.9%). The key design
36 factors responsible for such greenhouse structural design were the ground height, ventilation
37 design, integration with the building and its urban location. The improvement scenarios
38 allowed to compensate for additional steel inputs up to 35.9% and decrease environmental
39 impacts that might occur in the BIA context by 24.1%. The assessment also revealed that the
40 urban environment does not imply shifting environmental impacts per se, as greenhouse BIA
41 structures can take profit of its advantageous characteristics or be compensated by optimized
42 greenhouse structures.

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45 **Keywords**

46 Material flow analysis, resource use-efficiency, industrial ecology, structural modelling, urban
47 agriculture, urban metabolism.

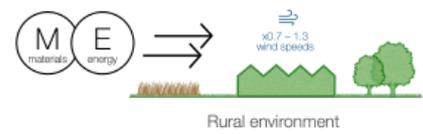
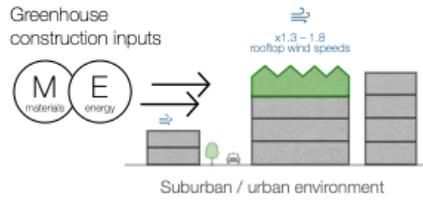
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Graphical abstract

51



SD - BAU Scenario

- x1.6** kg steel
- x7.2 - 8.1** kWh to build

- x2.4 - 5.9** kg concrete
- x0.3 - 0.5** GH lifetime

S1/2 - Optimized greenhouse scenarios



S1/ Suburban S2/ Urban

↓ **27.8%** ↓ **35.9%** kg steel

↓ **9.6%** ↓ **12.4%** CO₂ eq.

- ✓ Identify construction **resource flows**
- ✓ **Identify design factors** to minimize env. impacts
- ✓ Avoid **environmental shifting** from CA to BIA
- ✓ Increase **resource-use** efficiency of greenhouses

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87 **1. Introduction**

88 Environmental impacts derived from urban systems are one of the main concerns in
89 contemporary societies (IPCC, 2014); these impacts are expected to grow due to the 68%
90 increase on the world population predicted for 2050 (Population Division, 2018). Despite
91 consuming a vast amount of resources, cities offer unique opportunities for circular-resource
92 urban systems, contributing to sustainable development promotion. An example is urban
93 agriculture, which offers an opportunity to add value to urban waste resources reusing them
94 as inputs on crop production thanks to the circular management of urban resource flows
95 (Grard et al., 2015). That allows to decrease urban resource needs while contributing to key
96 societal challenges such us food security in a growing population context.

97
98 Different forms of Building-Integrated Agriculture (BIA) have been addressed, including
99 urban gardens, allotments and rooftop farming which provide diferent direct and indirect
100 resource savings. Among them, building-integrated rooftop greenhouses (iRTGs, also referred
101 as RTGs) are one of the most sophisticated BIA structures that in turn, offer major benefits.
102 For instance, they improve energy efficiency in buildings (Specht et al., 2013) by taking
103 advantage of greenhouse insulation (Muñoz-Liesa et al., 2020a; Nadal et al., 2017b) and by
104 utilizing building waste energy flows with high humidity content and occupant-generated
105 CO₂ to promote plant growth (Sanyé-Mengual et al., 2014). By these means, iRTGs enhance
106 crop productivity that could provide local communities with fresh food while promoting
107 more efficient food-supply chains (Nadal et al., 2017a). In turn, iRTGs as well as other
108 building-integrated agriculture (BIA) forms are nature-based solutions that bring agricultural
109 ecosystem services to the urban form (Artmann and Sartison, 2018), contributing to the
110 overall goal of decarbonizing the economy by improving land and resource efficiency within
111 urban systems (European Union, 2018).

112
113 However, integrating urban space into new forms of agriculture usually involves higher
114 complexity in agricultural technologies and facilities compared to conventional agriculture.
115 This not only may represent a social barrier and an issue of major concern for stakeholders
116 (Specht and Sanyé-Mengual, 2017), but also a technical, economic and an environmental
117 constrain due to the life cycle stages involved in the greenhouse construction, worsen by

118 building accessibility limitations (Cerón-Palma et al., 2012; Sanyé-Mengual et al., 2015a;
119 Specht and Sanyé-Mengual, 2017).

120 Environmental impacts derived from greenhouse structures largely contribute to the overall
121 food production impacts in both conventional and rooftop unheated greenhouses (Muñoz et
122 al., 2008; Ruffi-Salís et al., 2020a; Sanjuan-Delmás et al., 2018; Sanyé-Mengual et al., 2015c).
123 Ruffi-Salís and collaborators (Ruffi-Salís et al., 2020a) found that the structure of an iRTG
124 located in the Barcelona area, accounted for 42-61% of the climate change impacts when
125 assessing the life cycle environmental impacts of different crops. Similar impacts of 40% and
126 78% have been described for European conventional greenhouses (Torrellas et al., 2012) and
127 a Venlo Dutch greenhouse (Anton et al., 2012) respectively. Thus, their impacts can be
128 compared to other operational resource flows, which are commonly the greatest impact in
129 terms of life cycle assessment of food production in both conventional and rooftop
130 greenhouses (Vadiee and Martin, 2013; van Beveren et al., 2015; Wallgren and Höjer, 2009).

131
132 In rooftop farming, the structural loads are limited to the existing roof carrying capacity
133 (Castleton et al., 2010; Toboso Chavero et al., 2018), which varies depending on building age
134 and usage as well as the regulatory framework (Caputo et al., 2017). Moreover, BIA structural
135 design and covering material selection is limited by technical, legal and fire-safety
136 requirements, among others, stated in different building codes (Sanyé-Mengual et al., 2015c)
137 and directly affects greenhouse climate behavior and thus building energy needs (Muñoz-
138 Liesa et al., 2020b). Thus, BIA normally addresses multiple building constrains which are
139 translated into greater construction inputs, making them more difficult and expensive to build
140 (Ackerman et al., 2011; Benis et al., 2018). At the same time, BIA as well as other building
141 innovative technologies are needed to boost resource circularity that can support the
142 decarbonization of the economy (European Union, 2018). Accordingly, BIA pilot
143 implementations can be very useful to prove increased efficiency in food production
144 (Sanjuan-Delmás et al., 2018).

145
146 The ICTA building is an example of BIA implementation in the south of Europe hosting an
147 iRTG. The ICTA-iRTG system represents a good example of a well characterized pilot study,
148 although an in-depth analysis of structural environmental impacts is lacking.

149 Beyond the ICTA-iRTG, current methodologies that assess the potential of urban agriculture
150 does not consider structural aspects and its suitability for different urban environments yet
151 (Benis and Ferrão, 2017; Nadal et al., 2017a; 2016; Sanyé-Mengual et al., 2015b; Toboso
152 Chavero et al., 2018). Hence, there is a research gap in assessing urban greenhouse structures
153 and its environmental performance under different urban contexts (Goldstein et al., 2016;
154 Specht et al., 2013).

155
156 The construction industry, including buildings and BIA, are increasingly being designed to
157 meet current decarbonization targets and this is steeply gaining attention in literature
158 (Hossain et al., 2020). Structural designers are therefore rising their interest in lightweight
159 structures, which, together with membrane solutions or more flexible structures have the
160 potential to increase material efficiency and reduce environmentally-derived construction
161 impacts compared to conventional rigid and massive structures (Monticelli et al., 2017). In
162 BIA, cost-effective solutions with lightweight materials and techniques should also be further
163 investigated (Specht et al., 2013) In turn, building materials logistics and construction phase
164 could be further improved and simplified, especially when dealing with rooftop greenhouses.
165 Structural loads associated to building rooftop farming may also benefit from this optimization
166 when the existing roof carrying capacity represents a building constrain.

167
168 Greenhouses and buildings will necessarily tend to zero or nearly-zero emissions systems in
169 the near future (European Union, 2018; Montero et al., 2010). Hence, the embodied impacts
170 on urban assets will become increasingly important to effectively achieve a low-carbon
171 development. Material usage in the built environment is gaining concern and is listed as a
172 high relevance issue in the 5th IPCC report on climate change (IPCC, 2014). Therefore, Life
173 Cycle Assessment (LCA) will likely become more important in the future when assessing
174 sustainability issues. Among them, several studies in urban agriculture highlight the need to
175 adopt LCA in the analysis (Mok et al., 2013; Specht et al., 2013) to quantify the environmental
176 burdens and explore potential reductions of food production (Sanyé-Mengual et al., 2015c;
177 2012). Finally, this will avoid environmental shifting of impacts that could derive from
178 efficient UA resource flows to BIA structures such as iRTGs.

179

180 1.1 Objectives of the study

181 This study aims to quantify input construction materials and energy flows of iRTG structures
182 in the European context based on the ICTA-iRTG case study. By understanding how material
183 flows in the urban environments in comparison with rural environments, more resource-
184 efficient greenhouse structures will be designed in different improvement scenarios. In order
185 to do so, key design factors that affect such structures will be identified in order to minimize
186 greenhouse environmental impacts.

187
188 The outcome of this assessment has been used to compare them with a standard conventional
189 greenhouse within their related environmental impacts and quantify the potential
190 environmental problem shifting from conventional to BIA in all scenarios assessed. Finally,
191 this data is used to generalize and give guidelines to apply the obtained results across Europe,
192 improving greenhouse structures and BIA resource-use efficiency.

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194 **2. Methods**

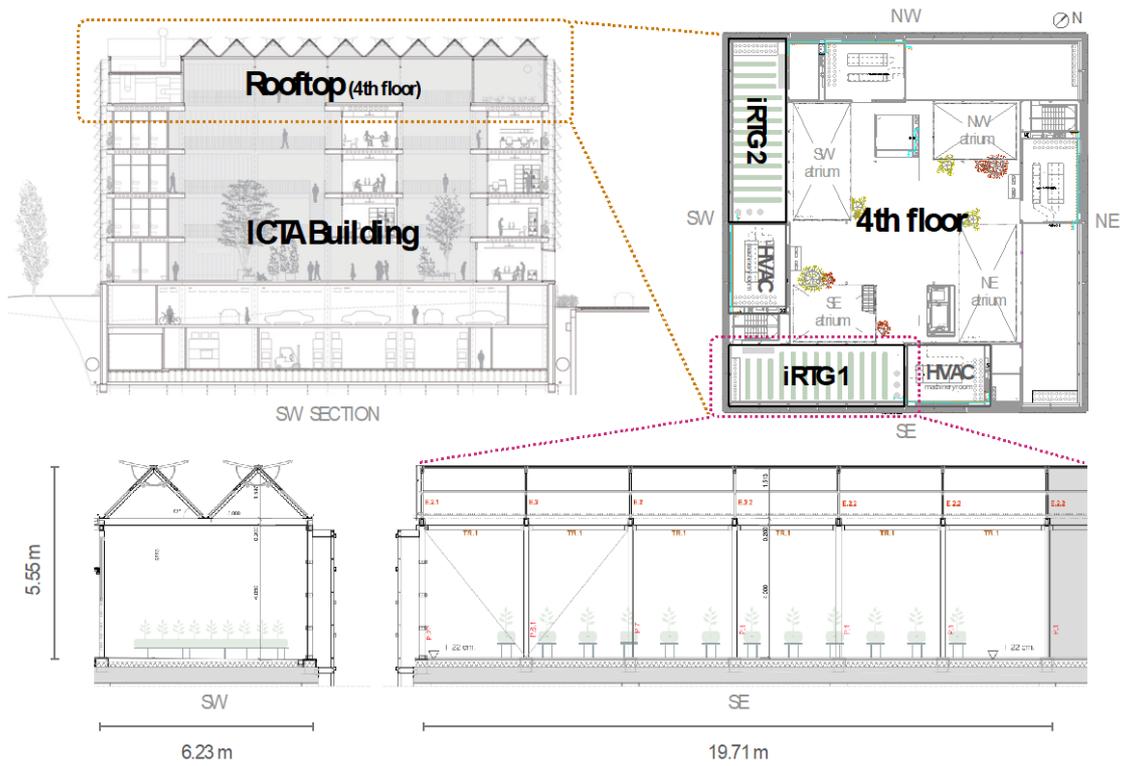
195 2.1 The ICTA-iRTG case study

196 The ICTA-iRTG system is located in the research Institute of Environmental Science and
197 Technology (ICTA) in the Universitat Autònoma de Barcelona campus (Barcelona
198 Metropolitan area). The building is designed in all its life cycle stages -from selected
199 construction materials to its later deconstruction- to improve building sustainability. An
200 essential feature of the building design is the bioclimatic envelope made out of a steel
201 structure and a corrugated polycarbonate covering the inner spaces of the building and
202 forming a double skin façade that autoregulates its climate with automatic-window openings.
203 Such mechanism is imported from the greenhouse industry and is also used in the rooftop,
204 which houses four integrated rooftop greenhouses. Four atriums (see Figure 1) enhance these
205 passive bioclimatic strategies and are combined with smart building controls. Both systems
206 enable to monitor and adjust the iRTG and the building internal climate. Additionally, a
207 rainwater harvesting system combined with a separate sewer allow to reduce the building
208 water demand and consumption. Hence, building design and assets try to favor the best use
209 of on-site available resources by dynamically interconnect with them.

210
211 The ICTA rooftop is based on a Venlo greenhouse structure replicated over the rooftop space
212 (measuring 1508.4 m² of gross area). Venlo greenhouses are very versatile structures and
213 widely used in Northern Europe. The iRTG here assessed is located in the SE façade, where a
214 hydroponic tomato among other crop cycles are grown (see Figure 1). Each iRTG has a
215 serviceable area for growing crops of 84.34 m² from the total net area of 122.8 m² and 125 m²
216 when counting the gross area including all pillars and the whole steel structure. The
217 greenhouse high up to the top of the two ridges of the roof measure 5.55 m high including
218 the truss spacing (4.05 m of net high up to the beam level) and allow 6.23m of span width.
219 The three external sides of the greenhouse are covered with a 0.8 mm corrugate
220 polycarbonate, which envelopes a total area of 243.66 m², including the two exterior façades
221 in each iRTG (98.99 m²) and the Venlo roof (144.67 m²). The internal sides of the greenhouse
222 facing the building (NW, SW) are a wood building wall and a thermal polyethylene climate
223 screen that can isolate the greenhouse from the rest of the rooftop area when needed.

224

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226

227

228

Figure 1. Cross section of ICTA building and iRTG 1 location and geometry in the 4th floor.

229 2.2 Structural assessment

230 The Venlo main structure of the iRTG is made out of tubular vertical pillars of galvanized steel
231 designed to support steel trusses that constitute the two chapels of the greenhouse (Figure 1).
232 These modular structure is the basis of a Venlo greenhouse, normally replicated throughout the
233 available space with common gutters, forming a range as it is in the ICTA rooftop (Figure 1).
234 Pillars are welded to steel plates anchored in the building concrete slab while the polycarbonate
235 covering is supported with auxiliary steel elements and rubber supports that hold the covering
236 material with the steel frame. Besides, the steel frame also supports 4 one-side window frames
237 and its automatic-opening mechanisms located in the rooftop and in each façade (Figure 2). The
238 iRTG SE and SW façades are also structurally connected with the double skin façade steel frame,
239 though this frame is excluded in both structural and environmental assessments. Isolating the
240 greenhouse from the rest of the building penalizes the iRTG structure as it does not consider
241 any other building elements that could aid supporting the iRTG environmental loads. However,
242 it allows to optimize a standard module of a Venlo greenhouse that can be applied to almost any
243 rooftop conditions.

244
245 The ICTA building and the rooftop steel structure are subjected to the legal requirements
246 established to comply with the Spanish Technical Code of Edification (CTE, 2009) which is in
247 line with Eurocode 1 and EN 13031-1 . Moreover, fire safety laws (RD 2267/2004 and Law
248 3/2010, BOE 2004 & 2010) are also taken into account, while the structural loads considered are
249 also in accordance with the CS2 service class established by the CTE (see supplementary
250 material for details). Wind loads have been considered on top of the iRTG ridge at 28m high
251 (according to Eurocode guidelines for a Venlo roof type) and have been subdivided into pressure
252 and suction forces to structurally assess the greenhouse. Suction forces have been considered due
253 to the large ventilation areas by more than 30% in two façades needed for the greenhouse and
254 building bioclimatic operation. As noted in this assessment, these are higher than pressure forces
255 as it is in conventional greenhouse construction (Max et al., 2012). In addition to wind loads,
256 live loads also included maintenance work (0.4 kN/m²) and snow loads (0.4—1.6 kN/m²), as
257 stated in EC-1 for the different regions of Europe assessed (see results section for details).
258 Finally, dead loads from the building materials considered sum 0.5 kN/m². The serviceability
259 limit has been set at L/300 for all beams and columns. Softwares CYPE 3D (CYPE Ingenieros,
260 2018) and Wineva (Universitat Politècnica de Catalunya, Sastre et al., 2014) have been used to

261 test all load combinations and various optimized design cases to meet the ultimate and
262 serviceability limit states of the structure.

263

264 2.3 Improvement studied scenarios

265 Greenhouse design is not a trivial issue and many factors influence its operational performance.
266 Thus, the structural components of the greenhouse have been assessed without changing its
267 geometry (roof slope, iRTG height or dimensions), which would directly impact the light
268 transmissivity, ventilation rates, inner temperatures and thus, crop productivity. The scenarios
269 proposed derive from the factors identified by structural modelling as the most relevant for
270 greenhouse design. Accordingly, internal and external greenhouse variables have been modified
271 as follows:

- 272 1. *Internal variables:* (i) optimizing profiles section and orientation; (ii) increasing the
273 steel strength from 275 to 355 MPa in accordance with EN 1993-1-1 (CEN, 2019);
274 and by (iii) substituting beams with lightweight tensioned cables (Figure 3)
275 according to tensegrity design principles .
- 276 2. *External variables:* terrain category conditions according to EC-1 (cat. II for rural-
277 suburban area as it is located the ICTA building; and cat. IV for dense urban
278 environment). Rural environment (cat. I) has been also assessed, as it applies to
279 conventional greenhouses here also compared with.

280

281 These variables have been evaluated in different improvement scenarios (S1, S2, see
282 Figure 2) respect to the baseline scenario (S0). Then, they have been compared with existing
283 literature and with further detail with conventional Venlo greenhouse scenarios placed on
284 soil and covered with a 4mm single glass (SCG.1) and with an EVA single-plastic film (SCG.2),
285 both adapted from (Boulard et al., 2011).

286

287 **S0. BAU – Baseline scenario**

288

289 **S1. Suburban structural improvement**

290

S1.1 Steel S275, suburban environment

291

S1.2 Steel S355, suburban environment

292

293 **S2. Urban structural improvement**

294

S2.1 Steel S275, urban environment

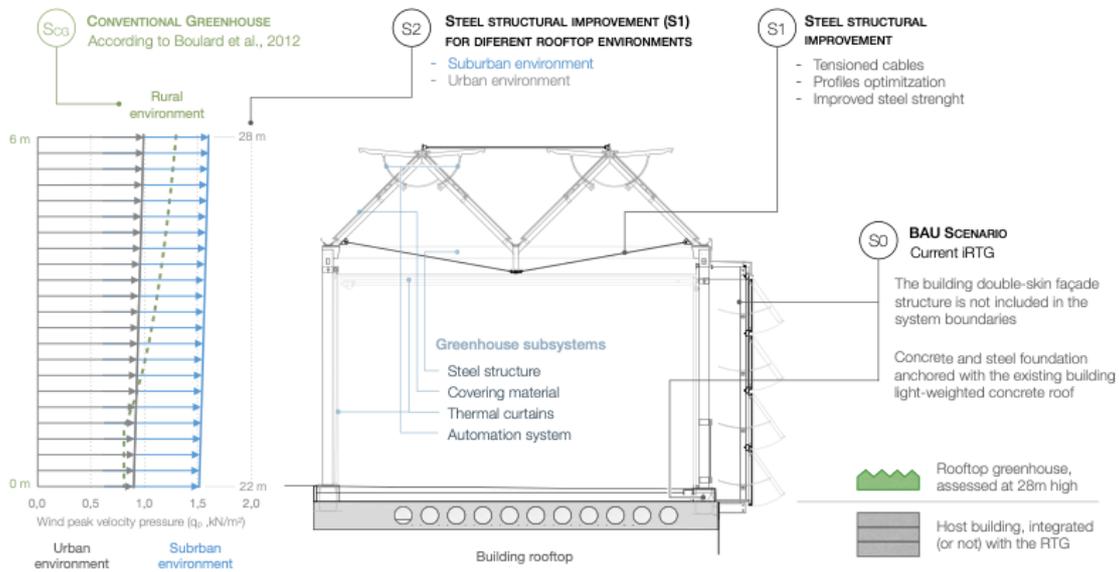
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S2.2 Steel S355, urban environment

SCG. Conventional greenhouse scenarios (Boulard et al., 2011)

SCG.1 Steel structure + horticultural glass, rural environment

SCG.2 Steel structure + EVA plastic film, rural environment



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302
303

Figure 2. Cross section of the ICTA iRTG with all identified scenarios assessed and its main characteristics.

304
305

2.5 Life Cycle Assessment

306 Life Cycle Assessment has been widely used as a standard methodology defined by ISO 14040
307 (International Organization for Standardization, 2006) to identify resources and assess its
308 environmental performance throughout the life cycle of all alternative system scenarios set
309 in this study.

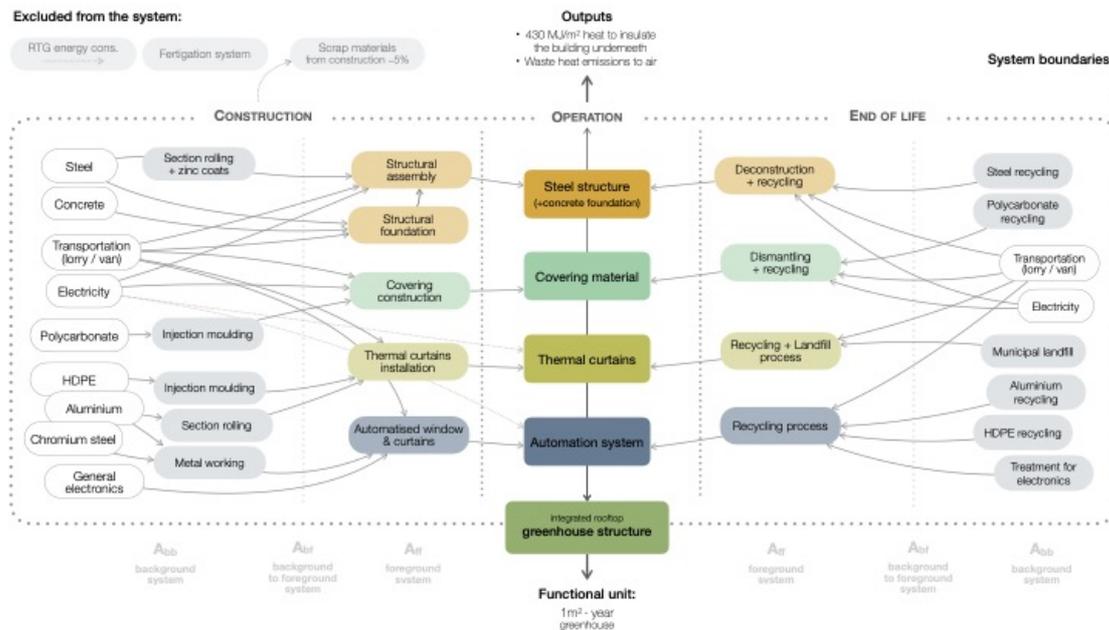
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2.5.1 Goal and scope definition

312 The functional unit employed in this assessment was “1 m² of a greenhouse structure for a
313 timeframe of 1 year”. This functional unit is in line with previous studies in greenhouses
314 (Sanyé-Mengual et al., 2015c) and buildings (Cabeza et al., 2014; Chau et al., 2015), while
315 excludes the crop production processes commonly assessed in agriculture (usually measured
316 in kg of produced crops) to place the environmental focus in the greenhouse structure solely.
317

318 The greenhouse system here considered all input construction materials as well as all
319 permanent technical infrastructure (Figure 3), distinguishing all material flows in all its life
320 cycle stages for 50 years of greenhouse structural maintenance. The fertigation system and

321 the energy to passively operate the greenhouse indoor climate are considered operational
 322 flows which vary depending on the crop and thus, are excluded from the assessment. The
 323 system model used was cut-off, assuming that all impacts and benefits of the recycling process
 324 are allocated to secondary products.
 325



326
 327 Figure 3. System boundaries of the greenhouse system.

328
 329 2.5.2 Life cycle inventory

330 Data compilation of the system under study included the production, transportation,
 331 construction, maintenance and waste management of all 4 subsystems in which the iRTG has
 332 been analyzed: steel structure (including concrete foundation); covering material; thermal
 333 curtains and automation system.

334
 335 Data from previous work in this iRTG has been used (Ruff-Salís et al., 2020a; 2020b; Sanjuan-
 336 Delmás et al., 2018; Sanyé-Mengual et al., 2015c) and updated with the available construction
 337 details after consulting the architects and stakeholders involved in the building construction
 338 process. All subsystems have been updated for this study, taking into account additional input
 339 materials not accounted before. Moreover, the automation subsystem has been added, which
 340 covers all mechanisms necessary to operate the greenhouse passive climate controls (windows
 341 and thermal curtains). This additionally allowed to distinguish the steel amounts needed for
 342 automation mechanisms to those that strictly belong to the structure that could be improved

343 from the structural assessment perspective of this paper. In order to do so, direct
344 measurements and project data has been used to account such mechanisms as well as the
345 electronic equipment needed as reported by (Muñoz-Liesa et al., 2020b). Space allocation has
346 been applied to part of the automation subsystem components that also operate the rest of the
347 passive climate building controls.

348
349 To account the machinery and energy needs for the construction process of the iRTG, on-site
350 building monitoring information has been used. The dismantling phase of the iRTG has been
351 estimated to be half of the inputs needed for its construction. Specific details of the
352 construction process of the iRTG can be found in Supplementary material. All selected
353 materials and processes were contrasted with existing literature in greenhouses (Boulard et
354 al., 2011) and buildings construction (Monticelli, 2010).

355
356 The reference scenario for conventional greenhouses used in agriculture has been based on
357 the study by (Boulard et al., 2011), which has been adapted from the Agribalyse 1.2 database
358 as stated in Ecoinvent database version 3.5 (Swiss Center for Life Cycle Inventories, 2018).
359 The foreground data from a glass and a plastic Venlo-type greenhouse has been adapted to
360 match with the functional unit of this study. Other background life cycle inventory from all
361 scenarios has been also retrieved from the Ecoinvent database. The end of life of materials
362 have been considered to be recyclable at the nearest point from the iRTG at 35km, despite a
363 small fraction of materials which would be landfilled. Details on all compiled data, as well
364 as inputs and outputs from the system, transportation distances and the waste scenarios, are
365 available in the Supplementary Material.

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367
368

2.5.3 Environmental impacts calculation

369 To perform the life cycle impact assessment (LCIA), the software Simapro version 9.0 has
370 been used with the latest ReCiPe method at the midpoint level (hierarchical perspective). The
371 most pertinent impact categories were selected based on authors judgment and previous
372 literature in buildings (Cabeza et al., 2014; Chau et al., 2015) and crop production (Sanyé-
373 Mengual et al., 2015c): Global Warming (GW, kg CO₂ eq.), Terrestrial Acidification (TA, kg
374 SO₂ eq.), Freshwater Eutrophication (FE, kg P eq.), Marine Eutrophication (ME, kg N eq.),
375 Fossil Resource Scarcity (FRS, kg oil eq.), Ecotoxicity (ET, kg 1,4-DB eq., including Marine,

376 Terrestrial and Freshwater Ecotoxicity), Stratospheric Ozone Depletion (SOD, kg CFC-11 eq.)
377 and Cumulative Energy Demand (CED, MJ, including renewable and non-renewable energy
378 sources).
379

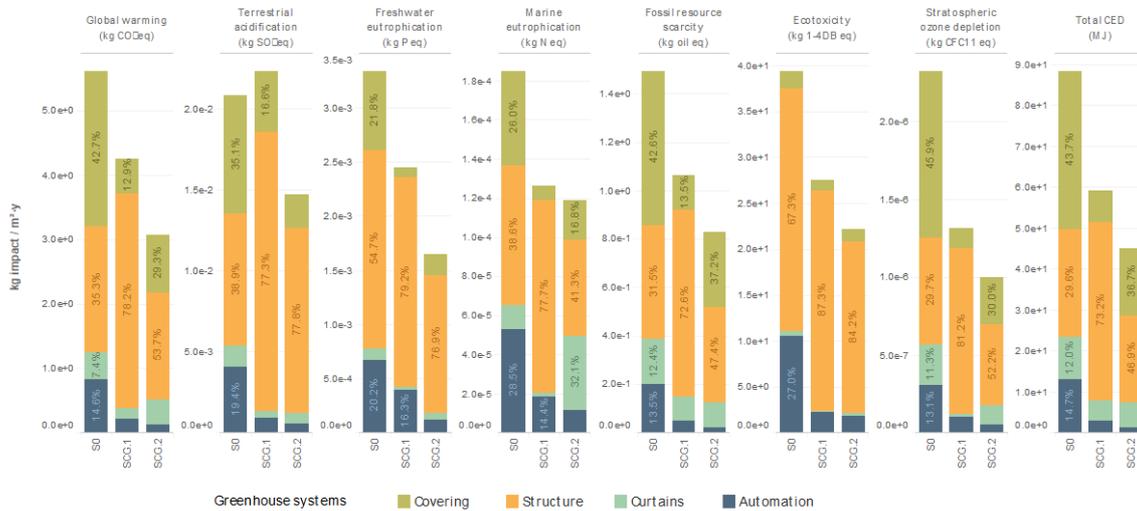
380 **3 Results and Discussion**

381 **3.1 Current iRTG (BAU – S0 scenario)**

382 **3.1.1 Impact assessment**

383 Figure 4 illustrates the environmental performance of 1m² per year of the current iRTG (S0)
 384 and the share of impacts among all greenhouse subsystems for all 8 impact categories
 385 analyzed. Besides, impacts for conventional greenhouses scenarios (SCG.1 and 2) have been
 386 added to compare and contextualize S0 impacts. The majority of environmental impacts are
 387 associated with the steel structure in half of impact categories analyzed (ranging from 31.5 to
 388 67.3%), especially due to the steel production and processing (section bar rolling and zinc
 389 coating). Polycarbonate covering impacts range from 21.8 to 45.9%, especially to its
 390 consequent emissions of carbon dioxide and methane (Sanyé-Mengual et al., 2015c) except
 391 for the Ecotoxicity category, which contributes less than 5% of the overall impacts. Only in
 392 FE and ME, polycarbonate covering impacts (particularly due to its construction energy
 393 burdens) are comparable with the automation subsystem impacts due to the metal inputs for
 394 automation and steel structure subsystems.

395



396

397 Figure 4. Environmental performance of 1m² per year of the iRTG in the current situation (scenario 0) and
 398 conventional greenhouse scenarios (SCG.1, 2) for all addressed impact categories. Percentatges indicate the
 399 share of impacts among greenhouse subsystems analyzed.

400 For both structure and covering subsystem their impact differs during the iRTG lifetime.
 401 Since polycarbonate and steel structure have 10 and 50 years of lifetime respectively, steel
 402 contributes to more than 70.0% of all impact categories during the construction phase while
 403 polycarbonate only impacts less than 20.7%. In contrast, during the operational phase,

404 between 42.0 and 65.3% of all impact categories (except for ET, with 14.6%) are due to
405 covering material replacement, followed by the automation subsystem. Finally, the energy
406 needed to dismantle the iRTG accounted for more than 82.5% at the end of life phase for all
407 impact categories as the majority of metals and polycarbonate are considered recyclable. Such
408 consideration has been done due to the simplicity of the greenhouse structure which
409 facilitates its dismantling process. Details for each subsystem impacts during its lifetime are
410 available at Supplementary material.

411

412 3.1.2 Differences with conventional greenhouse scenarios (SCG)

413 The overall assessment revealed a fold increase between the iRTG (S0) and the conventional
414 greenhouse scenarios (SCG.1 glass, SCG.2 plastic-film) of 1.3–1.8 and 1.6-2.3 respectively in
415 7 out of 8 impact categories analyzed. TA showed minor differences, of 0.9 and 1.4
416 respectively. The rationale behind these findings are the following.

417

418 First, the structure impacts are greater as a result of the higher complexity of the iRTG (S0,
419 see section 3.1.3) respect to conventional greenhouses (as SCG.1 and SCG.2). However, this is
420 compensated to some extent with the presence of aluminum in the conventional greenhouse
421 structures, especially used to reinforce the glass covered greenhouse (SCG.1). That causes
422 between 27.8% to 39.8% of the overall SCG.1 impacts for all impact categories, while only
423 contributes around 1% of all impact categories in SCG.2.

424

425 Second, the construction process entails greater energy needs than conventional greenhouse
426 construction especially due to the rooftop accessibility constraints (Kortright, 2001). Here,
427 4.78 MJ/m²·y was needed to build the greenhouse, which represents between 7.2- to 8.1-fold
428 increase compared to the conventional greenhouse scenarios (SCG.1 and 2, respectively,
429 (Boulard et al., 2011)). Moreover, unlike CA, more energy was needed to build the covering
430 material rather than the steel frame due to the articulated boom lift considered (which depend
431 on the building accessibility, see Supplementary material for details) to rise and install the
432 polycarbonate panels at the rooftop level up to 28m high. Besides, both greenhouse
433 construction would require building machinery and specialized installation at the
434 construction point, while in addition, conventional greenhouses normally require

435 agricultural machinery to prepare the soil (Boulard et al., 2011) which increases by 4-6% the
436 steel construction impacts for all impact categories.

437
438 Third, concrete amounts for BIA are much lower than CA as the former takes profit of the
439 existing building fabric and is only required to reinforce the steel anchoring system. In
440 particular, the multi-tunnel greenhouse assessed by (Sanyé-Mengual et al., 2015c) requires
441 2.4 times the amount of concrete of this RTG (0.212 kg/m²-y), while in Venlo-type
442 greenhouses concrete fold increase ranges between 4.6 and 5.9 (Anton et al., 2012; Bosona
443 and Gebresenbet, 2018; Röös and Karlsson, 2013; Torrellas et al., 2012). Similar trends show
444 SCG.1 and 2, with a 4.7- and 5.2-fold increase compared to S0, despite concrete contributes
445 only between 1.0% and 4.8% of the conventional greenhouse scenarios environmental
446 impacts. However, increased thermal inertia derived from higher concrete loads in RTGs,
447 representing an indirect quantifiable benefit (Muñoz-Liesa et al., 2020b). In turn, this could
448 compensate for the increasing height of currently built and projected greenhouses designed
449 to improve its thermal inertia.

450
451 Finally, the lifetime of greenhouse structures. While for the iRTG the service lifetime is
452 considered to be equal as the hosted building (50 years), conventional greenhouses are
453 expected to last maximum 15 years according to EN 13031-1 (CEN, 2019). Despite many
454 studies consider this reference value in their assessments (Anton et al., 2012; Sanyé-Mengual
455 et al., 2015c; Torrellas et al., 2012), others consider that longer lifetimes could be assumed as
456 the conventional greenhouses scenarios here assessed (SCG.1 and 2) for 25 years as published
457 by (Boulard et al., 2011). In contrast, 15 years of lifetime would result in a 1.66-fold increase
458 of their impacts. From the authors perspective, that probably relies on the greenhouse
459 structure and whether its design is less sophisticated and more understood as a provisional
460 solution (as some soil-based multi-tunnel greenhouses covered with simple plastic-films) or
461 not (such as Venlo-greenhouse structures highly insulated).

462
463 3.1.3 Greenhouse design factors
464 The higher sophistication of the ICTA-iRTG compared to CA lies on key design factors that
465 have been identified within the structural assessment. Particularly, design factors 1-4 heavily
466 penalizes structure boundary conditions of the ICTA-iRTG leading to greater steel

467 reinforcement. Each key factor and its structural implications have been analyzed in relation
 468 with BAU scenario (S0) and in comparison with the improved associated scenarios assessed
 469 (Table 1).

470
 471

Design factor	Structural implications	Associated scenario
1. Building integration	The host building boundary conditions determine the steel sections, in order to match with building structural profiles and aesthetics to better integrate the RTG.	Scenarios 1.1 and 2.1 represent a standard module of a iRTG, with optimized steel sections efficiently orientated to minimize its costs. A standard S275 steel is used.
2. Urban / suburban / rural environment	Wind speeds for greenhouse located in different rural or urban environments vary between 0.6—1.7x due to the upper terrain roughness, which affects wind design loads.	Scenario 1 represents a RTG located in a suburban environment, while scenario 2 in a dense urban environment. Scenarios SCG.1 and 2 represent a greenhouse in a rural environment.
3. Greenhouse ground height	Wind design loads in higher altitudes such in building rooftops at 28m height, are between 1.3—1.8x times the design load in the ground (for a greenhouse 6m height). Similarly, as higher is the greenhouse ridge, higher are the wind design loads.	Scenarios 0, 1 and 2 are located at 28m height, while scenario SCG.1 and 2 are 6m height at the ground level. Greenhouse geometry, including ridge height, has been unchanged as that would change internal climate conditions.
4. Lateral ventilation design: suction forces	If there are more than >30% of holes in two or more façades, suction forces must be accounted, which largely penalizes environmental loads to be accounted.	For iRTGs placed in Southern Europe, natural ventilation in façades has been accounted, needed to reduce iRTG overheating during summer (Muñoz-Liesa et al., 2020b). As conventional venlo greenhouses, no lateral ventilation has been accounted for Northern European RTGs, leading to higher resistance to snow loads up to 1.6 kN/m ² .
5. Dead and snow loads	Because suction forces (4) and its derived environmental loads are greater than dead loads, covering material loads do not affect the iRTG design. Similarly, no suction forces are accounted for Northern Europe, which compensates to certain extent snow loads.	All scenarios are tested for heavier materials than polycarbonate (S0) such as double glass (0.3 kN/m ²). Snow loads with suction forces could be up to 0.4kN/m ² (Southern Europe) and up to 1.6 kN/m ² without it (Northern Europe regions located H<1000m AMSL).
6. Building accessibility: construction costs	According to S0 assessment, construction costs represent between 3.1—24.1% (and more than 10.5% in 7 out of 8 categories) share of all impact categories. Building machinery needs greatly relies on building accessibility.	No alternative scenarios have been proposed in order to account the worst structural hypothesis. However, alternative machineries are presented in Supplementary Material.

472
 473 Table 1.Greenhouse design factors identified in the structural assessment and a description of its structural
 474 implications and the proposed associated scenarios covering each factor.

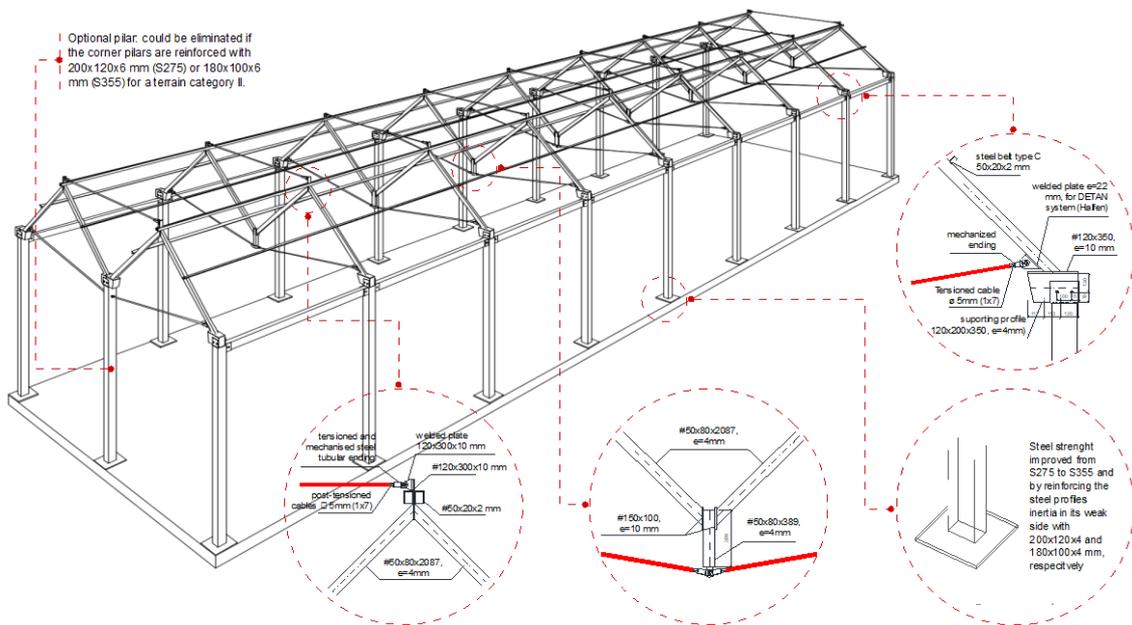
475
 476 Thus, in order to minimize the steel structure impacts revealed in S0, the alternative
 477 optimized scenarios for different rooftop conditions have been proposed according to the key
 478 design factors of greenhouses structures which apply in both BIA and CA contexts). As a
 479 result, improvement scenarios aim to generalize the iRTG structure to other environments
 480 and boundary conditions while improving its structural design. Similarly, these key design
 481 factors can be used in further assessments as a guideline to design resource-efficient
 482 greenhouse structures.

484 3.2 Structural improvement

485 3.2.1 Suburban environment: S1 scenarios

486 Scenario 1.1 a profile optimization has been done mainly by replacing the squared steel
487 columns of the RTG, originally chosen to match with all rooftop structure and the double
488 skin façade, simplifying this way the building structure and improving RTG integration in
489 terms of buildings architecture. This allowed to reduce by 9.6% the structural steel weight
490 compared to the current iRTG structure (Figure 5 and Figure 6). Therefore, by using
491 rectangular profiles properly orientated, they better efficiently use their inertia and take
492 profit of their maximum strength side. By doing so, this scenario represents a standard rooftop
493 Venlo greenhouse structure attached to a building in a suburban environment with a standard
494 S275 steel structure.

495



496

497 Figure 5. Greenhouse perspective of the optimized iRTG main steel structure for the ICTA case study with a
498 redesigned tensegrity Venlo-type chapels and steel sections. Auxiliary steel components, as well as
499 greenhouse bearing systems, have been not represented to show major optimized elements.

500

501 An additional 14.4% weight reduction has been obtained by increasing the steel strength from
502 275 to 355 MPa. Despite 275 MPa is the most available commercial steel, strengthen steels
503 such as 355 MPa are also available for a +17% increased cost (ITeC, 2020), which does not
504 economically compensate the steel reduction and thus, probably explains the chosen strength
505 in the ICTA case study. Finally, the steel beams that support the greenhouse chapel have been
506 substituted by two post-tensioned steel cables (Figure 5). Applying a 3.5 kN pre-stress force

507 to both cables, compression loads are avoided improving this way the steel efficiency. Such
508 structural design results from tensegrity principles (Cowcher, 2015) and, similarly to the
509 bearing systems, it constitutes a simple and effective way to improve the structural stiffness
510 and performance. By doing so, the greenhouse chapel works as a part of the structure forming
511 a steel truss instead of being supported by the traditional steel frames and beams. This resulted
512 in an optimized structure 13.4% lighter that sums up a total steel weight reduction of 27.8%
513 (scenario 1.2, see KPI table from Figure 6).

514
515 Scenario 1.2 is, therefore, a more complex greenhouse but without compromising too much
516 neither its construction process nor its costs, as the use of post-tensioned cables is a well-
517 known technique in building industry (such in ICTA building) but here applied in the
518 greenhouse system. Such design also largely reduces RTG steel weight, which is especially
519 relevant when rooftop loads are a limitation in BIA as in rehabilitated buildings (Toboso
520 Chavero et al., 2018). Besides, the use of steel cables in conventional greenhouses mainly to
521 reduce its costs can also be found at the most simple Parral-type greenhouses in Almeria
522 (Montero, 2012) or in multi-tunnel greenhouses to increase the greenhouse span (FAO, 2002)
523 and even in more sophisticated and visually attractive greenhouses as the Edinburg Royal
524 Botanical Gardens, UK (Maunder, 2008).

525

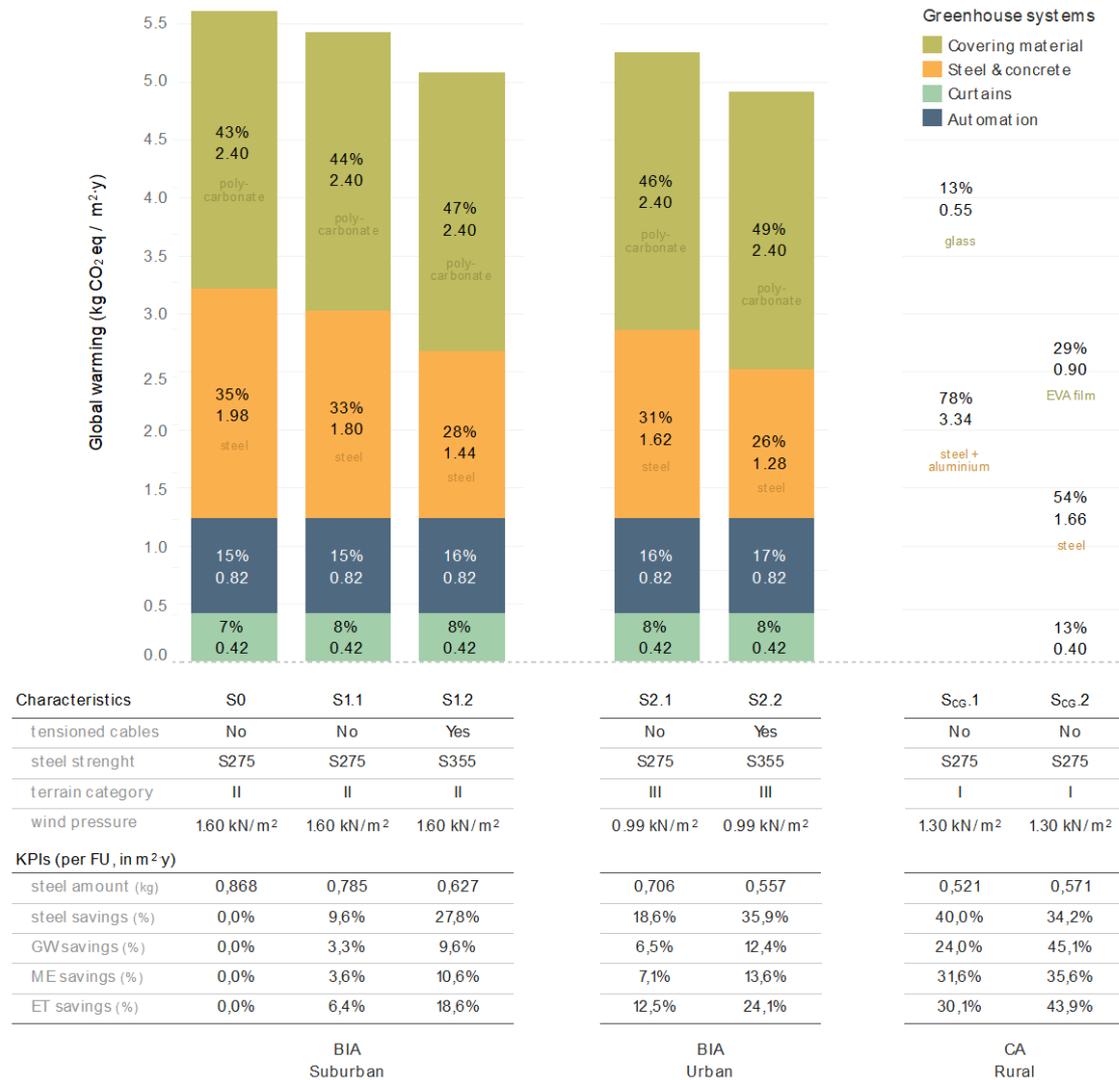


Figure 6. Steel structure characteristics and key performance indicators (KPIs) for each studied scenario. Lighter colours diferenciate adapted data of CA from original data (BIA).

3.2.2 Suburban environment (S2 scenarios)

Scenarios 2.1 and 2.2 applied the same profiles optimization and increased strength combined with tensile principles applied in scenarios 1.1 and 1.2 respectively but considering the iRTG was located in an dense urban area instead (category IV in EC-1). That results in a wind pressure forces reduction up to 38.1% (see table from Figure 6), which have led to a structural steel reduction of 18.2% and 35.9% for scenarios 2.1 and 2.2 respectively (see Figure 6). Note that as the wind pressure for a rural environment is even higher than a rooftop at 28m high in urban conditions (see wind graph from Figure 2), the non-optimized steel structure of conventional greenhouses have a major steel amount (0.571 kg/m²·y) and environmental impact than urban scenarios (S1.3 and S1.4, Figure

540 6). Details on wind pressure design loads in BIA and CA environments are available in
541 Supplementary Material.

542

543 3.2.3 Environmental assessment of greenhouse improvement scenarios

544 The environmental burdens of the steel structure subsystem in all improvement scenarios
545 are reduced at a similar rate than the steel weight savings (Figure 6). Particularly, 6 out of 8
546 impact categories decrease from 9 to 35% for scenarios 1.1 and 2.2 respectively, while little
547 more improvement exists in ET and FE impact categories (10 – 36%). Compared to SCG
548 scenarios, the structural improvement compensated the greater amounts of steel of the
549 suburban environment. In SCG.2 this is also translated, for instance, into 13.3% less GW
550 impacts, while SCG.1 the aluminium contribution greatly penalizes its environmental
551 performance. Since polycarbonate impacts are of great importance in all BIA scenarios, the
552 overall environmental savings of the structural improvement range from 3 to 12% for GW,
553 FRS, SOD and CED; 4 to 14% for ME and TA; and 5 to 24% for ET and FE (see table from
554 Figure 6). Besides, all impact categories are reduced with similar behavior as the GW here
555 presented (see Figure A.1 for further details).

556

557 The increased relative impacts of covering materials after the optimization underlines the
558 importance to optimize its performance with less impacting materials such as glass (SCG.1) or
559 plastic films (SCG.2) suitable for buildings (e.g., ETFE films) in further research. As noted
560 earlier, all scenarios here assessed accounted wind suction loads, and since these are more
561 important than dead loads, the structural design heavily relies on suction environmental loads
562 rather than dead loads. As a side effect, no structural changes are required for heavier
563 materials than the ICTA-iRTG polycarbonate such as double glass panel (0.3 kN/m²). This also
564 occurs in rural environments, where the structural design for conventional greenhouse
565 structures covered with glass or plastics differ only slightly (Max et al., 2012).

566

567 3.3 Environmental impacts shifting between CA and BIA

568 RTGs are one of the most complex BIA structures in urban agriculture. The comparison of
569 greenhouse structures between BIA and CA contexts revealed that material and energy
570 construction flows are generally greater in BIA. Because BIA and RTG are still a novel field
571 not studied in depth, authors previously suggested that those additional impacts where

572 derived from the greenhouse building integration and building codes requirements (Cerón-
573 Palma et al., 2012; Sanyé-Mengual et al., 2015c) as well as due to the greater wind loads on
574 rooftops compared to soil-based greenhouses (Montero et al., 2017). That would turn BIA
575 RTG structures less suitable in environmental terms compared to CA.

576
577 However, the identified factors that affect greenhouse structural design reveals that the
578 construction impacts in the urban environment do not imply environmental shifting of
579 impacts per se. Particularly, the current assessment revealed that ICTA-iRTG structure
580 integration with the building implies sub-optimal steel profiles that caused 10.5% of
581 additional steel inputs (scenarios 1.1, 2.1). Moreover, the structure is also harmed by suburban
582 environment location (S1), less suitable than a urban location (S2) as wind desing loads are
583 higher (1.60 and 1.30 kN/m², respectively, see table from Figure 6). In order to compensate
584 these additional constrains, the optimized structure allowed to reduce the steel amounts of
585 BIA up to 22.9% compared to SCG.2.

586
587 Overall, even environmental shifting exists from CA to BIA in the assessed scenarios due to
588 the covering material impacts, BIA structures in urban areas could benefit from less wind
589 speeds that could avoid this effect, independently from the chosen covering materials or the
590 structural design and materials (aluminium and/or steel). Thus, rooftop conditions do not
591 always imply higher environmental impacts, as only if BIA structures are located in suburban
592 areas construction environmental impacts might result higher. In any case, the optimized
593 structural design here proposed could aid to compensate BIA boundary conditions (including
594 its greater construction costs) in order to reduce structural impacts of RTG in further BIA
595 projects.

596
597 These findings are applicable at the greenhouse structural level (i.e., per functional unit,
598 m²·y), including the environmental burdens of the whole life cycle stages of the structure.
599 Thus, despite they not cover the whole life cycle of greenhouse crop production, they place
600 the environmental focus on one of the major impacts in unheated greenhouse crop production
601 for both BIA and CA contexts (Anton et al., 2012; Muñoz et al., 2008; Rufí-Salís et al., 2020a;
602 Sanjuan-Delmás et al., 2018; Torrellas et al., 2012). Covering materials structural implications
603 have been also included in order to assess alternative less impacting materials in further

604 research (such as glass, assessed in SCG.1). Therefore, by avoiding environmental shifting of
605 its construction impacts, the overall BIA impacts could be avoided as well. Further assessment
606 at the production point would probably demonstrate that potential initial construction
607 burdens could be further compensated with the advantageous operational flows derived from
608 BIA (e.g., by recovering waste building heat), demonstrating the feasibility of BIA structures
609 and urban agriculture compared to conventional greenhouses.

610

611 3.4 Generalization to other BIA / CA contexts

612 The structural improvement of the RTG here assessed has been done following the European
613 standards to generalize the proposed greenhouse structures in urban environments beyond
614 the ICTA-iRTG case study. Moreover, because the Venlo greenhouse is a highly versatile
615 structure with a “quasi-standard” design (Montero and Van Henten, 2011), it that can meet
616 different requirements. Alternative covering materials are also possible with the designed
617 scenarios as well as lateral and roof ventilation if needed. However, certain conditions apply
618 when generalizing these results to other European regions: i) RTGs located below 1000m from
619 the sea level; ii) snow loads up to 0.4kN/m² in Southern Europe where lateral ventilation is
620 needed and up to 1.6kN/m² in Northern Europe regions without lateral ventilation (which
621 covers the majority of cities in Europe except for some Scandinavian countries and Iceland
622 according to CEN, 1991); and iii) RTGs must be located below the maximum rooftop height
623 depending on the scenario and urban environment. Detailed guidelines on extrapolations of
624 the assessed scenarios to other European contexts can be found in Supplementary Material.

625

626 The generalization to other environments here mentioned could derive to non-optimized
627 structures and, therefore, would need to recalculate the structure for each specific conditions.
628 Moreover, it is important to note that specific environments located near the sea or next to a
629 plane area with less terrain rugosity are less suitable for BIA as wind loads are higher
630 compared to a centric location of a urban area. However, it can be useful as a first assessment
631 as the current ICTA-iRTG’s inventory (Sanyé-Mengual et al., 2015c) has been used in other
632 studies such as (Benis et al., 2018). Finally, the tensegrity structure design can also be
633 replicable to conventional Venlo greenhouse structures, though adaptations would be needed
634 to match with specific boundary conditions beyond the urban environments here assessed.

635 **Conclusions**

636 Achieving better levels of environmental performance of resource consumption in buildings
637 and agricultural systems is crucial to improve cities metabolism. This study assessed the
638 material and energy flows and its environmental impacts at the European level of rooftop
639 greenhouse structures based on the ICTA-iRTG case study in order to identify the main key
640 design factors and propose alternative optimized scenarios.

641
642 Business as usual scenario revealed that the steel structure and covering material are
643 responsible for the majority of material environmental burdens, up to 67.3% and 45.9%
644 respectively, from all impact categories analyzed. The iRTG structure required higher steel
645 amounts and needed an initial energy investment around 8 times higher than in the case of
646 conventional greenhouses. In turn, it resulted in a 6-fold reduction in terms of concrete
647 amount, due to the existing urban fabric and its increased thermal inertia. Finally, the iRTG
648 assessed in this study, as well as other BIA structures benefited from greater lifetime
649 expectancies (between 2 and 3.3-fold) than conventional greenhouses.

650
651 The proposed optimized greenhouse structural design and the identification of key design
652 factors resulted in 4 improvement scenarios that allowed to mitigate BIA environmental
653 burdens and extrapolate RTG impacts in the European context. These key design factors that
654 affect material use-efficiency in RTGs were: (i) building rooftop height and accessibility; (ii)
655 greenhouse location (i.e., rural, suburban or urban); and iii) greenhouse ventilation design.
656 The improvement scenarios resulted in overall savings from 3.3 to 24.1% among the impact
657 categories addressed. Moreover, such design was tested for alternative covering materials that
658 could aid to decrease iRTG life-cycle impacts in further assessments.

659
660 Understanding the design factors applied in a Venlo greenhouse design allowed us to
661 demonstrate that urban environment characteristics (such as lower wind loads or existing
662 building fabric) could favor BIA structures compared to CA structures in rural environments.
663 Thus, BIA does not imply greater material inputs and environmental burdens per se, as other
664 authors previously suggested due to the greater wind loads in rooftops or more strict building
665 codes. In conclusion, shifting main environmental burdens from CA to BIA is avoidable in
666 favorable urban contexts or when compensated by optimized greenhouse structures.

667 **Acknowledgement**

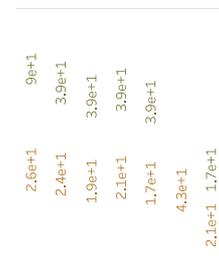
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679

680

681 **Appendix**

Global warming (kg CO₂ eq)



682

683

684

Figure A.1 Environmental impacts of the improvement studied scenarios compared with the conventional greenhouse ones.

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