

1       **Carbon footprint of constructed wetlands for winery wastewater**  
2   **treatment**

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19

20 **Abstract**

21 The aim of this study was to estimate the carbon footprint (CFP) of constructed wetlands  
22 for winery wastewater treatment. In particular, a constructed wetland scenario was  
23 compared to the previous scenario (third-party management) and to an activated sludge  
24 system. CFP considered both indirect and direct greenhouse gas (GHG) emissions  
25 measured on-site. Moreover, an economic analysis of the considered scenarios was also  
26 addressed. The results showed that the constructed wetland scenario had the lowest CFP  
27 ( $1.2 \text{ kg CO}_2\text{eq m}_{\text{water}}^{-3}$ ), while the third-party management was the worst scenario ( $52 \text{ kg}$   
28  $\text{CO}_2\text{eq m}_{\text{water}}^{-3}$ ) followed by the activated sludge system ( $4.5 \text{ kg CO}_2\text{eq m}_{\text{water}}^{-3}$ ). This was  
29 mainly due to the high GHG emissions generated by wastewater and sludge transportation  
30 as well as chemicals and electricity consumption in the third-party and activated sludge  
31 scenarios compared to the constructed wetlands. In terms of costs, the constructed  
32 wetland system was shown to be a low-cost technology which would reduce the capital,  
33 operation and maintenance costs associated with winery wastewater treatment up to 50  
34 and 98%, respectively. Finally, constructed wetlands are low-cost and environmentally  
35 friendly technologies which constitute a sustainable alternative to conventional solutions  
36 for winery wastewater treatment.

37

38 **Keywords:** activated sludge; treatment wetland; greenhouse gas emissions; life cycle  
39 assessment; winery wastewater.

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41

## 42 **1. Introduction**

43 Climate change has become a major issue that has created a global concern. This  
44 phenomenon is attributed to the increase of anthropogenic greenhouse gas (GHG)  
45 emissions (e.g. carbon dioxide (CO<sub>2</sub>), methane (CH<sub>4</sub>) and nitrous oxide (N<sub>2</sub>O)) from  
46 different human activities. In particular, it was estimated that wastewater treatment may  
47 account for around 10 per cent of anthropogenic methane emissions, both from domestic  
48 and industrial sources (IPCC, 2006; UNFCCC, 2018). The Carbon footprint (CFP) is a  
49 tool that can be used to estimate the contribution of wastewater treatment plants to global  
50 warming and to identify hotspots for its prevention and/or mitigation (Flores-Alsina et  
51 al., 2011; Wiedmann and Minx, 2008). Several studies, which assessed the CFP of  
52 conventional wastewater treatment plants (e.g. activated sludge system), pointed out that  
53 their contribution to the global GHG emissions is mainly due to energy and chemicals  
54 consumption for plants operation (Biswas and Yek, 2016; Caniani et al., 2018; Caivano  
55 et al., 2017; Chai et al., 2015; Flores-Alsina et al., 2011; Gu et al., 2016; Gustavsson and  
56 Tumlin, 2013; Parravicini et al., 2016; Rosso and Bolzonella, 2009; Vijayan et al., 2017).

57         Constructed wetland systems are natural technologies which constitute an  
58 alternative to activated sludge systems for urban and industrial wastewater treatment due  
59 to their low cost, low energy requirement and easy operation and maintenance (Arden  
60 and Ma, 2018; Vymazal, 2014). Specifically, they have been proved to be a suitable  
61 solution for winery wastewater treatment. Indeed, constructed wetlands, which can be  
62 perfectly integrated into the rural landscape, are able to couple with seasonal variation in  
63 wastewater flows and loadings that typically occur in some food industries (e.g. wine  
64 industry) (Ávila et al., 2016; Kim et al., 2014; Rozema et al., 2016; Serrano et al., 2011  
65 Shepherd et al., 2001).

66 Previous studies comparing the environmental impacts of constructed wetland  
67 systems with conventional technologies pointed out that the former was the most  
68 environmentally friendly wastewater treatment option, mainly due to the low electricity  
69 and chemicals consumption (Dixon et al., 2013; Fuchs, et al., 2011; Garfí et al., 2017;  
70 Machado et al., 2007; Yildirim et al., 2012). Nevertheless, most of these studies  
71 considered systems treating urban wastewater. To the best of the authors' knowledge,  
72 only one study analysed the environmental impacts of constructed wetlands treating  
73 winery wastewater (Flores et al., 2019a). However, in this study, direct GHG emissions  
74 from wastewater treatment were estimated considering the emissions rates from the  
75 literature. On the other hand, the importance of considering real GHG emissions  
76 measured on-site in full-scale wastewater treatment plants was pointed out by several  
77 studies in order to improve the quality of the assessment (Gallego-Schmid and Zepon-  
78 Tarpani, 2019; Flores et al., 2019a; Maktabifard et al., 2020; Nguyen et al., 2020).

79 In this context, the WETWINE project (<http://wetwine.eu/en/>) aimed to promote  
80 constructed wetlands as an environmentally friendly and innovative solution to treat  
81 effluents produced by wine industries in South-Western Europe (i.e. Spain, Portugal and  
82 the South of France) (SUDOE Programme). One of the main goals of the project was to  
83 quantify the environmental benefits in terms of GHG emissions reduction caused by the  
84 implementation of this technology compared to the existing solutions (i.e. activated  
85 sludge systems, third-party management). To this end, a constructed wetland system was  
86 implemented in a winery located in Galicia (Spain) and direct GHG emissions were  
87 monitored during the vintage season and the rest of the year.

88 The aim of this study was to estimate, for the first time, the CFP of constructed  
89 wetlands for winery wastewater treatment in the frame of the WETWINE project. In

90 particular, the constructed wetland scenario was compared to the previous scenario (third-  
91 party management) and to an activated sludge system also implemented in another winery  
92 located in Galicia (Spain). The CFP considered both indirect and direct GHG emissions  
93 measured in all the systems. Moreover, an economic analysis of the considered scenarios  
94 was also addressed.

95

## 96 **2. Materials and methods**

97 The CFP is defined as the total set of GHG emissions caused by an activity or product  
98 expressed as carbon dioxide equivalent (CO<sub>2</sub>eq). It is a measure of the total amount of  
99 GHG (e.g. CO<sub>2</sub>, CH<sub>4</sub> and N<sub>2</sub>O) emissions of a defined system or activity, considering the  
100 whole life cycle (ISO, 2013; Vijayan et al., 2017). It is calculated by converting the  
101 estimated GHG emissions into carbon dioxide equivalents (CO<sub>2</sub>eq) by global warming  
102 potentials (GWPs) over 100 years (e.g. 1, 28 and 265 CO<sub>2</sub>eq for CO<sub>2</sub>, CH<sub>4</sub>, and N<sub>2</sub>O  
103 respectively) (IPPC, 2006, 2014).

104

### 105 **2.1 Scenarios description**

106 In this study, three real winery wastewater treatment and management alternatives  
107 implemented in two wineries (Ws) located in Galicia (Spain) were considered. Their  
108 characteristics are summarized in Table 1.

109 The W1 scenario consisted of a third-party wastewater management implemented  
110 in a winery located in Galicia (Spain). In this winery, around 1,400 m<sup>3</sup> of wastewater are  
111 produced per year. Wastewater was stored in a septic tank and then transported (240 km),  
112 treated and discharged by a third-party.

113           The W2 scenario consisted of a constructed wetland system recently implemented  
114 in the same winery as the W1 scenario in the frame of the WETWINE project, in order to  
115 replace the third-party management. The constructed wetland system consists of a  
116 hydrolytic upflow sludge blanket (HUSB) reactor, followed by two vertical subsurface  
117 flow constructed wetlands (30 m<sup>2</sup>), one horizontal subsurface flow constructed wetland  
118 (30 m<sup>2</sup>), and a sludge treatment wetland (20 m<sup>2</sup>). Treated wastewater is discharged into  
119 the sewer system and treated in a municipal wastewater treatment plant. Stabilized sludge  
120 is reused as fertilizer or soil conditioner.

121           The W3 scenario consisted of an activated sludge system implemented in a winery  
122 which treats approximately 4,800 m<sup>3</sup> of winery wastewater per year. After a pre-  
123 treatment, wastewater is treated in an extended aeration reactor followed by a secondary  
124 settler. Treated wastewater is discharged into the municipal sewer system and treated in  
125 a municipal wastewater treatment plant. The sludge produced is stored on-site,  
126 centrifuged and transported (150 km) by a third-party to an incineration facility.

127

## 128 **2.2 System boundaries and functional unit**

129 System boundaries included systems construction, operation and maintenance over a 20-  
130 years period. Input and output flows of materials (i.e. construction materials and  
131 chemicals) and energy resources (electricity) were systematically studied for all  
132 scenarios. Direct GHG emissions associated with wastewater treatment as well as sludge  
133 reuse and application to agricultural soil were also included in the boundaries. In the case  
134 of scenario W1 (third-party management), inputs and outputs associated with wastewater  
135 transportation and disposal were also accounted for. In the case of the activated sludge  
136 system (scenario W3), inputs and outputs associated with sludge transportation and

137 disposal (i.e. incineration) were also included in the boundaries. In the case of the  
138 constructed wetland system (scenario W2), the system expansion method has been used  
139 in order to consider the avoided burdens of using the fertilizer obtained from the sludge  
140 instead of a conventional fertilizer (Guinée, 2002; ISO, 2006b).

141 The functional unit was defined as 1 m<sup>3</sup> of treated water, since the main function  
142 of the solutions considered was to treat wastewater.

143

### 144 **2.3 Inventory analysis**

145 Inventory data for the investigated scenarios are shown in Table 2, 3 and 4. Due to the  
146 seasonal variation in wastewater flows and loadings, and, subsequently, in systems  
147 operation and performance, inventory data were presented considering two seasons (i.e.  
148 the vintage season and the rest of the year). For all scenarios, inventory data regarding  
149 construction materials and operation were based on the specific case studies and were  
150 collected by means of a survey carried out during 2017 and 2018 (UPC, 2018).

151 Direct GHG (i.e. CO<sub>2</sub>, CH<sub>4</sub> and N<sub>2</sub>O) emissions generated in the septic tank  
152 (scenario W1), the constructed wetlands (scenario W2) and the activated sludge system  
153 (scenario W3) were measured by using a Gaset DX4015 Fourier transform infrared  
154 (FTIR) gas analyser. The measurements of CO<sub>2</sub>, CH<sub>4</sub> and N<sub>2</sub>O fluxes were done using  
155 the static chamber method for the constructed wetlands (scenario W2) (Chen et al., 1997;  
156 De la Varga et al., 2015; Uggetti et al., 2012) and the floating chamber method for the  
157 activated sludge treatment plant (scenario W3) (Czepiel et al., 1995; Hwang et al., 2016;  
158 Ribera-Guardia et al., 2019). Two campaigns were carried out during the vintage season  
159 (August/September 2018) and the rest of the year (February/March 2018). Different  
160 points of each treatment unit of the systems were monitored to envisage the spatial

161 variation of the emissions. Moreover, for the constructed wetlands, feeding and resting  
162 periods and in between feeding pulses periods were considered for the measurements.  
163 This let to take into account the difference between the constructed wetlands types  
164 (Mander et al., 2014). Further details on the methodology used and the results obtained  
165 can be found elsewhere (Flores et al., 2019b; Flores et al., submitted).

166       Regarding the constructed wetlands (scenario W2), CO<sub>2</sub> uptake due to plants  
167 photosynthesis was taken into account considering sequestration rate from the literature  
168 (Kanungo et al., 2017; Mitsch et al., 2012). They were withdrawn from the overall CO<sub>2</sub>  
169 emissions (Table 3 and 4). it has to be mentioned that CO<sub>2</sub> from biogenic sources does  
170 not contribute to Climate Change Potential (Doorn et al., 2006). Thus, the LCA results  
171 do not depend on plants species.

172       Direct GHG (i.e. CH<sub>4</sub> and N<sub>2</sub>O) emissions due to sludge reuse and application to  
173 soil were obtained using the emission rates proposed by the literature (Arashiro et al.,  
174 2018; Flores et al., 2019a; IPCC, 2006; Lundin, 2000). GHG emissions associated with  
175 the production and transportation of construction materials and chemicals, electricity  
176 consumption, wastewater and sludge transportation and disposal, and the avoided  
177 fertilizer were obtained from the *Ecoinvent 3* database (Moreno-Ruíz et al., 2014;  
178 Weidema et al., 2013).

179

## 180 **2.5 Impact assessment**

181 The impact assessment is the transformation of the direct and indirect GHG emissions  
182 associated with the construction and operation of the systems to CO<sub>2</sub> equivalents (CO<sub>2</sub>eq).  
183 The CFP was calculated using the software SimaPro® 8 (Pré Consultants, 2018) and the  
184 IPCC Global Warming Potential method (IPCC GWP 100 years). For all the scenarios,



185 the CFP was calculated for the vintage season and the rest of the year in order to assess  
186 their fluctuations over the year.

187

## 188 **2.6 Economic analysis**

189 An economic analysis was conducted comparing the capital cost and the operation and  
190 maintenance costs of each scenario for a lifespan of 20 years. Data regarding systems  
191 design was based on specific case studies and were collected by means of a survey (UPC,  
192 2018). Prices were provided by local companies. The capital cost included the cost for  
193 earthmoving, construction materials purchase and electrical works. The operation and  
194 maintenance costs included the prices of electricity, chemicals, sludge transportation and  
195 disposal and equipment replacement.

196

## 197 **3. Results and Discussion**

### 198 **3.1 Carbon Footprint**

199 The CFPs of the three winery wastewater treatment alternatives ranged from 0.9 to 52.7  
200 kg CO<sub>2</sub>eq m<sub>water</sub><sup>-3</sup> (Figure 1). As shown in Figure 1, constructed wetlands (scenario W2)  
201 had the lowest CFP (1.6 and 0.9 kg CO<sub>2</sub>eq m<sub>water</sub><sup>-3</sup> during the vintage season and the rest  
202 of the year, respectively), while the third-party management (scenario W1) had the  
203 highest CFP (around 50 kg CO<sub>2</sub>eq m<sub>water</sub><sup>-3</sup> during both seasons considered). The activated  
204 sludge system (scenario W3) had a CFP of 5.9 and 3.2 kg CO<sub>2</sub>eq m<sub>water</sub><sup>-3</sup> during the  
205 vintage season and the rest of the year, respectively. This means that constructed wetlands  
206 helped to reduce the CFP associated with winery wastewater management by 70-98%  
207 compared to the conventional solutions. This was in accordance with previous studies  
208 which highlighted that constructed wetlands had lower GHG emissions and less

209 environmental impacts than conventional plants treating urban and industrial wastewater  
210 (Garfí et al., 2017; Ingrao et al., 2020).

211 The CFP for the third-party management (scenario W1) did not show significant  
212 fluctuations over the year, since in this solution wastewater is stored and transported by  
213 a third-party once per month. On the contrary, the CFPs generated during the vintage  
214 season were higher (around 2 times) than those generated during the rest of the year for  
215 the constructed wetland and activated sludge systems (scenarios W2 and W3). As  
216 mentioned above, winery wastewater is characterized by fluctuations in terms of quality  
217 and quantity over the year. In particular, flow rates and organic loadings generated during  
218 the vintage season were up to 10 times higher than those produced during the rest of the  
219 year, when winery effluents are comparable to urban wastewater (Flores et al., 2019a).  
220 For this reason, during the vintage season, direct GHG emissions, as well as electricity  
221 and chemicals consumption, were higher than those generated during the rest of the year  
222 (Table 3 and 4).

223 As shown in Figure 2, the CFP of the third-party management (scenario W1) was  
224 mostly associated with wastewater transportation and disposal (99% of the overall CFP).  
225 On the other hand, the CFP of the constructed wetland system (scenario W2) was mainly  
226 due to direct GHG emissions (5 and 30% of the overall CFP during the rest of the year  
227 and the vintage season respectively), the additional effluent treatment at the municipal  
228 wastewater treatment plant (56 and 35%, of the overall CFP during the rest of the year  
229 and the vintage season, respectively) and construction materials (30 and 19% of the  
230 overall CFP during the rest of the year and the vintage season, respectively). These results  
231 were in accordance with recent studies which stated that the environmental impact of  
232 constructed wetlands treating urban wastewater was mainly due to direct GHG emissions

233 and construction materials (around 30% of the overall impacts for each of them) (Diaz-  
234 Elsayed et al., 2020; Resende et al., 2019).

235 In the case of the activated sludge system (scenario W3), the CFP was mainly  
236 influenced by chemicals and electricity consumption (around 45% and 12% of the overall  
237 CFP during both seasons, respectively), as well as sludge transportation and disposal  
238 (around 15% of the overall CFP for both seasons). This was in accordance with previous  
239 studies which observed that chemicals and electricity consumption, as well as wastewater  
240 and sludge transportation, generated the highest environmental impacts in conventional  
241 wastewater treatment plants (Flores et al., 2019a; Lehtoranta et al., 2014). In particular,  
242 electricity consumption and the transport of sludge to centralized treatment were found  
243 to be the major causes of the environmental impacts of different conventional municipal  
244 wastewater treatment options (e.g. dry toilets, greywater treatment, biofilters and sludge  
245 bed reactors) in Finland (Lehtoranta et al., 2014). This study also suggested that the  
246 footprints of the sludge management options could be reduced by not transporting the  
247 sludge to the centralized wastewater treatment plant but by composting it on-site or by  
248 applying it to farmlands. In this context, sludge treatment wetlands can be implemented  
249 to avoid sludge transportation and thus, reducing the environmental impacts associated  
250 with it (Flores et al., 2019a).

251 Although in the constructed wetland system (scenario W2) direct GHG emissions  
252 generated and measured in the plants had a high contribution, in the third-party  
253 management (scenario W1) and the activated sludge system (scenario W3) they  
254 accounted for less than 1% of the overall CFP (Figure 2). Indeed, in scenario W1 and W3  
255 indirect GHG emissions due to wastewater and sludge transportation as well as electricity  
256 consumption had the highest contribution (Figure 2). This was in accordance with

257 previous studies which analysed the CFP of different conventional wastewater treatment  
258 plants (Caivano et al., 2017; Chai et al., 2015). Moreover, it has to be mentioned that  
259 winery wastewater had a low content of nitrogen and thus, lower N<sub>2</sub>O emissions were  
260 released in the treatment systems in comparison to municipal wastewater treatment plants  
261 (Flores et al., submitted). For this reason, the contribution of direct GHG emissions to the  
262 overall CFP in conventional systems treating urban wastewater found in literature was  
263 higher (up to 70%) than in the present study (Chetty and Pillay, 2015; Delre et al., 2019;  
264 Longo et al., 2017). This means that direct GHG emissions and CFP depend not only on  
265 the technology used, but also on the wastewater quality. Thus, the results of this study  
266 confirmed the importance of measuring direct GHG emissions on-site (Gallego-Schmid  
267 and Zepon-Tarpani, 2019; Flores et al., 2019; Maktabifard et al., 2020; Nguyen et al.,  
268 2020). Indeed, previous studies stated that real measurements and transparency in the  
269 calculation methods applied should be encouraged and that it is vital to create a complete  
270 and reliable database to improve the overall quality of the CFP (Gallego-Schmid and  
271 Zepon-Tarpani, 2019; Nguyen et al., 2020).

272 In summary, the annual average CFP of the constructed wetland system (scenario  
273 W2) was 1.2 kg CO<sub>2</sub>eq m<sub>water</sub><sup>-3</sup>. This value was around 42 and 4 times lower than the  
274 third-party (scenario W1) (52 kg CO<sub>2</sub>eq m<sub>water</sub><sup>-3</sup>) and the activated sludge scenarios  
275 (scenario W3) (4.5 kg CO<sub>2</sub>eq m<sub>water</sub><sup>-3</sup>), respectively. This was mainly due to the high GHG  
276 emissions generated by wastewater and sludge transportation, as well as chemicals and  
277 electricity consumption, in the third-party and activated sludge scenarios compared to the  
278 constructed wetlands. This is in accordance with previous studies which observed that  
279 constructed wetland systems helped to reduce environmental impacts associated with

280 wastewater treatment compared with conventional technologies (Casas-Ledón et al.,  
281 2017; Flores et al., 2019; Garfí et al., 2017; Yildirim and Topkaya, 2012).

282 In conclusion, constructed wetlands are environmentally friendly technologies  
283 which help to reduce CFP associated with winery wastewater treatment, by treating  
284 winery waste on-site with low energy and chemicals requirements.

285

### 286 **3.2 Economic analysis**

287 The results of the economic analysis are shown in Table 5. As expected, the capital cost  
288 of the third-party (scenario W1) appeared to be the lowest, due to the lower amount of  
289 materials required for the construction of the wastewater storage tank. On the other hand,  
290 the capital cost of constructed wetlands (scenario W2) and activated sludge system  
291 (scenario W3) was similar. It is due to the fact that the latter treated a flow which is around  
292 3.5 times higher than that treated by the former (Table 1). Indeed, it was observed that  
293 the smaller the size of the wastewater treatment plant the higher the capital cost per cubic  
294 meter of treated water (Acampa et al., 2019). If the constructed wetlands (scenario W2)  
295 treated the same flow as the activated sludge system (scenario W3) considered in this  
296 study, the capital cost of the former would be reduced by 50% (around 1 €m<sup>-3</sup>), which is  
297 in accordance with previous studies (Corbella et al., 2017).

298 Regarding operation and maintenance, the activated sludge system (scenario W3)  
299 had the highest cost followed by the third-party alternative (scenario W1). It was mainly  
300 due to the high cost associated with chemicals and electricity consumption, as well as  
301 wastewater and sludge transportation and disposal. The constructed wetlands system  
302 (scenario W2) presented a very low operation and maintenance cost (up to 60 times lower  
303 compared to the other scenarios) due to their small energy requirements.

304 In conclusion, the constructed wetland system was shown to be a low-cost  
305 technology which would reduce the capital, operation and maintenance costs associated  
306 with winery wastewater treatment up to 50 and 98%, respectively.

307

#### 308 **4. Conclusions**

309 This study assessed the carbon footprint (CFP) of constructed wetlands for winery  
310 wastewater treatment. In particular, the constructed wetland scenario was compared to  
311 the previous scenario (third-party management) and to an activated sludge system.  
312 Moreover, an economic analysis was also addressed. The results showed that the  
313 constructed wetland scenario had the lowest CFP ( $1.2 \text{ kg CO}_2\text{eq m}_{\text{water}}^{-3}$ ), while the third-  
314 party management was the worst scenario followed by the activated sludge system.  
315 Specifically, the CFP of the constructed wetland scenario was 42 and 4 times lower than  
316 the third-party and the activated sludge scenarios, respectively. This was mainly due to  
317 the high GHG emissions generated by wastewater and sludge transportation, as well as  
318 chemicals and electricity consumption in the third-party and activated sludge scenarios  
319 compared to the constructed wetlands.

320 From an economic point of view, constructed wetland system was shown to be a  
321 low-cost technology which reduces the capital, operation and maintenance costs  
322 associated with winery wastewater treatment up to 50 and 98%, respectively.

323 In conclusion, constructed wetlands are low-cost and environmentally friendly  
324 technologies which constitute a sustainable alternative to conventional solutions for  
325 winery wastewater treatment.

326

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336

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524

525 **Table 1.** Main characteristics of the wineries and their wastewater treatment systems and management strategies considered in this study

	Unit	Scenarios	
		W1 and W2	W3
<i>General data</i>			
Location	-	Galicia (Spain)	Galicia (Spain)
Total wine production	L y <sup>-1</sup>	368,000	3,850,000
Vintage season duration	d y <sup>-1</sup>	26	15
<i>Wastewater treatment and management</i>			
<i>Wastewater flows</i>			
Total	m <sup>3</sup> y <sup>-1</sup>	1,400	4,832
Vintage season	m <sup>3</sup> during the vintage season	620	2,416
Rest of the year	m <sup>3</sup> during the rest of the year	780	2,416
Wastewater treatment/management alternatives	-	W1: third-party management (previous scenario) W2: constructed wetlands (current scenario)	Activated sludge system
Sludge management	-	W1: third-party management (previous scenario) W2: sludge treatment wetlands (current scenario)	Third-party management
<i>Wastewater quality characteristics (vintage season)</i>			
pH	-	5	7
COD	mg L <sup>-1</sup>	1,031	11,957
BOD <sub>5</sub>	mg L <sup>-1</sup>	650	4,110
TSS	mg L <sup>-1</sup>	706	2,190
TN	mg L <sup>-1</sup>	9.7	-
TP	mg L <sup>-1</sup>	1.5	-
<i>Wastewater quality characteristics (rest of the year)</i>			
pH	-	6.5-7.5	6.5-7.5
COD	mg L <sup>-1</sup>	< 500	< 2,000
BOD <sub>5</sub>	mg L <sup>-1</sup>	< 250	< 1,000
TSS	mg L <sup>-1</sup>	< 200	< 1,000
TN	mg L <sup>-1</sup>	< 20	-
TP	mg L <sup>-1</sup>	< 10	-

526 Note: COD: Chemical Oxygen Demand; BOD<sub>5</sub>: Biochemical Oxygen Demand; TSS: Total Suspended Solids; TN: Total Nitrogen; TP: Total Phosphorous. The W2  
527 scenario consisted of a constructed wetland system recently implemented in the same winery as the W1 scenario, in order to replace the third-party management (W1).

528

529 **Table 2.** Inventory results referred to the functional unit (1 m<sup>3</sup> of treated water) for the construction of the wastewater treatment systems

530

	Unit	Scenarios		
		W1	W2	W3
<b>Inputs</b>				
Concrete	m <sup>3</sup> m <sup>-3</sup>	1.011E-03	1.339E-04	1.244E-03
Reinforcing steel	kg m <sup>-3</sup>	6.943E-02	7.340E-03	1.244E-01
Steel	kg m <sup>-3</sup>	2.336E-04	1.170E-03	6.766E-05
Copper	kg m <sup>-3</sup>	3.507E-04	1.756E-03	1.016E-04
Cast iron	kg m <sup>-3</sup>	7.014E-04	3.512E-03	2.032E-04
PVC	kg m <sup>-3</sup>	-	6.385E-03	6.207E-04
Gravel	m <sup>3</sup> m <sup>-3</sup>	-	1.967E-03	-
Sand	m <sup>3</sup> m <sup>-3</sup>	-	2.145E-04	-
Geotextile	kg m <sup>-3</sup>	-	2.989E-03	-
Geomembrane	kg m <sup>-3</sup>	-	6.401E-03	-
Polyethylene	kg m <sup>-3</sup>	-	3.755E-02	-
Glass fibre reinforced plastic	kg m <sup>-3</sup>	-	6.705E-03	-

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*Scenarios: W1: third-party management; W2: constructed wetland system; W3: activated sludge system.*

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535 **Table 3.** Inventory results referred to the functional unit (1 m<sup>3</sup> of treated water) for the operation of the wastewater treatment systems and  
 536 management during the vintage season

	Unit	Scenarios		
		W1	W2	W3
<b>Inputs</b>				
Electricity	kWh m <sup>-3</sup>	0.000E+00	5.032E-01	2.000E+00
Flocculant	kg m <sup>-3</sup>	-	-	1.242E-01
Sodium hydroxide	kg m <sup>-3</sup>	-	-	4.139E-01
Urea	kg m <sup>-3</sup>	-	-	6.623E-01
Phosphoric acid	kg m <sup>-3</sup>	-	-	4.139E-01
<b>Outputs</b>				
Sludge	kg m <sup>-3</sup>	-	-	9.934E+00
Sludge transportation	tkm m <sup>-3</sup>	-	-	1.490E+00
Wastewater transportation	tkm m <sup>-3</sup>	2.400E+02	-	-
<i>Direct emissions to air (released by wastewater treatment systems)</i>				
CO <sub>2</sub>	g m <sup>-3</sup>	1.034E+01	2.080E+03	2.394E+02
CH <sub>4</sub>	g m <sup>-3</sup>	1.893E-01	1.142E+01	4.477E-01
N <sub>2</sub> O	g m <sup>-3</sup>	6.553E-03	6.775E-01	8.532E-02
<i>Direct emissions to air (due to fertilizer application to soil)</i>				
CH <sub>4</sub>	g m <sup>-3</sup>	-	9.518E-01	-
N <sub>2</sub> O	g m <sup>-3</sup>	-	8.848E-02	-
<i>Avoided products</i>				
N as Fertiliser (from sludge reuse as fertilizer)	g m <sup>-3</sup>	-	7.373E+00	-
P as Fertiliser (from sludge reuse as fertilizer)	g m <sup>-3</sup>	-	4.074E+00	-

537 *Scenarios: W1: third-party management; W2: constructed wetland system; W3: activated sludge system.*

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542 **Table 4.** Inventory results referred to the functional unit (1 m<sup>3</sup> of treated water) for the operation of the wastewater treatment systems and  
 543 management during the rest of the year.

	Unit	Scenarios		
		W1	W2	W3
<b>Inputs</b>				
Electricity	kWh m <sup>-3</sup>	0.000E+00	1.743E-01	6.900E-01
Flocculant	kg m <sup>-3</sup>	-	-	1.034E-01
Sodium hydroxide	kg m <sup>-3</sup>	-	-	1.241E-01
Urea	kg m <sup>-3</sup>	-	-	3.310E-01
Phosphoric acid	kg m <sup>-3</sup>	-	-	2.069E-01
<b>Outputs</b>				
Sludge	kg m <sup>-3</sup>	-	-	4.137E+00
Sludge transportation	tkm m <sup>-3</sup>	-	-	6.206E-01
Wastewater transportation	tkm m <sup>-3</sup>	2.400E+02	-	-
<i>Direct emissions to air (released by wastewater treatment systems)</i>				
CO <sub>2</sub>	g m <sup>-3</sup>	1.034E+01	1.230E+02	2.823E+02
CH <sub>4</sub>	g m <sup>-3</sup>	1.893E-01	1.969E+00	2.079E-01
N <sub>2</sub> O	g m <sup>-3</sup>	6.553E-03	1.160E-02	7.631E-02
<i>Direct emissions to air (due to fertilizer application to soil)</i>				
CH <sub>4</sub>	g m <sup>-3</sup>	-	9.518E-01	-
N <sub>2</sub> O	g m <sup>-3</sup>	-	8.848E-02	-
<i>Avoided products</i>				
N as Fertiliser (from sludge reuse as fertilizer)	g m <sup>-3</sup>	-	7.373E+00	-
P as Fertiliser (from sludge reuse as fertilizer)	g m <sup>-3</sup>	-	4.074E+00	-

544 *Scenarios: W1: third-party management; W2: constructed wetland system; W3: activated sludge system.*

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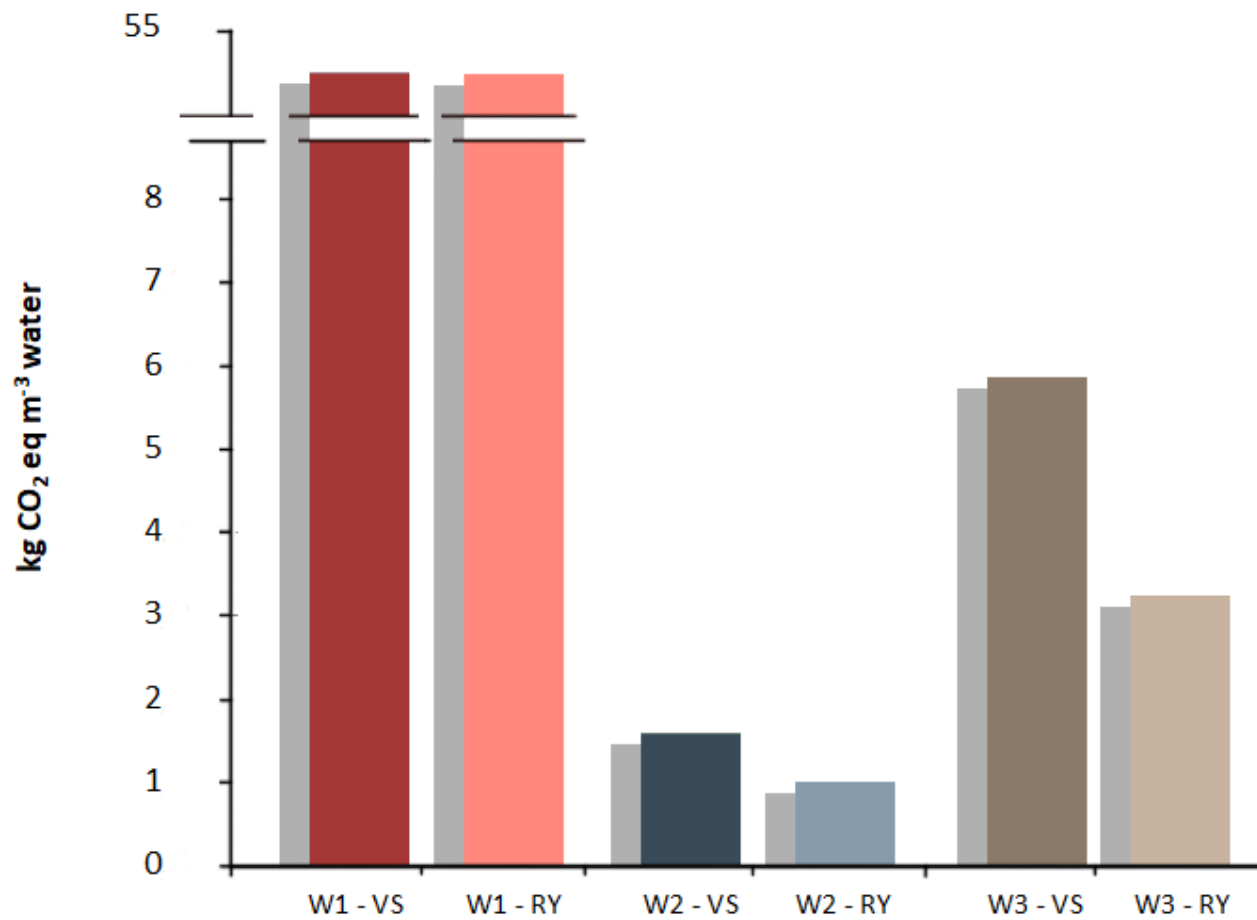
**Table 5.** Capital and operation and maintenance costs of the considered scenarios expressed in terms of euros per cubic meter of treated water

	Unit	Scenarios		
		W1	W2	W3
Capital cost	€m <sup>-3</sup>	0.20	2.30	2.58
Operation and maintenance cost	€m <sup>-3</sup>	1.76	0.04	2.49

*Scenarios: W1: third-party management; W2: constructed wetland system; W3: activated sludge system.*

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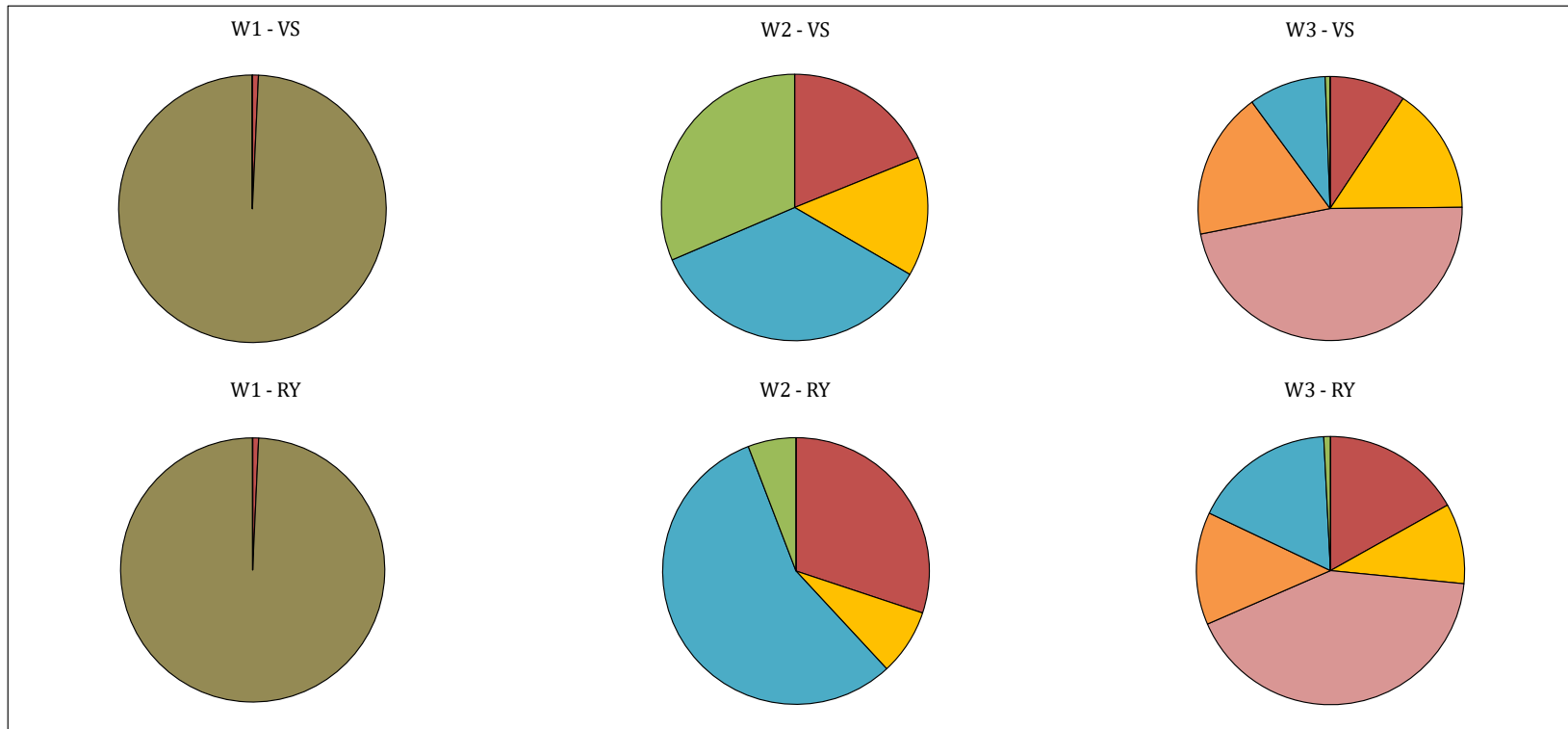




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**Figure 1.** Carbon footprint of the three scenarios considered during the vintage season (VS) and the rest of the year (RY). Values are referred to the functional unit (1 m<sup>3</sup> of treated water). Scenarios: W1: third-party management; W2: constructed wetland system; W3: activated sludge system.

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■ Construction materials  
■ Third-party wastewater transportation and disposal  
■ Fertilizer avoided and application to soil  
■ Electricity  
■ Third-party sludge transportation and disposal  
■ Direct emissions to air  
■ Chemicals  
■ Treatment at municipal wastewater treatment plant

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**Figure 2.** Contribution analysis for the three scenarios considered during the vintage season (VS) and the rest of the year (RY). Scenarios: W1: third-party management; W2: constructed wetland system; W3: activated sludge system.