

# POLYTECHNICAL UNIVERSITY OF CATALONIA

## AEROSPACE ENGINEERING

# ANNEX: Design of an azimuth/elevation mount for Sun-tracking of a solar panel

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#### A Radiation for different Sun-tracking PV

This appendix presents the code used to perform the radiation study, which is discussed in section 4.1.

```
1 % Radiation study script
2
3
  % Control parameters
  phi = 12.3; % Latitude [deg]
  lambda = -1.53388; %Longitude [deg]
\mathbf{5}
  load ('Database irradiance \ Horizontal direct radiation 2
6
      . mat ')
  load ('Database_irradiance \ Horizontal_difuse_radiation_2
\overline{7}
      . mat ')
  load ('Database irradiance k factor 2.mat')
8
9
  %Official time
10
  UTC = 0:0.0625:23;
11
12
  %Day of the year
13
  day = 15:30:345 ;
14
15
  % Declination of Sun [deg]
16
  deltas = 23.45 * sind((360 * (day + 284)) / 365);
17
18
  % Solar time parameters
19
 M = (2*pi*day)/365.24;
20
 EoT = 229.18 * (-0.0334 * \sin (M) + 0.04184 * \sin (2*M + M))
21
      3.5884));
_{22} GMT = 0 ;
  AO = 0;
23
  var_lambda = lambda - GMT*15;
^{24}
25
  % Preallocate omegas
26
  omegas = NaN(length(day), length(UTC));
27
28
  %Solar time [deg]
29
30
```

```
for k = 1: length (day)
31
                       for t = 1: length (UTC)
32
                                     omegas (k, t) = 15 * (UTC(t) - AO - 12) +
33
                                               var lambda + (EoT(k)/4);
                       end
34
        end
35
36
       % Preallocate vars
37
        theta zss = NaN(length(day), length(omegas));
38
        psi ss = NaN(length(day), length(omegas));
39
        theta s = NaN (4, length(day), length(omegas));
40
41
         for t = 1:4
42
43
                       for j = 1: length (day)
44
45
                                     for i = 1: length(omegas)
46
                                                  %Current hour angle and declination
47
                                                   omega = omegas(j, i);
48
                                                    delta = deltas(j);
49
50
                                                  % Pre-compute some parameters for
51
                                                              performance
                                                   cosd phi = cosd(phi);
52
                                                   sind phi = sind(phi);
53
                                                    cosd delta = cosd(delta);
54
                                                    sind delta = sind(delta);
55
                                                   \cos d \cos d = \cos d (\operatorname{omega});
56
                                                   sind_omega = sind(omega);
57
58
                                                  % Compute Zenith angle
59
                                                    \cos d theta zs = (\cos d delta * \cos d omega * delta * cos d omega * 
60
                                                              cosd _phi) + (sind_delta * sind_phi);
                                                   sind theta zs = sind(acosd(cosd theta zs));
61
                                                    theta zs = acosd(cosd theta zs);
62
63
                                                  % Compute azimuth angle
64
```

```
sind psi s = (\cos d delta * \sin d omega) /
65
                   sind theta zs;
                cosd_psi_s = (cosd_delta * cosd_omega *
66
                   sind phi – cosd phi * sind delta) /
                   sind_theta zs;
67
                % Get correct value of angle psi s
68
                psi s = asind(sind psi s);
69
70
                if \cos d \ psi \ s < 0
71
                    if sind_{psi_s} > 0, psi_s = 180 - psi_s;
72
                    elseif sind psi s < 0, psi s = -180 -
73
                       psi_s;
                    else, psi_s = psi_s + 180;
74
                    end
75
                end
76
77
           % Save angle values
78
           theta zss(j,i) = theta zs; \% Zenith angle
79
           psi ss(j,i) = psi s; \% Azimuth angle
80
81
           if t = 1 %CASE 1: static panel
82
                beta = 3.7 + 0.69 * phi; %optimal tilt
83
                   angle
                alfa = 0; % pointing to N-S axis
84
85
            elseif t = 2 % CASE 2: azimuth 1-axis panel
86
87
                beta = phi ; %optimal tilt angle
88
                alfa = psi s ;
89
90
            elseif t = 3 % CASE 3: horizontal 1-axis panel
91
                beta = theta zs;
92
93
                if day(j) > 114 \&\& day(j) < 232
94
                    alfa = 180;
95
                else
96
                    alfa = 0;
97
```

end 98 99 %CASE 4: 2-axis panel else 100 beta = theta zs; 101 alfa = psi s ;102 end 103 104%Angle between Sun and PV panel 105theta s = (sign(phi) \* (sind(beta) \* cosd(alfa)))106 \*cosd (delta)\*cosd (omega)\*sind (phi)... - sind (beta) \* cosd (alfa) \* cosd (phi) 107 \*sind(delta))... + (sind(beta) \* sind(alfa) \* cosd(108 delta) \* sind (omega)) ... +  $(\cos d (beta) * \cos d (delta) * \cos d (delta)$ 109  $omega) * cosd(phi)) \dots$ +  $(\cos d(beta) * \sin d(delta) * \sin d($ 110phi))); 111 G b(j, i, t) = (B(j, i) \* max(0, theta s)) / (112cosd\_theta\_zs) ;  $G_d(j, i, t) = (D(j, i) * (1 - k_factor(j, i)) * ((1 + k_factor(j, i))) * ((1 + k_factor(j, i)$ 113  $\cos d(beta))/(2)) + ( (D(j,i)*k factor(j,i))$  $*\max(0, \text{theta s}))/(\cos d \text{ theta zs}));$ G(j, i, t) = G b(j, i, t) + G d(j, i, t); 114 end 115116end 117118 end 119 120S = sum(G) / 12; 121  $dry\_season = (G(1,:,:) + G(2,:,:) + G(3,:,:) + G(3,::) + G(3$ 122(4,:,:) + G(5,:,:) + G(10,:,:) + G(11,:,:) + G(12, :, :) ) / 8 ;rainy\_season = (G(6,:,:) + G(7,:,:) + G(8,:,:) + G(8,:,:))123(9, :, :) ) / 4 ;

124

jan = G(1, :, :); feb = G(2, :, :)126mar = G(3, :, :)127apr = G(4, :, :); 128may = G(5, :, :)129jun = G(6, :, :)130jul = G(7, :, :)131 aug = G(8, :, :)132sep = G(9, :, :)133 oct = G(10, :, :)134nov = G(11, :, :)135dec = G(12, :, :); 136 137for j = 1:4138 139for i = 1 : (length(omegas)-1)140141  $dA_dry(i,j) = ((dry_season(1,i+1,j) +$ 142dry season (1, i, j) ) \* (UTC(i+1)-UTC(i)) / 2; $dA_rainy(i,j) = ((rainy_season(1,i+1,j) +$ 143 $rainy\_season(1, i, j)$  \* (UTC(i+1)–UTC(i)) / 2 ;144 $dA_jan(i,j) = ((jan(1,i+1,j) + jan(1,i,j))) *$ 145(UTC(i+1)-UTC(i)) / 2 ;dA feb(i,j) = ((feb(1,i+1,j) + feb(1,i,j)) \*146(UTC(i+1)-UTC(i))) / 2; $dA_mar(i, j) = ((mar(1, i+1, j) + mar(1, i, j))) *$ 147(UTC(i+1)-UTC(i)) / 2 ;dA apr(i,j) = ((apr(1,i+1,j) + apr(1,i,j))) \*148(UTC(i+1)-UTC(i)) / 2 ; $dA_may(i, j) = ((may(1, i+1, j) + may(1, i, j))) *$ 149(UTC(i+1)-UTC(i))) / 2; $dA_jun(i,j) = ((jun(1,i+1,j) + jun(1,i,j)) *$ 150(UTC(i+1)-UTC(i)) / 2 ; $dA_jul(i,j) = ((jul(1,i+1,j) + jul(1,i,j)) *$ 151(UTC(i+1)-UTC(i)) / 2 ;

125

 $dA_aug(i, j) = ((aug(1, i+1, j) + aug(1, i, j)) *$ 152(UTC(i+1)-UTC(i))) / 2; $dA_sep(i,j) = ((sep(1,i+1,j) + sep(1,i,j)) *$ 153(UTC(i+1)-UTC(i)) / 2 ; $dA_oct(i, j) = ( (oct(1, i+1, j) + oct(1, i, j)) *$ 154(UTC(i+1)-UTC(i))) / 2 $dA_nov(i, j) = ((nov(1, i+1, j) + nov(1, i, j)) *$ 155(UTC(i+1)-UTC(i)) / 2 ; $dA \ dec(i,j) = ((dec(1,i+1,j) + dec(1,i,j))) *$ 156(UTC(i+1)-UTC(i)) / 2 ;157end 158159end 160 161A dry = sum (dA dry, 1); 162A rainy = sum (dA rainy, 1); 163 164A jan = sum (dA jan, 1) 165A feb = sum (dA feb, 1); 166 A mar = sum (dA mar, 1) 167A apr = sum (dA apr, 1) 168  $A_{may} = sum (dA may, 1)$ 169 A jun = sum (dA jun, 1)170A jul = sum (dA jul, 1) 171A aug = sum (dA aug, 1)172A sep = sum (dA sep, 1) 173 $A_{oct} = sum (dA oct, 1)$ 174A nov = sum (dA nov, 1)175A dec = sum (dA dec, 1) 176 : 177 $kWh_meses = [A_jan; A_feb; A_mar; A_apr; A_may; A_jun; A_jul;$ 178 A  $\operatorname{aug}$ ; A  $\operatorname{sep}$ ; A  $\operatorname{oct}$ ; A  $\operatorname{nov}$ ; A  $\operatorname{dec}$ ];  $\min rad = \min (kWh meses)$ ; 179180 %INSTALLATION 181 %Consumo equipo 182 C = 1000:2000:11000; 183

```
184
   %Rendimiento instalacion
185
   eta = 0.75;
186
   E = C ./ eta ;
187
188
   %Hora solar pico
189
   \mathbf{x} = 4; %Tipo de tracker: 1) Static, 2) Azimuth, 3) Horiz, 4)
190
      2-axis
   HSP = \min rad(x) / 1000 ;
191
192
   %Numero de modulos
193
   p = 0.8; %perdidas ensuciamiento
194
   W = 50:1:450;
195
196
   for i=1:length(E)
197
        for j=1:length(W)
198
            N(i, j) = (E(i)) / (HSP * p * W(j));
199
        end
200
   end
201
202
   E_{ob} = (6 * HSP * p * 340) * eta ;
203
204
   %Capacidad acumuladores
205
   dias_autonomia = 1:1:4;
206
   V = 24;
207
   descarga = 0.5:0.01:0.8;
208
209
   for j=1:length(E)
210
211
        for i=1:length(dias_autonomia)
212
213
             for k=1:length(descarga)
214
215
            A(j,k,i) = (E(j) * dias autonomia(i)) / (V*)
216
                descarga(k));
217
             end
218
        end
219
```

220 end

### B Monthly global irradiance comparison

This appendix presents the monthly comparison between different tracker systems, which are discussed in section 4.1.











#### C Solar geometry in Burkina Faso

This appendix presents the azimuth and zenith angle values for a year in Burkina Faso. The results are discussed in section 4.3.2.

```
<sup>1</sup> % Solar geometry
2
  % Control parameters
3
  phi = ; \% Latitud [deg]
  omegas = -180:1:180; % Hora solar [deg] [-180,180]
5
  days = 1:1:365; % Dia any [1,365]
6
7
  % Preallocate arrays
8
  zenmd = NaN(length(days), 1); \% Zenith at midday
9
  azmd = NaN(length(days), 1); \% Azimuth at midday
10
  deltas = NaN(length(days), 1); \% Sun declination
11
12
  % Loop days
13
  for k = 1: length (days)
14
15
      % Day
16
       day = days(k);
17
18
      % Declination of Sun [deg]
19
       delta = 23.45 * sind((360 * (day + 284)) / 365);
20
       deltas(k) = delta;
21
22
      % Preallocate vars
23
       theta zss = NaN(length(omegas), 1);
24
       psi ss = NaN(length(omegas), 1);
25
26
      % Loop solar hour angle
27
       for i=1:length (omegas)
28
29
           % Current hour angle
30
           omega = omegas(i);
31
32
           % Pre-compute some parameters for performance
33
```

cosd phi = cosd(phi);34 sind phi = sind(phi);35 $\cos d = \operatorname{cosd} (\operatorname{delta});$ 36 sind delta = sind(delta); 37 cosd omega = cosd(omega);38 sind omega = sind(omega);39 40% Compute Zenith angle 41 $\cos d$  theta  $zs = (\cos d delta * \cos d omega * delta * cos d omega *$ 42 $\cos d_{phi}$  +  $(\sin d_{delta} * \sin d_{phi});$ sind theta zs = sind(acosd(cosd theta zs));43theta zs = acosd(cosd theta zs);44 45% Compute azimuth angle 46 sind psi s =  $(\cos d delta * \sin d omega) /$ 47sind theta zs;  $\cos d psi s = (\cos d delta * \cos d omega *$ 48 sind phi - cosd phi \* sind delta) / sind theta zs; 49% Get correct value of angle psi\_s 50 $psi_s = asind(sind_psi_s);$ 51if  $\cos d$  psi s < 0 52if  $sind_{psi_s} > 0$ ,  $psi_s = 180 - psi_s$ ; 53 $elseif sind_{psi_s} < 0, psi_s = -180 - psi_s$ 54; else, psi s = psi s + 180;55end 56end 5758% Save angle values 59theta zss(i) = theta zs; % Zenith angle 60  $psi_s(i) = psi_s; \%$  Azimuth angle 61 62 end 63 64 % Get minimum zenith 65

```
\operatorname{zenmd}(k) = \min(\operatorname{theta} \operatorname{zss}); \% Minimum Zenith (sun is
66
            highest on sky)
       idxmd = find(theta zss = zenmd(k)); % Index at min
67
           zenith
       azmd(k) = psi ss(idxmd); \% Azimuth at min zenith
68
69
   end
70
71
  \% Plot min zenith + azimuth vs day of year
72
   figure(); hold on; grid on; box on;
73
   xlabel('Day of the year');
74
  \operatorname{xlim}(\operatorname{days}([1, \operatorname{end}]));
75
   xticks ([1,30:30:365]);
76
77
   yyaxis left;
   plot (days, zenmd, '. ');
78
   ylabel ('Minimum Zenith angle [deg] (0 is up, 180 is
79
      \operatorname{down})');
   yyaxis right;
80
   plot (days, azmd, 'x');
81
   ylabel('Azimuth angle at min zenith [deg] (0 is south,
82
      180 is north)');
83
  % Plot sun declination vs day of year
84
  figure(); hold on; grid on; box on;
85
   xlabel('Day of the year');
86
  xlim(days([1, end]));
87
   xticks ([1,30:30:365]);
88
   plot(days, deltas, '. '); % Sun declination
89
   plot (days, 0*days+phi, '---'); % Latitud geografica
90
ylabel('Sun declination angle [deg]');
  legend ('Sun Declination', 'Geographic Latitude');
92
```

## D Bolt geometry tables

This appendix presents bolt geometry tables, which are used in section 5.5. Both tables have been adapted from *Uniones*, Universidade da Coruña.

|  | M 10   | M 12 | M 16 | M 20 | M 22 | M 24 | M 27 | M 30 | M 33 | M 36 |
|--|--|------|------|------|------|------|------|------|------|------|
| longitud<br>nominal<br>/ (mm)                          | longitud de la caña<br><i>I<sub>g</sub></i> (mm) |      |      |      |      |      |      |      |      |      |
| 30   | 10   | 8    |      |      |      |      |      |      |      |      |
| 35   | 15   | 13   | 9    |      |      |      |      |      |      |      |
| 40   | 20   | 18   | 14   | 10   | 8    |      |      |      |      |      |
| 45   | 25   | 23   | 19   | 15   | 13   | 11   |      |      |      |      |
| 50   | 30   | 28   | 24   | 20   | 18   | 16   |      |      |      |      |
| 55   | 35   | 33   | 29   | 25   | 23   | 21   |      |      |      |      |
| 60   | 40   | 38   | 34   | 30   | 28   | 26   | 23   |      |      |      |
| 65   | 45   | 43   | 39   | 35   | 33   | 31   | 28   |      |      |      |
| 70   | 50   | 48   | 44   | 40   | 38   | 36   | 33   |      |      |      |
| 75   | 55   | 53   | 49   | 45   | 43   | 41   | 38   |      |      |      |
| 80   |  | 58   | 54   | 50   | 48   | 46   | 43   | 40   |      |      |
| 85   |  | 63   | 59   | 55   | 53   | 51   | 48   | 45   |      |      |
| 90   |  | 68   | 64   | 60   | 58   | 56   | 53   | 50   |      |      |
| (95)   |  | 73   | 69   | 65   | 63   | 61   | 58   | 55   |      |      |
| 100  |  | 78   | 74   | 70   | 68   | 66   | 63   | 60   | 57   | 54   |
| (105)  |  | 83   | 79   | 75   | 73   | 71   | 68   | 65   | 62   | 59   |
| 110  |  | 88   | 84   | 80   | 78   | 76   | 73   | 70   | 67   | 64   |
| (115)  |  | 93   | 89   | 85   | 83   | 81   | 78   | 75   | 72   | 69   |
| 120  |  | 98   | 94   | 90   | 88   | 86   | 83   | 80   | 77   | 74   |
| (125)  |  |      | 99   | 95   | 93   | 91   | 88   | 85   | 82   | 79   |
| 130  |  |      | 104  | 100  | 98   | 96   | 93   | 90   | 87   | 84   |
| 140  |  |      | 114  | 110  | 108  | 106  | 103  | 100  | 97   | 94   |
| 150  |  |      | 124  | 120  | 118  | 116  | 113  | 110  | 107  | 104  |
| 160  |  |      |      | 130  | 128  | 126  | 123  | 120  | 117  | 114  |
| 170  |  |      |      | 140  | 138  | 136  | 133  | 130  | 127  | 124  |
| 180  |  |      |      |      | 148  | 146  | 143  | 140  | 137  | 134  |
| 190  |  |      |      |      | 158  | 156  | 153  | 150  | 147  | 144  |
| 200  |  |      |      |      | 168  | 166  | 163  | 160  | 157  | 154  |
| Se evitarán en lo posible los valores entre paréntesis |  |      |      |      |      |      |      |      |      |      |

| TIPO   | vástago |        | área<br>resistente |        |              |  |
|--------|---------|--------|--------------------|--------|--------------|--|
|        | d (mm)  | k (mm) | s (mm)             | e (mm) | $A_s (cm^2)$ |  |
| M 10   | 10      | 7      | 17                 | 19,6   | 0,580        |  |
| M 12   | 12      | 8      | 19                 | 21,9   | 0,843        |  |
| M 16   | 16      | 10     | 24                 | 27,7   | 1,570        |  |
| M 20   | 20      | 13     | 30                 | 34,6   | 2,450        |  |
| (M 22) | 22      | 14     | 32                 | 36,9   | 3,030        |  |
| M 24   | 24      | 15     | 36                 | 41,6   | 3,530        |  |
| (M 27) | 27      | 17     | 41                 | 47,3   | 4,560        |  |
| M 30   | 30      | 19     | 46                 | 53,1   | 5,610        |  |
| (M 33) | 33      | 21     | 50                 | 57,7   | 6,940        |  |
| M 36   | 36      | 23     | 55                 | 63,5   | 8,170        |  |