

Decentralized Shaping for Pilot Generation and Detection in Opportunistic Communications

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Abstract—The uncoordinated design of pulse shaping filters for opportunistic communications is addressed. We show that under degrees-of-freedom sensing uncertainties the waveform design problem can be cast as a minimum-norm optimization, admitting hence a closed-form expression. Because designed waveforms are adapted to scenario working conditions, proposed design scheme may be considered in pilot reference signals design to achieve orthogonality, regardless the traditionally considered pilot symbols orthogonality. Hence, the effect of interferences such as pilot contamination is diminished. However, a crucial aspect relies on their detectability. Since each node uses only local observations from the wireless network, the sensed degrees-of-freedom may slightly differ from one node to others. In this paper we prove that, thanks to the existence of some *invariances*, designed waveforms can be detected by neighboring nodes. Even though degrees-of-freedom sensing uncertainties may incur in a performance loss, we propose a least-squares constrained basis pursuit algorithm to reduce the effect of uncertainties by considering only the degrees-of-freedom subspace intersection.

Index Terms—Opportunistic communications, distributed networks, pulse generation, multi-signal detection, sparse detection.

I. INTRODUCTION

Opportunistic communication [1] allows efficient information transmission in distributed networks due to reduced signaling overhead avoiding centralized backbone infrastructures.

Although lots of works have been devoted to analyzing feasible transmission schemes (see, e.g., [2–4]), performance aspects should be also considered. As in any robust communication system, time-references are required to achieve node synchronization or acquire channel state information (CSI) in order to guarantee the desired performance in terms of achievable throughput and secrecy [5–7], and detection and decoding [8].

Classically, time-references are based on offline-designed pilot signals, which do not take network conditions into account. Therefore, the system performance is degraded in very high user-density scenarios dominated by the level of *pilot contamination* [9]. Even though pilot contamination has been classically studied in the well-known scenario of massive multiple-input multiple-output (MIMO) communications, it is also present in congested distributed networks [6].

Several signal processing techniques have been recently developed to cope with pilot contamination. These techniques

are encompassed in the concept of *pilot decontamination*. In that respect, some works are devoted to reducing (or, ideally, eliminating) the contamination [10], [11]. On the other side, we may find some works that address how pilot contamination can be avoided [12].

In contrast to the aforementioned works where pilot contamination is assumed and the performance is improved by means of pre- and/or post-processing techniques, we present in this paper a scenario-adapted pilot waveform design scheme. Each user of a distributed network acquires a set of observations from the wireless environment and adapts the waveform in such a way that only available resources are used. It is worth noting that the design scheme presented in this paper is also valid in the context of adaptive waveform pulse shaping design.

Once each user has designed its own pilot, the major challenge is how this node can discover neighboring ones without cooperation, using local pilots as time-references. Hence, this paper also deals with the pilot detectability. We show that, under the existence of some *invariances*, pilots can be detected. The latter is a necessary condition for using locally-designed pilots as time-references in noncooperative distributed systems.

However, the uncoordinated nature of this system incurs in a performance loss due to node-to-node uncertainty. We finally address how receiver can diminish the effects of uncertainties via a sparsity-based *subspace dimension reduction*. This contribution enables joint multi-waveform detection, justifying the feasibility of proposed pilot scheme in multiuser scenarios.

The rest of this paper is organized as follows. The problem addressed in this paper is formulated in Sec. II. The distributed pulse shaping generation design is tackled in Sec. III. In Sec. IV we formulate the problem of signal detectability and the required invariances to use distributed pilots as reference signals are analyzed in Sec. V. The (multi-) waveform detection and subspace dimension reduction is analyzed in Sec. VI. Numerical results are provided in Sec. VII and the paper is concluded in Sec. VIII.

II. PROBLEM STATEMENT

Robust communication systems use time-references as training and polling schemes, to achieve synchronization, identify the channel or assist multiuser detection. Typically, these reference signals are based on offline-designed pilots, which are not adapted to scenario working conditions. In congested networks, using offline-designed pilots is a source of interferences, such as pilot contamination, yielding a poor performance.

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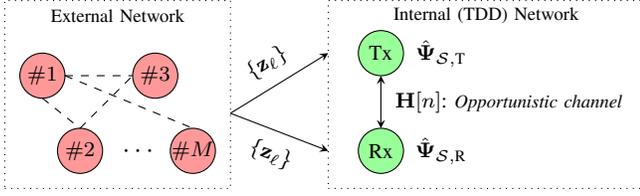


Fig. 1: Context-aware opportunistic communication in a distributed network.

In this work, we address the distributed design of reference signals taking into account the working conditions of a distributed opportunistic communication scenario. Let us consider the scenario depicted in Fig. 1. As we can appreciate, it is composed of two networks. On the one hand, external network is an M -user heterogeneous network, where these M users may present different communication formats. Nonetheless, they are simultaneously transmitting information exploiting D degrees-of-freedom (DoF) (cf. [13], [14]). On the other hand, users from internal network wish to setup a point-to-point link without interfering the external-network users. In other words, they want to exploit the *unused* DoF. To do so, each internal-network user acquires L observations of length N from the external network

$$\mathbf{z}_\ell = \mathbf{s}_\ell + \mathbf{v}_\ell, \text{ for } \ell = 1, \dots, L, \quad (1)$$

where \mathbf{s}_ℓ is the signal transmitted by existing users, and \mathbf{v}_ℓ is the noise distributed as $\mathbf{v}_\ell \sim \mathcal{CN}(\mathbf{0}, \sigma^2 \mathbf{I}_N)$.

Taking into account only local observations, each internal-network user has to design a pulse shaping filter $\varphi_i(n)$, where i indexes the internal user. Let $x(n)$ be the signal received by an arbitrary internal user. It can be written as

$$x(n) = \sum_m \sqrt{S_R} a[m] \varphi_i(n - mT) + v(n), \quad (2)$$

where $a[m]$ is a symbol from a given constellation, T denotes the symbol period and S_R , the received power. Here, the complex noise $v(n)$ is assumed to be a complex Gaussian random variable, i.e. $v(n) \sim \mathcal{CN}(0, \sigma_v^2)$. Due to the generality of (2), we can distinguish two different cases:

- (i) When the symbol $a[m]$ is an information symbol, the design of the pulse $\varphi_i(n)$ can be seen as an adaptive waveform design problem.
- (ii) If $a[m]$ is a known pseudorandom sequence, the problem turns to a distributed pilot waveform design. In that case, in order to avoid spectral lines, this sequence ought to spread the pilot signal energy spectral density.

Once each internal user has designed its pilot $\varphi_i(n)$, it first needs to detect the presence of neighboring nodes. Recall the scenario depicted in Fig. 1. Let $\varphi_T(n)$ and $\varphi_R(n)$ be the pulses designed at internal transmitter and receiver, respectively. Thus, the goal of internal system can be cast as

$$\max_j \left| \sum_n \varphi_T^*(n) \varphi_R(n, j) \right|. \quad (3)$$

In other words, receiver has to select a pulse $\varphi_R(n)$ from a set and adapt it as a matched filter response to detect the transmitter's signal without transmitter-receiver cooperation, while diminishing the pulse-shaping mismatch due to different knowledge of external-network state at each internal node.

III. UNCOORDINATED PULSE SHAPING DESIGN

Hereunder we detail the decentralized pulse shaping design scheme. It is worth noting that it consists in a generalization of particular examples presented by the authors in [15], [16].

Since external-network users employ D DoF, their transmissions belong to a D -dimensional subspace. Actually, this subspace corresponds to the *occupied DoF* (ODoF) subspace. In some frameworks, the latter is known as *signal* subspace. Henceforth, for simplicity of notation, we refer the ODoF subspace as signal subspace, namely \mathcal{S}^D . Hence,

$$\mathbf{s}_\ell \in \mathcal{S}^D, \forall \ell \in \{1, \dots, L\} \quad (4)$$

Whenever $D < N$, there exists a K -dimensional subspace, with $K = N - D$, orthogonal to \mathcal{S}^D . This subspace contains the *available DoF* (ADoF) for opportunistic communication. Similarly to the ODoF case, ADoF subspace is also known as *noise* subspace. For simplicity, we will denote ADoF subspace as noise subspace, namely \mathcal{N}^K .

Taking the latter into account and letting Ψ_S and φ be a signal-subspace basis and the opportunistic waveform, the design problem is cast as

$$\Psi_S^H \varphi(\mathbf{r}) = \mathbf{0}, \quad (5)$$

where \mathbf{r} is the position vector. In this Section, for simplicity of discussion, we address the pilot design at an arbitrary geographical position \mathbf{r} . In the sequel, we drop the dependence on \mathbf{r} for simplicity of notation.

Due to sensing uncertainties, shadowing or channel fading, internal users are not able to obtain an accurate signal-subspace basis. Thus, we may find two possible scenarios:

- (i) Internal users *overestimate* signal-subspace dimension: Internal users will lose transmission opportunities, which is not critical in view of (5).
- (ii) Internal users *underestimate* signal-subspace dimension: This is the critical scenario. Some of the occupied DoF are erroneously sensed as available. Hence, internal users will also use them, leading to a noise enhancement.

Bearing in mind the worst case, a signal-subspace basis can be written as

$$\Psi_S = \left[\hat{\Psi}_S \ ; \ \Xi \right], \quad (6)$$

where $\hat{\Psi}_S$ stands for the *sensed* signal-subspace basis, and Ξ represents those DoF that are erroneously sensed as available. In (6), an *actual* signal-subspace basis can be seen as a column-stacking of orthonormal bases $\hat{\Psi}_S$ and Ξ .

It is worth noting that, in view of (6), the signal subspace \mathcal{S}^D admits the following decomposition

$$\mathcal{S}^D = \hat{\mathcal{S}}^{\tilde{D}} \cup \mathcal{E}^\delta, \quad (7)$$

with $D = \tilde{D} + \delta$. In (7), \mathcal{E}^δ refers to the portion of the actual signal subspace spanned by Ξ . Since an arbitrary internal user will only be able to sense $\hat{\Psi}_S$, it will also exploit those DoF belonging to \mathcal{E}^δ . Therefore, taking (6) into consideration, the cost function becomes

$$\min_{\varphi} \max_{\Xi} \left\| \left[\hat{\Psi}_S \ ; \ \Xi \right]^H \varphi \right\|^2. \quad (8)$$

In order to constrain the uncertainty in our problem, we upper-bound the rank of Ξ . Furthermore, because (8) admits a trivial solution, we consider the linear predictor condition [17] as a non-trivial design constraint. Thus, (8) becomes

$$\min_{\varphi} \max_{\Xi} \left\| [\hat{\Psi}_S \Xi]^H \varphi \right\|^2 \quad \text{s.t.} \quad \|\Xi\|_F^2 \leq \epsilon \text{ and } \mathbf{e}_n^H \varphi = 1, \quad (9)$$

with $\mathbf{e}_n \triangleq [\mathbf{0}_{n-1}^T \ 1 \ \mathbf{0}_{N-n}^T]^T$. Because $\hat{\Psi}_S^H \varphi = \mathbf{0}$ and defining the orthogonal projector onto \mathcal{E}^δ as $\Sigma \triangleq \Xi \Xi^H$, the pulse shaping filter design problem is finally given by

$$\tilde{\varphi}_n = \arg \min_{\varphi} \max_{\Xi} \|\Sigma \varphi\|^2 \quad \text{s.t.} \quad \mathbf{e}_n^H \varphi = 1, \quad \|\Sigma\|_F^2 \leq \epsilon. \quad (10)$$

Due to lack of space, the derivation of (10) is only sketched herein. The reader is referred to [15], [16] for further details.

By solving the maximization problem in (10), we get

$$\Sigma_{\text{worst-case}} = \frac{\epsilon}{\|\varphi\|^2} \varphi \varphi^H. \quad (11)$$

Notice that, in view of (11), $\epsilon = 1$, which means that internal users inject all transmitted power into DoF occupied by external users. Then, since $\hat{\Psi}_S^H \varphi = \mathbf{0}$, the designed waveforms can be written as a linear combination of the elements of the sensed noise-subspace basis, i.e. $\varphi = \hat{\Psi}_{\mathcal{N}} \lambda$. Hence, (10) yields

$$\tilde{\varphi}_n = \left(\mathbf{e}_n^H \hat{\Psi}_{\mathcal{N}} \hat{\Psi}_{\mathcal{N}}^H \mathbf{e}_n \right)^{-1/2} \hat{\Psi}_{\mathcal{N}} \hat{\Psi}_{\mathcal{N}}^H \mathbf{e}_n, \quad (12)$$

with $\hat{\mathbf{P}}_{\mathcal{N}} = \hat{\Psi}_{\mathcal{N}} \hat{\Psi}_{\mathcal{N}}^H$ being the orthogonal projector onto the noise subspace. Notice that the solution in (12) is a normalized column of $\hat{\mathbf{P}}_{\mathcal{N}}$. Since all they are orthogonal to the sensed signal-subspace basis, any of them are a possible solution.

It is worth noting that the proposed design scheme reduces to a classical minimum-norm optimization problem. Therefore, the pulse shaping filters designed as (12) exhibit the good properties of minimum-norm estimator [17]. Moreover, its robustness in front of sensing errors is confirmed given the equivalence of (12) and total least-squares [18].

IV. IMPACT OF INCOMPLETE EXTERNAL-INTERFERENCE INFORMATION IN SIGNAL DETECTION

In the previous Section, we have reviewed the uncoordinated design of pulse shaping filters in opportunistic networks. Because each internal user only considers local observations, the subspaces sensed at each node may differ. Hence, the noise-subspace bases sensed at each node can be written as

$$\hat{\Psi}_{\mathcal{N},T} = \begin{bmatrix} \Psi_{\mathcal{N}}^{(0)} & \Delta_T \end{bmatrix}, \quad (13a)$$

$$\hat{\Psi}_{\mathcal{N},R} = \begin{bmatrix} \Psi_{\mathcal{N}}^{(0)} & \Delta_R \end{bmatrix}, \quad (13b)$$

where $\Psi_{\mathcal{N}}^{(0)}$ represents the DoF sensed as available at both internal nodes, and Δ_i , for $i = \{T, R\}$, contains those DoF that are sensed as available at only one internal node. Notice that $K_i = K_0 + \kappa_i$, with $K_0 = \text{rank}(\Psi_{\mathcal{N}}^{(0)})$ and $\kappa_i = \text{rank}(\Delta_i)$. Recalling the design scheme reviewed in Sec. III, each internal user will have a set of N possible pilot waveforms, namely *pilot-book*, such that

$$\mathcal{P}_T = \{\tilde{\varphi}_{T,1}, \dots, \tilde{\varphi}_{T,N}\} \in \hat{\mathcal{N}}_T, \quad (14a)$$

$$\mathcal{P}_R = \{\tilde{\varphi}_{R,1}, \dots, \tilde{\varphi}_{R,N}\} \in \hat{\mathcal{N}}_R, \quad (14b)$$

corresponding to the N columns of orthogonal projectors onto $\hat{\mathcal{N}}_T$ and $\hat{\mathcal{N}}_R$, respectively. Note that $\hat{\mathcal{N}}_T \neq \hat{\mathcal{N}}_R$ whenever $\kappa_i \neq 0$.

Therefore, when the receiving node uses their local pilots as reference signals, the *detectability* can be compromised. Moreover, receiver has to face the uncertainty exhibited by Δ_i to improve the performance of the opportunistic communication.

Regarding to the model presented in (2), the signal sensed by the receiver can be written as

$$x(n) = \sum_m \sqrt{S_R} a[m] \tilde{\varphi}_{T,k}(n - mT) + v_1(n) + v_2(n), \quad (15)$$

where $\tilde{\varphi}_{T,k}(n)$ is the k -th element of \mathcal{P}_T , $v_1(n)$ and $v_2(n)$ are the white complex noises from the common and uncommon DoF, respectively, assumed to be Gaussian random variables. It is worth noting that the receiver's performance can be improved by diminishing the noise enhancement introduced by $v_2(n)$.

Thus, the objectives of the internal system are twofold:

- 1) Since the transmitter will select an arbitrary pilot $\tilde{\varphi}_{T,i}$ from \mathcal{P}_T with probability $\frac{1}{N}$, the receiver should find the pilot $\tilde{\varphi}_{R,j}$ from \mathcal{P}_R such that

$$\max_j |\tilde{\varphi}_{T,i}^H \tilde{\varphi}_{R,j}|. \quad (16)$$

- 2) Recalling that $\hat{\mathcal{N}}_T \neq \hat{\mathcal{N}}_R$, the receiver should design a filter $\hat{\mathbf{w}}$, using the pilot selected in (16) as reference, such that only senses the K_0 DoF belonging to the intersection $\hat{\mathcal{N}}_T \cap \hat{\mathcal{N}}_R = \mathcal{N}_0$, i.e.

$$\hat{\mathbf{w}} \in \mathcal{N}_0. \quad (17)$$

Notice that this filter will (ideally) cancel noise sensed from uncommon dimensions. Furthermore, it can be used to assist the internal transmitting node to achieve subspace consensus via feedback.

Therefore, these two addressed objectives can be cast as a joint optimization problem, i.e.

$$\{\hat{\mathbf{w}}_\iota, \hat{\iota}\} = \arg \min_{\{\mathbf{w}_\iota, \iota\}} \mathbb{E} \left\{ |\mathbf{w}_\iota^H \mathbf{x}(n) - d_{R,\iota}(n)|^2 \right\}, \quad (18)$$

for $\iota \in \{1, \dots, N\}$. It is noteworthy that the reference signal at receiver $d_{R,\iota}(n)$ is the ι -th pilot from \mathcal{P}_R , i.e. $\tilde{\varphi}_{R,\iota}(n)$. Nevertheless, pilots from \mathcal{P}_R should exhibit certain invariances with respect to those from \mathcal{P}_T in order to be a valid reference signal, due to the lack of coordination between internal users.

V. ANALYSIS OF SOLUTION INVARIANCE

This Section is devoted to studying the invariance of the proposed pilot waveforms (12). As we have aforementioned, some invariances are required in order that (12) can be used as time-reference signals.

A. Invariance to Rotations

Because the proposed pilot waveforms rely on the orthogonal projector onto the noise subspace, they exhibit invariance to rotations when the sensed noise-subspace basis is acquired with a rotation within the noise subspace. This invariance is of paramount interest, because guarantees coherent detection.

The proof of this property can be found in [15], [16], and it is omitted in this conference presentation for space limitations.

B. Invariance to Subspace Uncertainties

In the ideal scenario where $\kappa_T = \kappa_R = 0$, the cross-correlation between the received signal and the selected pilot from \mathcal{P}_R will be almost one, and solely degraded by the signal-to-noise ratio (SNR). However, in the realistic scenario with sensing uncertainties, we will have a mismatching loss.

Hereunder, we analyze the penalty due to the lack of coordination between internal nodes.

Taking into account the noise-subspace bases decomposition in (13), the ι -th element of \mathcal{P}_i , for $i = \{T, R\}$, is given by

$$\tilde{\varphi}_{i,\iota} = (\mathbf{e}_{i,\iota}^H (\mathbf{P}_{\mathcal{N}} + \Upsilon_i) \mathbf{e}_{i,\iota})^{-1/2} (\mathbf{P}_{\mathcal{N}} + \Upsilon_i) \mathbf{e}_{i,\iota}, \quad (19)$$

where $\mathbf{P}_{\mathcal{N}}$ is the orthogonal projector onto the intersection $\hat{\mathcal{N}}_T \cap \hat{\mathcal{N}}_R = \mathcal{N}_0$, and Υ_i is the orthogonal projector onto the uncommon DoF subspace, namely $\bar{\mathcal{N}}^{\kappa_i}$. Therefore, (19) admits the following decomposition

$$\tilde{\varphi}_{i,\iota} = \tilde{\varphi}_{i,\iota}^{(0)} + \tilde{\varphi}_{i,\iota}^{(\bar{\mathcal{N}})}, \quad (20)$$

where $\tilde{\varphi}_{i,\iota}^{(0)}$ belongs to the intersection \mathcal{N}_0 , and $\tilde{\varphi}_{i,\iota}^{(\bar{\mathcal{N}})}$ to $\bar{\mathcal{N}}^{\kappa_i}$.

Therefore, taking into account that

$$\bar{\mathcal{N}}^{\kappa_T} \cap \bar{\mathcal{N}}^{\kappa_R} = \emptyset, \quad (21a)$$

$$\bar{\mathcal{N}}^{\kappa_i} \cap \mathcal{N}_0 = \emptyset, \text{ for } i = \{T, R\}, \quad (21b)$$

the output of a matched-filter receiver can be written as

$$\tilde{\varphi}_R^H \tilde{\varphi}_T = \frac{\mathbf{e}_R^H \mathbf{P}_{\mathcal{N}} \mathbf{P}_{\mathcal{N}} \mathbf{e}_T}{\sqrt{(\mathbf{e}_R^H \mathbf{P}_{\mathcal{N},R} \mathbf{e}_R) (\mathbf{e}_T^H \mathbf{P}_{\mathcal{N},T} \mathbf{e}_T)}}. \quad (22)$$

According to the proposed noise-subspace bases decomposition in (13), a fraction K_0/K_i of the total pulse energy at the i -th internal user will be transmitted through the intersection \mathcal{N}_0 , whereas the remaining fraction $(K_i - K_0)/K_i = \kappa_i/K_i$ will be lost. Finally, the matched-filter mismatch factor is given by

$$\tilde{\varphi}_R^H \tilde{\varphi}_T = \left(1 + \frac{\kappa_T + \kappa_R}{K_0} + \frac{\kappa_T \kappa_R}{K_0^2} \right)^{-1/2}. \quad (23)$$

It is worth noting that, when K_0 is large enough, the second-order term may be neglected. Therefore, due to those DoF belonging to the intersection are preserved (except a scaling factor), designed pilot waveforms are invariant to subspace uncertainties subject to an energy loss.

VI. SPARSITY-BASED JOINT CONSENSUS AND (MULTI-)SIGNAL DETECTION

Traditionally, the cost function in (18) is solved by the well-known mean-square error (MSE) optimal filter $\hat{\mathbf{w}}_\iota$, given the ι -th reference signal. Therefore, the MSE in (18) given the Wiener solution of $\hat{\mathbf{w}}_\iota$ is given by

$$\text{MSE}(\iota|\hat{\mathbf{w}}_\iota) = P_d(\iota) - P_y(\iota), \quad (24)$$

where $P_d(\iota) = \mathbb{E}\{|d_{R,\iota}(n)|^2\}$ is the power of the ι -th reference signal and $P_y(\iota) = \mathbb{E}\{\mathbf{p}(\iota)^H \mathbf{R}_{xx}^{-1} \mathbf{p}(\iota)\}$ is the power at the output of receiver's filter. Notice that \mathbf{R}_{xx} is the input signal autocorrelation matrix, whereas $\mathbf{p}(\iota) = \mathbb{E}\{\mathbf{x}(n)d_{R,\iota}^*(n)\}$ is the

cross-correlation vector. Since $P_d(\iota)$ is independent of the input data, the signal detection problem is cast as

$$\hat{\iota} = \arg \max_{\iota \in \{1, \dots, N\}} \mathbb{E}\{\mathbf{p}(\iota)^H \mathbf{R}_{xx}^{-1} \mathbf{p}(\iota)\}. \quad (25)$$

In other words, the receiver's pilot waveform which presents the highest correlation with the input signal has to be selected. Albeit it is out of the scope of this work, it is worth noting that this procedure can be accelerated by implementing a multiple-dwell scheme [19].

What it is very interesting to notice is that in our problem the waveform detection is an inherent sparse problem, specially when realistic (uncertainty-limited) scenarios are considered. Due to the partial knowledge of external-network state, the solution proposed in (25) is, in general, not optimal.

Note that, whenever $\kappa_T, \kappa_R \neq 0$, the SNR at receiver is given by

$$\text{SNR}_R = \frac{(1 - \frac{\kappa_T}{K_T})S_T}{(1 + \frac{\kappa_R}{K_R})N_0} = \frac{1 - \frac{\kappa_T}{K_T}}{1 + \frac{\kappa_R}{K_R}} \text{SNR}_0, \quad (26)$$

where SNR_0 is the nominal SNR (i.e. that when $\kappa_T = \kappa_R = 0$), and N_0 is the noise power. Since the received signal can be written as

$$\mathbf{x}_m = a[m] \sqrt{S_T} \tilde{\varphi}_T + \mathbf{v}_1 + \mathbf{v}_2, \quad (27)$$

and recalling the structure of pilot waveforms presented in (12), internal receiving node may estimate (27) as

$$\hat{\mathbf{x}} = \tilde{\mathbf{P}}_{\mathcal{N},R} \boldsymbol{\alpha}, \quad (28)$$

where $\boldsymbol{\alpha} = \{0, 1\}^N$ is a sparse vector that selects which pilot better estimates the input signal and $\tilde{\mathbf{P}}_{\mathcal{N},R}$ is a modified projector such that

$$\tilde{\mathbf{P}}_{\mathcal{N},R} = \sum_{n=1}^{K_R} \lambda_n \mathbf{P}_n, \quad (29)$$

with $\mathbf{P}_n = [\hat{\Psi}_{\mathcal{N},R}]_n [\hat{\Psi}_{\mathcal{N},R}]_n^H$ being the projector onto the n -th receiver's noise subspace singleton, where $[\hat{\Psi}_{\mathcal{N},R}]_n$ is the n -th column of basis in (13b), and λ_n is 0 or 1 depending on if the n -th singleton belongs to the intersection of noise subspaces or not. By defining $\boldsymbol{\lambda} = [\lambda_1, \dots, \lambda_{K_R}]^T$ and $\mathbf{P} = [\mathbf{P}_1 \cdots \mathbf{P}_{K_R}]$, design problems in (28) and (29) can be jointly cast as

$$\hat{\boldsymbol{\beta}} = \arg \min_{\boldsymbol{\beta}} \|\boldsymbol{\beta}\|_1 \text{ s.t. } \mathbf{x} = \mathbf{P}\boldsymbol{\beta}, \quad (30)$$

with $\boldsymbol{\beta} = \boldsymbol{\lambda} \otimes \boldsymbol{\alpha}$, being \otimes the Kronecker tensor product. It is noteworthy that the complexity of the design problem have increased due to the stacking in (30). However, it is an inherent advantage since the receiver is now able to simultaneously detect up to K orthogonal pilots from different users, which makes the discussed scheme feasible in multiuser scenarios.

As a last comment on (30), we note that it is sensitive to noise, specially in low-SNR regimes. Therefore, let us consider that receiver is able to capture Q observations from the transmitter, and they are stacked in a NQ column vector $\tilde{\mathbf{x}} = [\mathbf{x}_1^T \cdots \mathbf{x}_Q^T]^T$. In addition, let us consider the extended matrix $\tilde{\boldsymbol{\Phi}}^T = [\tilde{\mathbf{P}} \cdots \tilde{\mathbf{P}}]$, i.e. $\tilde{\boldsymbol{\Phi}}$ contains Q times matrix $\tilde{\mathbf{P}}$ stacked in columns. Thus, the extended joint design problem becomes

$$\hat{\boldsymbol{\beta}} = \arg \min_{\boldsymbol{\beta}} \|\boldsymbol{\beta}\|_1 \text{ s.t. } \|\tilde{\mathbf{x}} - \tilde{\boldsymbol{\Phi}}\boldsymbol{\beta}\|_2^2 \leq \epsilon^2. \quad (31)$$

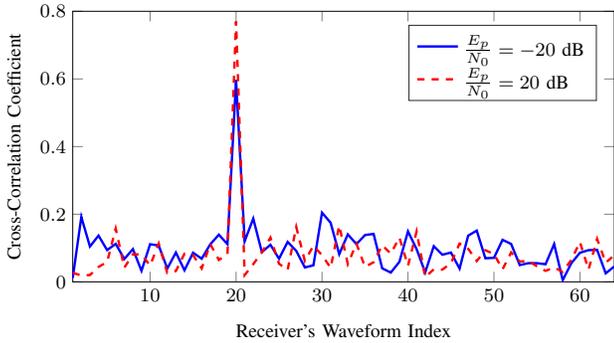


Fig. 2: Cross-correlation coefficient between received signal and all elements of the receiver's pilot-book in an uncertainty-free scenario, i.e. $\kappa_T = \kappa_R = 0$.

It is worth noting that for large data block-length Q , the proposed extended optimization in (31) may burden computational inefficiency. Nevertheless, it is straightforward to see that the extended problem in (31) is equivalent to

$$\hat{\beta} = \arg \min_{\beta} \|\beta\|_1 \text{ s.t. } \sum_{q=1}^Q \|\mathbf{x}_q - \mathbf{P}\beta\|_2^2 \leq \epsilon^2. \quad (32)$$

Therefore, the least-squares constraint of full NQ -length data-block in (31) can be tackled as the cumulative least-squares error of each N -length sub-block \mathbf{x}_q , yielding a reduced computational complexity with respect to (31).

VII. SIMULATION RESULTS

Numerical assessment of results derived in this work is presented in this Section.

A. Matched-Filter Detection: Proof-of-concept

The detection performance of the distributed pilot-based matched filter receiver is assessed herein. To do so, we consider an M -user heterogeneous external network transmitting in a 64-dimensional space. External-user DoF occupation is $3/8$, i.e. $D = 24$ DoF. Therefore, the actual number of available DoF is $K = 40$. For this proof-of-concept, two scenarios are considered: $E_p/N_0 = -20$ dB and $E_p/N_0 = 20$ dB, with E_p/N_0 being the pulse energy to noise ratio. Furthermore, we assume that internal transmitting node has arbitrarily selected the 20-th column of its noise-subspace projector.

In Fig. 2 we depict the cross-correlation coefficient between the received signal and the N elements of the receiver's pilot-book \mathcal{P}_R in an ideal scenario, i.e. $\kappa_T = \kappa_R = 0$. As it can be appreciated, the correct detection is guaranteed.

Concerning more realistic scenarios, we illustrate the cross-correlation coefficient under DoF sensing uncertainties in Fig. 3. Regarding to the uncertainty, let ρ_i be the relative uncertainty at the i -th internal node, defined as $\rho_i \triangleq \frac{\kappa_i}{K_i}$, for $i = \{T, R\}$.

For this particular example, we have considered $\rho_T = 5/45 = 11.11\%$ and $\rho_R = 15/55 = 27.27\%$. It is worth noting that ρ_T degrades the transmitted E_p , whereas ρ_R is a source of noise enhancement. As we may observe, although the detector exhibits a good performance in high- $\frac{E_p}{N_0}$ regimes, the detection can be compromised in low- $\frac{E_p}{N_0}$ regimes.

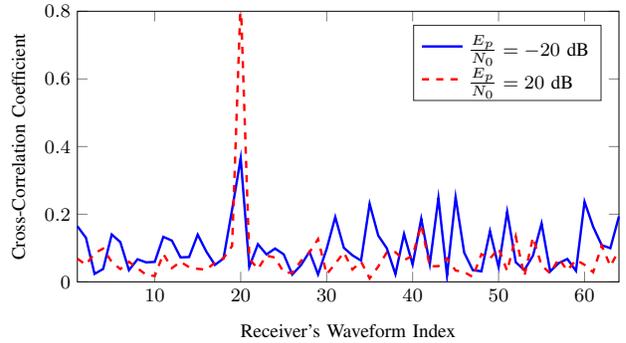


Fig. 3: Cross-correlation coefficient between received signal and all elements of the receiver's pilot-book with uncertainty ($\kappa_T, \kappa_R \neq 0$).

B. Uncertainty Analysis

As we appreciate in the previous Subsection, DoF sensing uncertainty degrades the detection performance, as we have analytically derived in Sec. V, eq. (23). Herein, we numerically assess the impact of the performance loss on the received signal-to-noise ratio as a function of the absolute uncertainty at receiver and for different absolute uncertainties at transmitter. Let us consider the scenario presented in Sec. VII-A. In Fig. 4 we compare the theoretical loss and a Montecarlo simulation of 100,000 independent realizations. It is worth noting that, for high noise level from uncommon DoF, the mismatch severely degrades the system performance, specially in low- $\frac{E_p}{N_0}$ regimes.

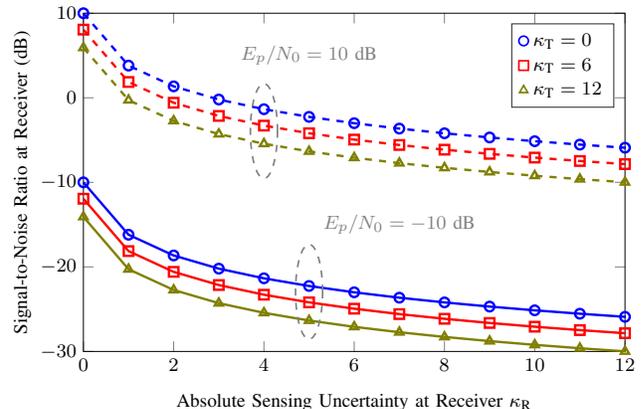


Fig. 4: Signal-to-Noise Ratio at Receiver in a realistic scenario. Lines and markers represent theoretical and simulated values, respectively.

C. Degrees-of-Freedom Detection Performance

In order to combat sensing uncertainties, we have proposed a joint ℓ_1 -norm optimization (32). This procedure is able to jointly detect which DoF are simultaneously used by transmitter and receiver and select the pulse shape that better detects the received signal. We assume the same scenario as in Sec. VII-A, i.e. $N = 64$ DoF and external-network occupation of $3/8$. For simplicity, we have assumed $\rho_T = \rho_R = 12/52$.

Herein, we assess the capacity of the proposed algorithm to differentiate which DoF are simultaneously used by both transmitter and receiver. To do so, let us define the probability of correct detection P_D as the probability of detecting as active

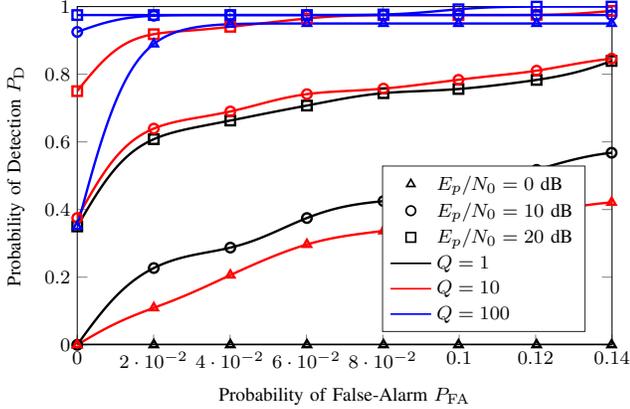


Fig. 5: ROC for $E_p/N_0 = \{0, 10, 20\}$ dB and different block-length $Q = \{1, 10, 100\}$ averaged over 10^4 independent realizations.

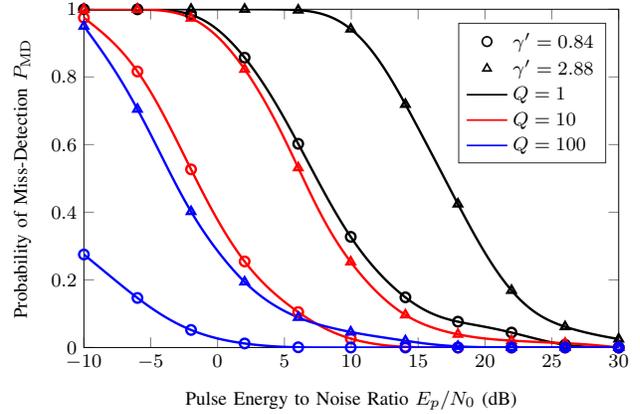


Fig. 6: Probability of Miss-Detection versus E_p/N_0 for $\gamma' = \{0.84, 2.88\}$ and block-length $Q = \{1, 10, 100\}$ averaged over 10^4 independent realizations.

a DoF belonging to the intersection. Likewise, we refer to the miss-detection probability P_{MD} as the probability of not detecting as active a DoF belonging to the intersection.

In Fig. 5 we have depicted the Receiver Operating Characteristics (ROC) of the proposed ℓ_1 -norm algorithm (32). In these simulations, we have considered different E_p/N_0 and different block-lengths Q . The probability of false-alarm P_{FA} is set as the probability of detecting as active a DoF not belonging to the intersection. In order to maximize P_D , we have considered a Neyman-Pearson threshold, i.e.

$$\gamma = \sqrt{(\sigma_R^2/Q)}\mathcal{Q}^{-1}(P_{FA}), \quad (33)$$

with $\mathcal{Q}(\cdot)$ being the tail probability of a Gaussian distribution. Notice that σ_R^2 is the noise variance at receiver. The miss-detection probability P_{MD} , defined as the probability of detecting a DoF not belonging to the intersection is depicted in Fig. 6 as a function of E_p/N_0 . For this particular example, we have considered $P_{FA} = \{0.1, 0.001\}$, i.e. $\gamma' = \mathcal{Q}^{-1}(P_{FA}) = \{0.84, 2.88\}$. It is worth noting that, even for small P_{FA} , P_{MD} rapidly diminishes with E_p/N_0 .

VIII. CONCLUSIONS

This paper has addressed the distributed scenario-adapted design of pilot reference signals in opportunistic communications. The use of these pilots as reference signals relies on the existence of certain invariances. Furthermore, although matched filter is optimal in white noise, sensing uncertainties worsen the performance by means of energy loss and noise enhancement. The latter can be solved by jointly selecting which DoF have two users in common and detecting the presence of such user. As we have seen, this extended ℓ_1 -norm problem enables the proposed technique in multiuser scenarios.

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