

1 **Nutrients recovery from Treated Secondary Mainstream in an Urban Wastewater Treatment**

2 **Plant: A financial assessment case study**

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16  
17 **Abstract**

18 This study presents the financial assessment for implementing an ammonium and phosphate  
19 simultaneous recovery process based on the use of calcium activated synthetic zeolites in a large  
20 urban Waste Water Treatment Plant (WWTP) located in the Metropolitan Area of Barcelona.

21 A calcium activated synthetic zeolites was selected, after a benchmarking analysis, as it reported  
22 capability for simultaneously recover ammonium and phosphate by a combined mechanism of ion

23 exchange for ammonium and formation of insoluble mineral phase for phosphate. The loaded  
24 sorbent, rich in ammonium and phosphate, can be used as slow-release fertilizer.

25 Financial indexes such as the net present value, the internal return Rate, the return of investment  
26 and the payback period were calculated concluding that the integration of a zeolite-based sorption  
27 treatment stage in the main stream is economically feasible, with a reasonable payback period.  
28 The need, to achieve low-levels of P and N on the discharged waters and the need to develop more  
29 sustainable WWTP facilities indicate that the deployment of nutrient recovery solutions will be  
30 encouraged. The sensitivity analysis carried out to define the critical parameters of the economic  
31 performance of the technology allows concluding that the main variable in the viability of the nutrient  
32 recovery unit is related to the nutrients sorbent, both in the cost of purchase and in the market for  
33 the sorbent loaded with nutrients.

34 Keywords: ammonium; phosphate; wastewater; nutrient recovery; zeolite; economic feasibility

35

## 36 1. Introduction

37 Nitrogen and phosphorus are essential elements for life and large amounts of these elements,  
38 mainly in the form of ammonium and phosphate, are needed for fertilizer production in order to  
39 supply growing population food demand (Roberts and Johnston, 2015; Röhling, 2010). It is  
40 estimated that about  $22 \times 10^6$  ton/y of phosphorus from mined fossil phosphate resources are  
41 added to the world economy (Reijnders, 2014), which leads to a significant alteration of the natural  
42 cycle of these elements resulting in problems with air and water quality as well as overall ecosystem  
43 balance (Bennett and Schipanski, 2013; Driscoll et al., 2003; Galloway and Cowling, 2002;  
44 Groffman and Rosi-Marshall, 2013).

45 Furthermore, nitrogen and phosphorus discharge limits become increasingly stringent. European  
46 Urban Waste Water Treatment Directive set the maximum annual mean total nitrogen

47 concentration between 1.5 and 10 mgN/L depending on the size of the urban area (Oenema et al.,  
48 2011) and phosphorus discharge regulation set its concentration on 2 mgP/L in Spain, 1 mgP/L in  
49 France, 0.1 mgP/L in UK or 0.01 mgP/L in different states of USA.

50 In the case of phosphorus, conventional treatments such as chemical precipitation or biological  
51 removal are not able to reach concentrations below 0.1 mgP/L and it is necessary to identify  
52 technical and economically feasible technologies able to reach ultra-low levels.

53 Furthermore, urban WWTPs are not any more considered as pollution removal systems but as  
54 resources (nutrients and energy) recovery plants (van der Hoek et al., 2016). In this new scheme,  
55 the systems focus mainly on the recovery of resources and the reuse of water to promote the  
56 circular economy approach where the pollution load becomes a source of secondary raw materials  
57 that can be recovered giving an added value to these sources (Kabbe et al., 2017; Ribanova et al.,  
58 2017; Scholz, 2017).

59 The use of secondary raw materials with sorption properties (e.g., natural sorbents or industrial  
60 wastes) is an area of increasing interest. Low cost sorbents with high affinity for ammonium and  
61 phosphate provide and attractive solution that offers the potential to recover nutrients of high quality  
62 that can be directly applied as a fertilizer as most of them will contain (N, P and K) (Egle et al.,  
63 2015; Scholz et al., 2013), which contribute to plant growth.

64 Furthermore, natural sorbent materials are often locally abundant, easy to dispose and include  
65 environmental friendly by-products such as shellfish shells (Abeynaike et al., 2011; Xiong et al.,  
66 2011), fly ash (He et al., 2012) or slag (Barca et al., 2012; Haddad et al., 2015; Jaouadi et al.,  
67 2014).

68 A summary of currently available phosphate and ammonium single recovery technologies from  
69 treated secondary effluent are listed in Table S1, most of them are already implemented in large  
70 WWTPs while in other cases has been applied to small scale (e.g., household in isolated  
71 communities).

72 Four technologies were identified, among all options listed in Table S1, with a TRL greater than 8  
73 (the system was completed and qualified through test and demonstration (United States  
74 Department of Defense, 2011)), which can produce effluents with ultra-low phosphorus (0.05  
75 mgP/L) concentration: Polonite, PhosphoReduc, CoMag and BluePro.

76 After the critical review of the state of the art, it can be concluded that there are several technologies  
77 available for the recovery of phosphorus from the WWTPs, but there is a lack of solutions focused  
78 on the recovery of nitrogen, since it is not a resource that presents scarcity, as if it exists for  
79 phosphorus. Different initiatives are widely developed worldwide to recover P for fertilization  
80 application from wastes generated on WWTPs. All of them are centered in two main directions: a)  
81 recovery of P as struvite from the sludge anaerobic digestion side-streams and b) recovery of P as  
82 phosphoric acid from the mono-incineration ashes generated from thermal treatments of sewage  
83 sludge in most of the northern countries of Europe and Japan (Amann et al., 2018). However, any  
84 initiative to recover ammonium at full scale could be found and the need to promote the deployment  
85 of solutions is a real challenge for the next decade.

86 In view of that, the aim of this study is to assess the financial feasibility of implementing a nutrients  
87 (simultaneous phosphorus and nitrogen) recovery system based on sorption technology from  
88 WWTP treated secondary effluent considering the CAPEX and OPEX of the required facilities, and  
89 potential revenues from cost savings and the sale of loaded adsorbent. The evaluation will be  
90 performed in a scenario in which the following boundary conditions have been selected: i) the use  
91 of a sorbent with dual capacity to sorb N and P simultaneously; ii) the implementation to a large  
92 WWTP (treatment capacity > 3m<sup>3</sup>/s) that incorporates a tertiary treatment; and iil) the saturated  
93 sorbent enriched on N, P will be commercialized as fertilizer.

94

## 95 2. Methodology

96 **2.1 Ammonia and phosphate adsorbents selection**

97 In previous studies the evaluation of polymeric sorbents as well as different salt activated synthetic  
 98 zeolites for nutrients recovery at the lab scale have been performed. The sorption performance of  
 99 these sorbents is summarized in table 2, where  $t_{90\%}$  is the time required for reaching the 90% of  
 100 maximum sorption capacity.

101 Table 2: Equilibrium and kinetic sorption properties of assessed adsorbents at lab scale

	$q_N$	$q_P$	$t_{90\%}$	Reference
	[mg N/g] <sup>1</sup>	[mg P/g] <sup>2</sup>	[min] <sup>3</sup>	
FO36	-	29.1	65	(You et al., 2016b)
Fiban-As	-	52.9	50	(You et al., 2016a)
Ze-Na	13.2	-	10	(You et al., 2017b)
Ze-K	22.6	-	2	
Ze-Ca	95.7	38.8	30	(You et al., 2017a)
Ze-Mg1	42.9	10.5	20	
Ze-Mg2	47.1	7.8	-	

102 1:  $q_N$  [mg N/g] is the total sorption capacity for ammonium; 2:  $q_P$  [mg P/g] is the total sorption capacity for ammonium; and 3:  $t_{90\%}$  is the time  
 103 required for reaching the 90% of maximum adsorption capacity.

104 The synthetic zeolite Ze-Ca was selected for the present study as it reported the best performance  
 105 for simultaneous recovery of nitrogen and phosphorus from wastewater treated effluent in terms of  
 106 the sorption capacity for both nutrients and the kinetic parameters that showed a faster sorption  
 107 rate, which represents a short hydraulic retention time (HRT). In addition, tertiary reactive media  
 108 filtration proved to be one of the most cost effectiveness alternatives for phosphorus removal in  
 109 municipal wastewater treatment (Bashar et al., 2018).

110 Furthermore, it is considered the Baix Llobregat WWTP as it is the largest and newest WWTP in  
111 the Metropolitan Area of Barcelona, which includes a water regeneration station, built in 2007 and  
112 which is based on filtration and reverse osmosis. This facility could be used for the filtration  
113 (ultrafiltration (UF) unit) and separation of loaded zeolite from treated secondary effluent (Hermassi  
114 et al., 2016).

## 115 **2.2 The Baix Llobregat WWTP (BLI-WWTP) as nutrients recovery site study**

116 The BLI-WWTP began to work at 2002 and several improvements have been introduced since  
117 then, such as the biologic treatment of wastewater, anaerobic digestion of sewage sludge or the  
118 implementation of a water regeneration station.

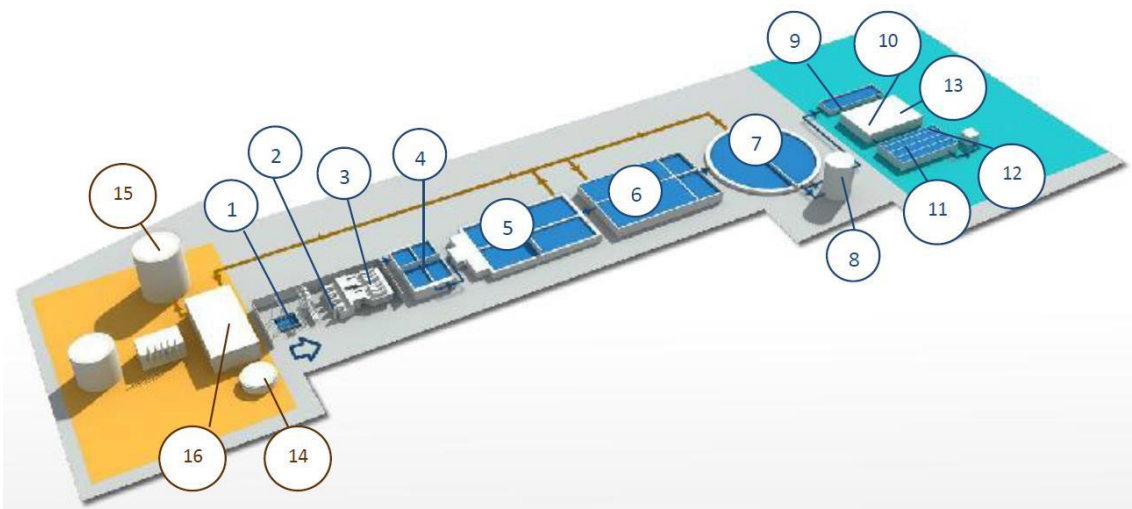
119 Nowadays, this plant treats the 36% of the wastewater generated in the Metropolitan Area of  
120 Barcelona and it provides service to approximately 2 million of population equivalent (PE) by  
121 treating 273330 m<sup>3</sup>/d of wastewater, which represents 65% of its design flow (4.86 m<sup>3</sup>/s) (Àrea  
122 Metropolitana de Barcelona, 2017a). According to the average composition of the wastewaters  
123 influent values (60 gN/m<sup>3</sup> and 6.8 gP/m<sup>3</sup>), the amount of N and P reaching the WWTP approaches  
124 to 9200 ton/y and 1100 ton/y, respectively.

125 12 identical working lines consisting on a primary settlement and a conventional secondary  
126 biological treatment compose the BLI-WWTP. At the initial design, the main part of the treated  
127 effluent was discharged into the Mediterranean Sea through an emissary 3.2 km long (Köck-  
128 Schulmeyer et al., 2011).

129 However, due to water crisis, a regeneration station was installed in 2007 with the capacity to  
130 provide tertiary treatment to WWTP effluent for reuse in agricultural irrigation, wetland conservation,  
131 groundwater hydraulic barriers against marine saline intrusion, and groundwater recharge of  
132 Llobregat river aquifer. The tertiary treatment consists on ultrafiltration (UF), reverse osmosis (RO),  
133 reverse electrodialysis (EDR) and disinfection (Köck-Schulmeyer et al., 2011). Analysis of the

134 average composition of the treated water along 2012 indicates that approximately 1200 tonN/y and  
135 390 tonP/y were discharged into the Mediterranean Sea.

136 The scheme of the BLI-WWTP and the main stages of treatment are shown in Figure 1. The zeolite  
137 filtration system is proposed to be installed after the secondary clarifier to use the existing UF unit  
138 of the regeneration station for separating the loaded zeolite from the treated water as has been  
139 proved successfully elsewhere (Hermassi et al., 2016).



140 Figure 1: Scheme of the BLI-WWTP configuration (Àrea Metropolitana de Barcelona, 2017b): 1  
141 Sedimentation tank, 2 Pumps, 3 Bar screen, 4 Grit chamber, 5 Primary clarifier, 6 Biologic reactor, 7  
142 Secondary clarifier, 8 Treated water discharge, 9 Flocculation tank, 10 Lamella clarifier, 11 Screening, 12  
143 Disinfection, 13 UF and RO+EDR, 14 Sludge thickener, 15 Sludge Digester, 16 Sludge thermic  
144 dewatering  
145

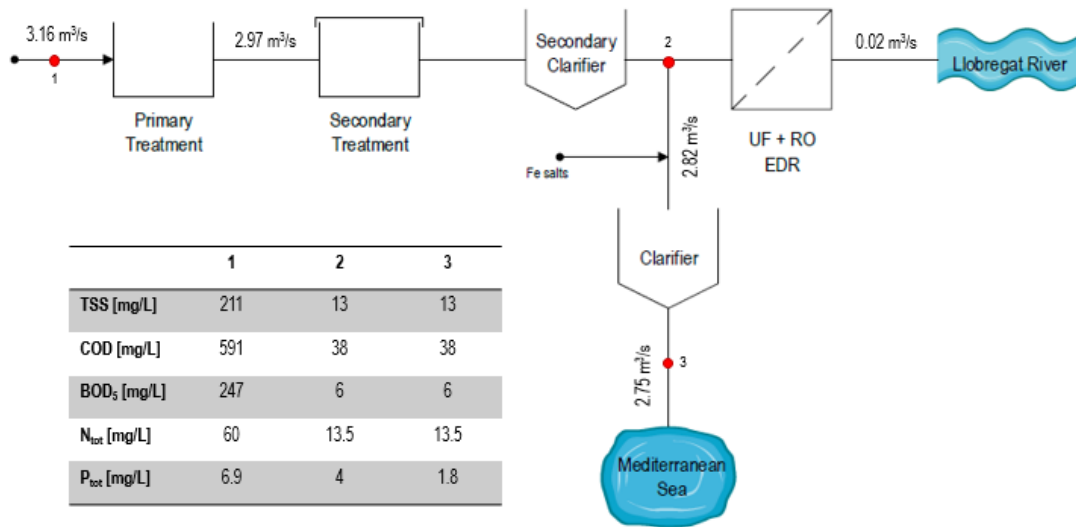
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147 The current phosphorus removal scheme in BLI-WWTP (Figure 2a) and the proposed scheme for  
148 nutrients recovery (Figure 2b) are depicted in Figure 2. The flow distribution shown in Figure 2b is  
149 defined in order to obtain a final P concentration below 2 mgP/L, as established by EU regulation  
150 (Mas-Pla et al., 2006).

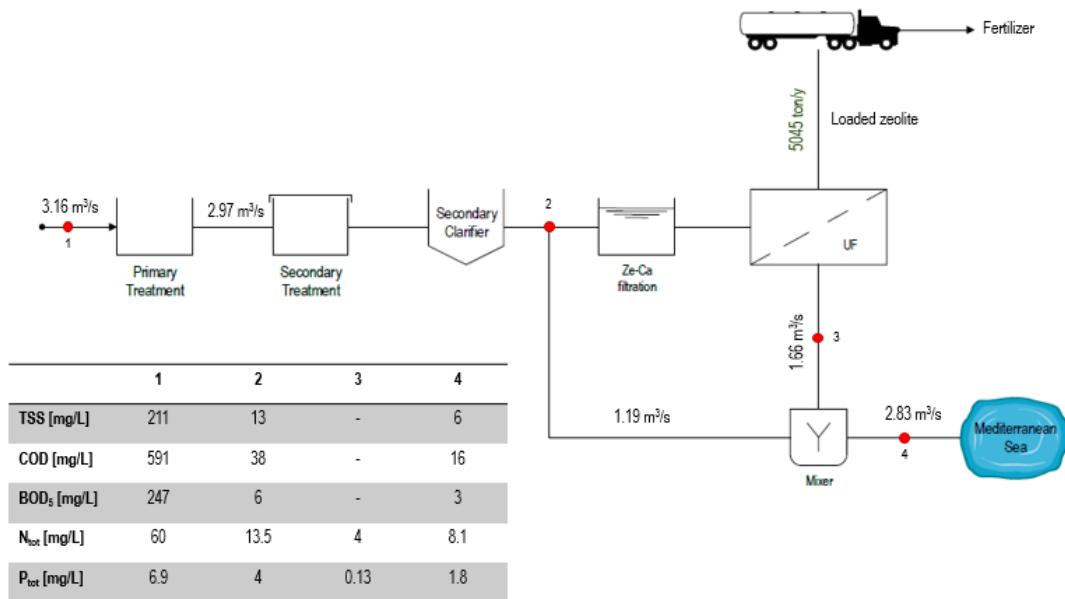
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152

a)



b)



154 Figure 2: a) Current and b) proposed working scheme and sampling data for recovery of nutrients at the  
 155 BLI-WWTP. Flow-rates and composition of the main parameters have been provided by the Metropolitan  
 156 Area of Barcelona (Àrea Metropolitana de Barcelona, 2017a).

157

158 It is worth mentioning that the average wastewater sampling data shown in Figure 2 are from 2010,  
 159 however, the BLI-WWTP has not introduced any significant technical modifications since then;



160 therefore, the average composition of the initial and treated wastewater has not presented relevant  
161 changes and can be used for this analysis. However, BLI-WWTP total treated flow is updated to  
162 the latest available records (2015).

163

### 164 **2.3. Financial Assessment**

165 Financial ratios were used in this work for assessing the economic feasibility of implementing a  
166 nutrients recovery unit based on zeolite sorbents in the BLI-WWTP. The net present value (NPV),  
167 internal rate of return (IRR), return of investment (ROI) and payback period (PP) were estimated  
168 for this purpose.

169 Net Present Value (NPV) (Eq. 1) is expressed as the difference between the current value of cash  
170 of inflows and outflows over a period and it is used to analyze the profitability of any investment.

$$NPV = \sum_{t=1}^T \frac{B_t - C_t}{(1 + r)^t} - I_0 \quad \text{Eq. 1}$$

171 where  $B_t$  and  $C_t$  are the inflows and outflows at the period  $t$ ,  $r$  is the discount rate, and  $I_0$  is the  
172 investment at  $t=0$ .

173 Internal Rate of Return (IRR) is calculated by solving the Eq. 2 and it specifies whether the project  
174 breaks even with an NPV of zero; if the obtained result is greater than the discount rate, the project  
175 is feasible.

$$0 = \sum_{t=1}^T \frac{B_t - C_t}{(1 + IRR)^t} - I_0 \quad \text{Eq. 2}$$

176 Return of Investment (ROI) (Eq. 3) is a measure to evaluate the efficiency of an investment, since  
177 it measures the amount of return of an investment in relation to the cost of investment.

$$ROI = \frac{\text{Gain from investment} - \text{Cost of investment}}{\text{Cost of investment}} \times 100 \quad \text{Eq. 3}$$

178 The Payback Period (PP) (Eq. 4) is the time required to recover the cost of the investment. For ROI  
179 calculation, a lifetime of 20 years has been considered taking as a reference the values reported  
180 for gravity filtration units in WWTPs (Machado et al., 2007)

$$PP = \frac{\text{Cost of investment}}{\text{Annual Gain from investment}} \quad \text{Eq. 4}$$

181 The investment is required for the installation of zeolite filtration tanks, as well as for the pumping  
182 systems and the modification of the plant pipelines. No further investment is needed as the zeolite  
183 filtration/separation (Alkas et al., 2013; Foreman, 1985; Hansen, 1997) will be performed by  
184 integration of the existing UF modules in the tertiary treatment stage of the regeneration station.

185 For zeolite filtration tank dimensioning it was considered the BLI-WWTP maximum treatment flow,  
186 the volume of zeolite for targeting a phosphorus concentration of 0.05 mg/L and the volume of  
187 wastewater for 60 minutes of HRT by using a scaling factor of 2 to the kinetic parameter obtained  
188 at the laboratory scale (Table 2). Taking into account these criteria it was determined that the  
189 volume needed for the filtration tanks was 860 m<sup>3</sup>.

190 The OPEX were calculated considering the cost of sorbent as well as an increase 5% of the current  
191 BLI-WWTP OPEX (8.4 M €/year) due to the significant increase of operational demand of UF  
192 modules in terms of energy and maintenance. Moreover, taking into account a lifetime of the UF  
193 membrane of 10 years, an annual amortization of 10% of total cost of UF modules was considered  
194 (2.9 M €) composed of hollow fiber UF membranes with a total active surface of 288000 m<sup>2</sup> able to  
195 obtaining a filtration flow up to 2 m<sup>3</sup>/s (Originblue, 2017).

196 Finally, as the loaded zeolite contains calcium phosphate (You et al., 2017a) it can be sell as Triple  
197 SuperPhosphate (TSP) fertilizer with approximately a 15% of phosphorus nutrient content.  
198 According to Maaß, (2014) the commodity price for fertilizer which contains 20% of phosphorus  
199 nutrient is set on 220 €/ton. In addition, the implementation of the zeolite filtration system would  
200 lead to a saving in the costs related to the iron salt used as coagulant to limit the phosphorus levels

201 in the discharge water according to the current regulation. According to a non-published study  
 202 performed by SUEZ Spain, the average cost of the phosphorus chemical removal is estimated on  
 203 0.7 €/kg P<sub>in</sub>.

204 **3. Results and Discussion**

205 **3.1. Financial Assessment**

206 For the estimation of CAPEX, the cost reported by Saiz (2010) was taken as a reference for a 1000  
 207 m<sup>3</sup> tank resulting in 250.6 k€ at 2010. Thus, considering a linear decrease of the cost with the tank  
 208 volume and a Retail Price Index (RPI) increase of 11.6 % (Instituto Nacional de Estadística, 2017)  
 209 from 2010 to December 2017, the investment for each sedimentation tank can be estimated on 239  
 210 k€. For achieving 1.8 mgP/L of total phosphorus concentration at the discharged wastewater  
 211 stream, the installation of zeolite filtration tank is needed in 7 operating lines, which leads to a cost  
 212 of 1673 k€.

213 Furthermore, according to the project for reusing BLI-WWT treated water quotation for the BLI-  
 214 WWTP regeneration station, pumping facilities and pipeline installations would cost around 150 k€  
 215 (Depuradora Baix Llobregat S.A., 2007), which represents a total initial investment of 1823 k€.

216 Wastewater production in Metropolitan Area of Barcelona have been quite constant with a  
 217 fluctuation of ±1% in the last 3 years, thus, for the financial assessment during BLI-WWTP lifetime,  
 218 an annual increase of treated flow of 1%, a sorbent cost of 115 €/ton and the UF membrane price  
 219 of 10 €/m<sup>2</sup> were considered. Finally, a discount rate of 4% was considered, as it was the mean  
 220 value in Euro Area since year 2000 for reliable business (Federal Reserve Bank of St. Louis, 2018).

221 A summary of variables considered for the economic analysis is listed in the Table 3.

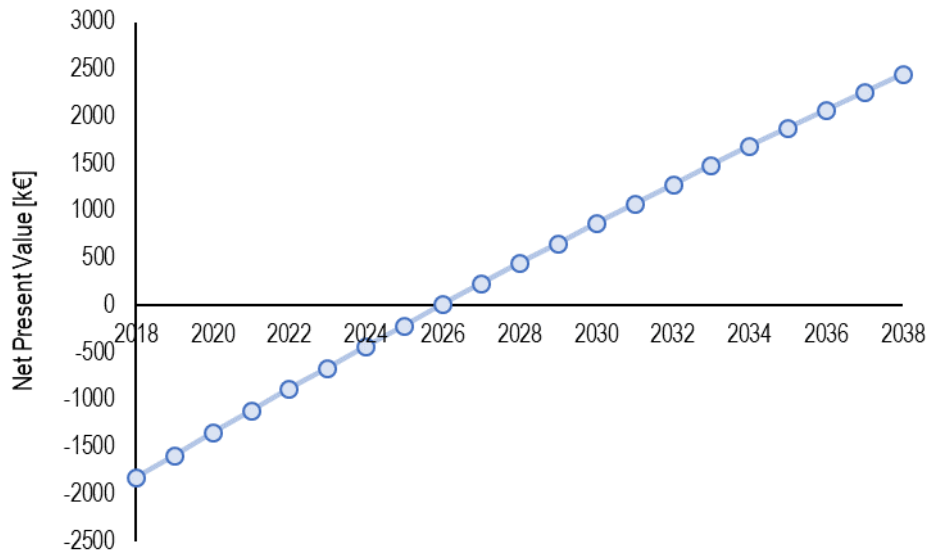
222 Table 3: Summary of considered variables for economic assessment

BLI-WWTP lifetime	20 years	Raw zeolite price	115 €/ton
P <sub>tot</sub> after zeolite filtration	0.01 mgP/L	Loaded zeolite (15% of PO <sub>4</sub> <sup>3-</sup> content)	220 €/ton

$P_{\text{tot final}}$	1.8 mgP/L	Chemical cost saving	0.7 €/kg $P_{\text{in}}$
HRT	60 minutes	UF membranes	288000 m <sup>2</sup>
Variation of BLI-WWTP treated flow	+ 1% per year	UF membranes price	10 €/m <sup>2</sup>
Discount rate	4%		

223

224 The expected evolution of NPV (according to Eq. 1 - 4) is exhibited in Figure 3.



225

226 Figure 3. Variation of Net Present Value (k€) during WWTP lifetime.

227

228 The NPV values are plotted as a function to time (years) (Figure 3), indicating that positive values  
 229 can be reached after 8 years of the operation of the nutrients recovery system.

230 Few data are available in the literature in terms of payback periods (PP) for the implementation of  
 231 nutrients recovery option on WWTPs. The most successful technology in terms of wide deployment  
 232 is the P recovery units from side-streams of sludge anaerobic digestion. Published reports from  
 233 technology suppliers or WWTP facilities show that similar PPs have been reported from 10 to 20  
 234 years, as it depends mainly on the price allocated for recovered struvite, which fluctuates from  
 235 negative values to positive values (300 €/ton struvite) (Cornel and Schaum, 2009; Dockhorn, 2009;  
 236 Peng et al., 2018).

237 The financial ratios were calculated in order to assess the feasibility of implementing a zeolite  
238 filtration system for nutrients recovery from the BLI-WWTP and are summarized in [Table 4](#).

239 Table 4: Financial indexes estimated according for the nutrients recovery in the BLI-WWTP

Net Present Value [k€]	2354.2
Internal Rate of Return [%]	14.9
Return of Investment [%]	356.95
Payback Period [years]	7.4

240

241 As shown in results ([Table 4](#)), the investment in nutrients recovery system is economically feasible  
242 with a short PP and the IRR is greater than the discount rate considered. It is worth mentioning that  
243 these results are due to the existence of the UF unit as part of the regeneration station. Otherwise,  
244 the cost of the UF equipment and the installation of its control systems is estimated at 9.1M €  
245 ([Depuradora Baix Llobregat S.A., 2007](#)) and the results of the financial ratios would be less  
246 favorable as summarized in [Table 5](#).

247 Table 5: Financial ratios estimated according for the nutrients recovery in the BLI-WWTP including UF unit

Net Present Value [k€]	-6396
Internal Rate of Return	-4.20
Return of Investment [%]	60
Payback Period [years]	44.4

248 Thus, the implementation of this technology for phosphorus and nitrogen recovery from wastewater  
249 secondary treated effluent is not feasible for small WWTPs that do not have tertiary treatment  
250 facilities based on membrane technologies (e.g., UF).

### 251 3.2. Sensitivity analysis

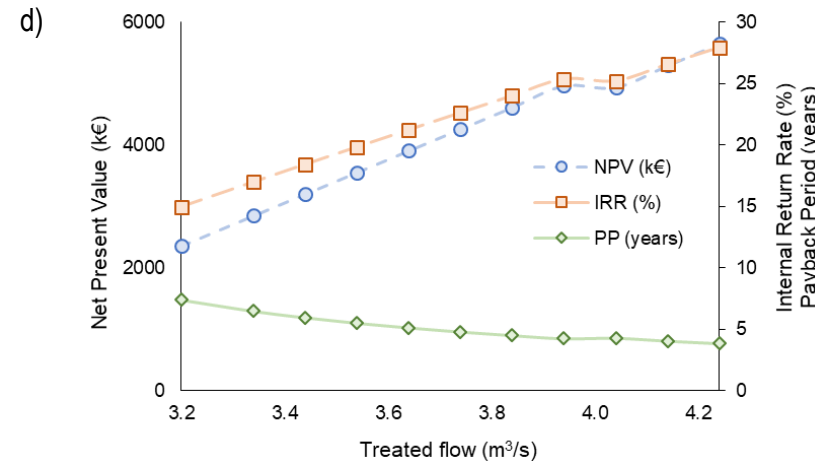
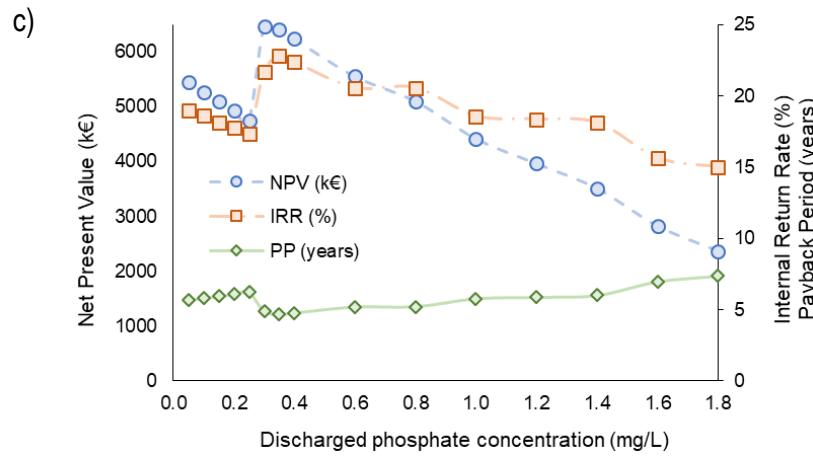
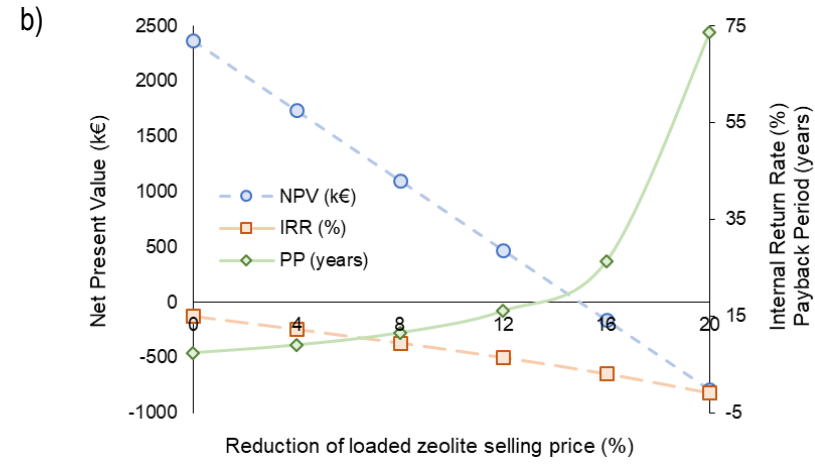
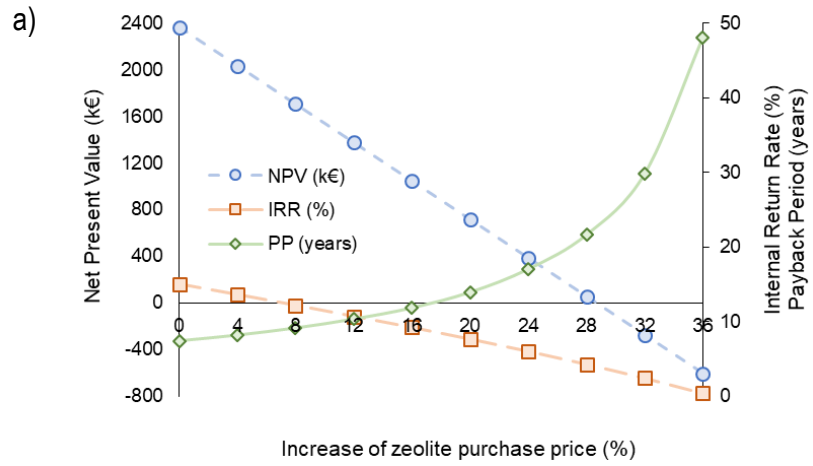
252 Considering that a lifetime of 20 years has been defined for this analysis, it is expected that some  
253 parameters will not be constant. Then, a sensitivity analysis was performed considering five  
254 scenarios as follows: i) increasing the cost of zeolite; ii) reduction of the market price of loaded  
255 zeolite rich in nutrients; iii) reducing phosphorus discharge limit; iv) increasing treated flow-rate,  
256 and v) variation of the discount rate. The sensitivity analysis was carried out considering the  
257 variations in the following key parameters:

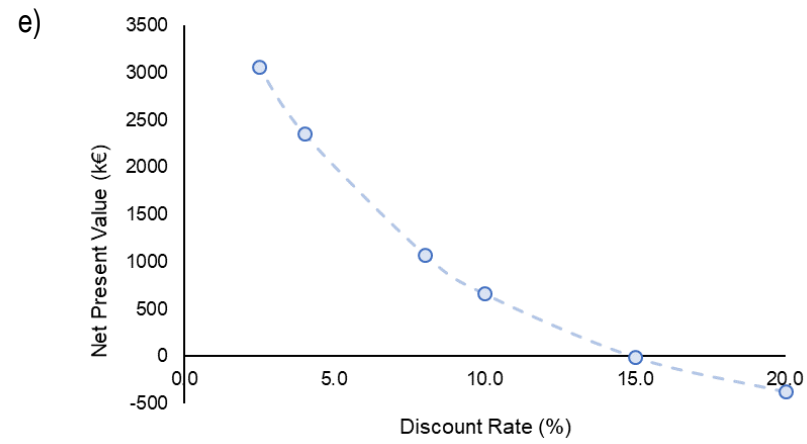
258 i. The price of raw and loaded zeolites is assessed with variations of 4% taking into account possible  
259 market fluctuations as well as Retail Price Index increase along the project lifetime.

260 ii. The variation of phosphorus discharge limit is set at 0.2 mg/L for concentrations higher than 0.4  
261 mgP/L and at 0.05 mg/L for concentrations lower than 0.4 mgP/L. These two variation of the  
262 discharge limits are set according to technical possibilities for reducing phosphorus content in  
263 wastewater treated effluents.

264 iii. The WWTP treated flow is assessed in increment intervals of 0.1 m<sup>3</sup>/s according to the increase  
265 of the population in the Metropolitan Area of Barcelona and the trend in water consumption shown  
266 in the last five years.

267 iv. The variation of the discount rate evaluates the case of investment for private companies with  
268 not predictable growth (20%), private companies that are scaling predictably (10%) as well as public  
269 companies (2.5%). In addition, other intermediate values of the discount rate were studied. The  
270 financial ratios resulting from the sensitivity analysis are shown in the [Figure 4](#).





272 Figure 4: Variation of financial ratios by varying a) the zeolite purchase price; b) the zeolite loaded selling price; c) the phosphorus discharge limit; d) the treated flow; and e) the  
 273 discount rate.



274 **Increasing the cost of zeolite:** As is shown in [Figure 4a](#)), with an increase in the purchase price  
275 of zeolite higher than 28%, an IRR of 3.9 is obtained, lower than the considered discount rate (4%);  
276 as well as a negative NPV. These results indicate that the implementation of nutrients recovery  
277 system for nutrient recovery is not economically feasible.

278 As the Ze-Ca is obtained by hydrothermal synthesis from fly ash ([Querol et al., 1996](#)), it is important  
279 to improve the efficiency of the process to avoid a significant increase in the cost of the sorbent as  
280 well as reduce environmental impact of chemical and energy consumption in the synthesis stage.  
281 The main reduction of the zeolite cost, according to the analysis of the synthetic route of the zeolite  
282 production, is associated to the final stage of drying. As the sorption process could be carried out  
283 using zeolites in a slurry mode the cost of the zeolite could be reduced by a factor of two if the  
284 zeolites are not dried ([Industrias Químicas del Ebro, n.d.](#)).

285 **Reduction of the market price of loaded zeolite with nutrients:** Sensitivity analysis reported  
286 that if zeolite selling price decreases over 15 %, the IRR would be lower than the discount rate of  
287 4% and the PP would be 23 years, which means that the investment related to the construction of  
288 zeolite filtration tanks and pumping system would not be recovered along the project lifetime.

289 Since there is a great interest in the recovery of nutrients from WWTP, it is feasible to expect a  
290 reduction in the price of phosphorus-based fertilizer. Therefore, the efficiency of the sorption  
291 process is a key parameter that would allow increasing the N and P content in the loaded sorbent  
292 and increase its value in the market.

293 In the case of Europe, the inclusion of phosphate rock as one of the elements inside the Critical  
294 Raw Materials List ([European Commission, 2017](#)), the recovery of P from secondary resources will  
295 be mandatory. It has been estimated that up-to 30-40% of the total P needs at EU level could be  
296 recovered from the urban waste water cycle, and this has been traduced that in countries like  
297 Switzerland recovery of nutrients from WWTP is an obligation from 2016 ([United Nations World](#)

298 [Water Assessment Programme, 2017](#)). The main initiatives have been centered on the recovery of  
299 P from sewage sludge side-streams as struvite or as phosphoric from mono-incineration ashes of  
300 sewage sludge. In both cases the economic feasibility of the technologies is not clear; however, a  
301 policy and regulatory framework is being developed to support both recovery options.

302 **Reducing phosphorus discharge limit:** As the proposed WWTP configuration implies the  
303 installation of zeolite filtration tanks in only 7 working lines in order to minimize the CAPEX, the  
304 reduction of discharge limits implies the need of more filtration tanks. Thus, more investment is  
305 needed for the installation of additional filtration tanks and related pumping systems as well as a  
306 for UF membranes due to the shorter lifetime, which results in a fluctuation of the financial ratios  
307 shown in [Figure 4c](#).

308 However, more restrictive regulation in phosphate discharge limits would not affect negatively the  
309 economic feasibility of the implementation of the nutrients recovery system. On the contrary, as  
310 shown in [Figure 4c](#), a stricter regulation would lead to an increase in NPV and IRR, as well as a  
311 reduction in the PP.

312 **Increasing treated flow:** Increasing treated flow leads to a slightly improvement of all financial  
313 ratios according to sensitivity analysis, which corresponds to the expected increase in treated  
314 capacity of WWTP and consequently more loaded zeolites could be produced and potentially  
315 disposed as fertilizer.

316 **Variation of the discount rate:** as can be seen in [Figure 4e](#)), the fluctuation of the discount rate  
317 could lead to a significant variation of NPV during project lifetime, since the sensitivity analysis  
318 reported negative NPV values when considering a discount greater than 15% while if considering  
319 the water management is carried out by a public company, it is obtained 3063 k€ as NPV.

320

321 After conducting the financial assessment of the implementation of zeolite filtration system for  
322 nutrient recovery, an average OPEX/treated flow of 0.119 €/m<sup>3</sup> was obtained, significantly lower  
323 than 0.15 €/m<sup>3</sup> for PhosphoReduc (see Supplementary Material). If it is compared with Necovery  
324 treatment, which is currently being developed by CETaqua for Nutrient and Energy Recovery in  
325 Waste Water Treatment Plants by pre-concentration and Adsorption processes, the operating cost  
326 is slightly higher than 0.114 €/m<sup>3</sup>, reported in a medium size WWTP in Barcelona metropolitan  
327 Area.

328 Currently, the operating cost of BLI-WWTP is estimated at 0.084 €/m<sup>3</sup>, slightly lower than 0.119  
329 €/m<sup>3</sup> after implementing the zeolite filtration system. However, if an analysis is made of total value  
330 of the recovery of nutrients taking into account the savings in chemicals, the production of fertilizers,  
331 the improvement of the operation and the performance in the BLI-WWTP, the net balance is an  
332 economic benefit of 0.002 €/m<sup>3</sup>.

333 Furthermore, it is important to point out other non-economic benefits (externalities) as protection  
334 and improvement of Water Quality or food Security improvement and social equity (Mayer et al.,  
335 2016). Thus, the implementation of zeolite filtration system for nutrient recovery from WWTP  
336 secondary effluents leads to additional benefits as:

- 337 i. Promotes circular economy by valorizing the fly ash, a byproduct of coal power plant, as  
338 a sorbent for nutrients recovery (Mayer et al., 2016)
- 339 ii. Reduces the environmental issues due to the metal lixiviation of fly ash disposal (Izquierdo  
340 and Querol, 2012)

341 However, internalizing these benefits is beyond the scope of this study, although it can certainly  
342 provide a better economic equilibrium when positive externalities are expressed in monetary terms.

343

344

345

#### 346 **4. Conclusions**

347 In this study, the feasibility of implementing a simultaneous ammonium and phosphate recovery  
348 system, based on the sorption by a calcium-activated synthetic zeolite, in a large WWTP  
349 (>1.000.000 PE) as it is the case of the BLI-WWTP in the Barcelona Metropolitan Area was  
350 assessed.

351 Results show that the implementation of this alternative technology in BLI-WWTP is economically  
352 profitable, since it reported a PP of 7.5 years and an IRR of 15%, higher than considered discount  
353 rate. It is important to point out that these values are obtained due to the existence of an UF unit in  
354 the regeneration station of the studied WWTP. Otherwise, the required CAPEX would be  
355 considerable higher and the economic evaluation may not result feasible.

356 Sensitivity analysis showed that the critical parameters in economic feasibility are those related  
357 with the purchase or sale of the sorbent, an increase in the cost of the sorbent (28%) and a  
358 decrease in the sale price (15%) could make the implementation economically unfeasible.

359 More research is needed in synthesis and activation of zeolites to reduce the effects of price  
360 fluctuation of the sorbent. In addition, further studies on the performance of nutrients uptake and  
361 the potential use of loaded zeolites at the pilot plant scale are needed, which will allow to evaluate  
362 the economic feasibility of its implementation.

363 Finally, before the implementation of the nutrients recovery system in a WWTP it is necessary to  
364 consider the logistics necessary to evacuate 5000 tons/y of loaded zeolites, which according to  
365 [Blachowski \(2014\)](#), would be evacuated weekly through road transport by using trucks.

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373

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