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#### Validation of a gonio-hyperspectral imaging 1 system based on light-emitting diodes for the 2 spectral and colorimetric analysis of automotive 3 coatings 4

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In this study, a novel gonio-hyperspectral imaging system based on light-emitting diodes for the analysis of automotive coatings was validated colorimetrically and spectrally from 368 to 1309 nm. A total of 30 pearlescent, 30 metallic, and 30 solid real automotive coatings were evaluated with this system, the BYK-mac and X-Rite MA98 gonio-spectrophotometers, and also with the SPECTRO 320 spectrometer for further comparison. The results showed very precise correlations, especially in the visible range. In conclusion, this new system provides a deeper assessment of goniochromatic pigments than current approaches due to the expansion of the spectral range to the infrared. © 2017 Optical Society of America

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#### 1. INTRODUCTION 20

Goniochromatic pigments, also called effect or gonioapparent 21 22 pigments, are known by their appearance changes as a function of the angles of illumination and observation [1-3]. These 23 changes can affect both color and texture, resulting in very 24 25 diverse visual impressions. Accordingly, they are classified as pearlescent pigments, which mainly exhibit hue and chroma 26 27 shifts, and metallic pigments, which show lightness variations; 28 the traditional absorption pigments with a constant angular appearance are designated as solids. These pigments have 29 30 acquired relevance in the industry during the last two decades, specifically in the automotive, cosmetic, printing, and packag-31 32 ing sectors [2,4].

The angle-dependent coatings prompted the definition of a 33 new angular concept, the aspecular angle, which corresponds to 34 the angle between the specular reflection and the direction of 35 36 observation. Two additional concepts, the interference and 37 aspecular lines, were subsequently generated (Fig. 1). These 38 lines are used in the representation of the visual appearance 39 of goniochromatic samples in a color space. The aspecular angle remains constant along the interference line, while the illumi-40 41 nation angle is variable. However, in the aspecular line the 42 illumination angle remains invariable. The main function of

the interference line is to reveal abrupt shifts in hue and chroma for different illumination angles (pearlescent pigments), in contrast to the aspecular line, where lightness shows the most significant variation when moving far away from the specular reflection (metallic pigments).

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The growing use of coatings based on goniochromatic pigments called for the characterization at different illumination and observation geometries. Since traditional devices included just one fixed configuration, the multi-angle or goniospectrophotometers were created to provide more accurate assessments of effect pigments through a larger variety of measurement geometries [5]. At the same time, new standards for the complete evaluation of these pigments were issued by the German Institute for Normalization (Deutsches Institut für Normung, DIN) and the American Society for Testing Materials (ASTM) [6-8]. First, the guidelines for the analysis of metallic pigments were detailed in DIN 6175-02 and ASTM E2194. The measurement geometries described the fixed angle of illumination for the correct assessment of lightness variations along the observations angles. Since these two standards could not accurately characterize pearlescent pigments, a specific standard, ASTM E2539, was later issued. This new standard recommends two illumination angles since chroma and hue

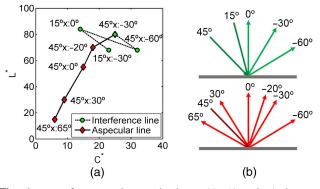


Fig. 1. Interference and aspecular lines: (a)  $C^*$  and  $L^*$  diagram F1:1 F1:2 showing the behavior along the different measurement geometries. F1:3 (b) Measurement geometries for the interference (top) and aspecular F1:4 lines (bottom).

shifts of pearlescent pigments mostly appear for different direc-66 tions of illumination. Table 1 summarizes the measurement 67 68 geometries recommended by these three standards.

In addition, values were established for the aperture angle 69 70  $(2\sigma)$  between the sample and the illumination and observation directions, defined as the angle subtended by the sensor or the 71 72 light source with respect to the center of the sample. For ASTM 73 E2194 and ASTM E2539, the angle should be  $2\sigma < 8^{\circ}$  and equal for both directions, while DIN 6175-2 specifies the value 74 75 of these angles for each measurement geometry. Furthermore, this standard differentiates between constant and variable direc-76 tions, which can refer to the illumination or observation beams, 77 depending on which has the fixed element. Therefore, the 78 aperture angle for the constant direction must be  $2\sigma \leq 5^{\circ}$ 79 and for variable directions  $2\sigma_{-20^{\circ}} \le 4^{\circ}$ ,  $2\sigma_{0} \le 4^{\circ}$ ,  $2\sigma_{30} \le 10^{\circ}$ , 80 and  $2\sigma_{65} \leq 10^{\circ}$ . Another condition is the CIE 1964 standard 81 observer (10°) proposed by the Commission Internationale 82 83 del'Éclairage (CIE). The colorimetric features of goniochro-84 matic pigments require a large field of view evaluation due 85 to the broad spatial distribution of pearlescent and metallic particles over the sample. 86

In view of these developments, all large companies 87 involved in color measurement (Datacolor, Konica Minolta, 88 GretagMacbeth, X-Rite, BYK Additives & Instruments, 89 90 Hunterlab, etc.) have launched desktop or portable goniospectrophotometers. The major driving force has been the 91 92 interest of the automotive industry in improving the visual 93 quality control of car finishes. Indeed, the automotive industry

Table 1. Measurement Geometries of DIN 6175-02, ASTM E2194, and ASTM E2539 Standards ([Angle of Illumination with Respect to the Normal] x: [Angle of Observation with Respect to the Normal])

Sta	undards	Measurement Geometries				
	N 6175-02, TMs	45° × : -20°	$45^{\circ} \times :0^{\circ}$	45° × :30°	45° × :65°	
	TM E2194, 539	45° × : -30°				
AS	TM E2539	$45^{\circ} \times :-60^{\circ}$	$15^{\circ} \times :0^{\circ}$	$15^{\circ} \times :-30^{\circ}$		

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is still the sector with a stronger demand for goniometric analysis.

Experimental gonio-spectrophotometers have also been developed with diverse operating principles and providing additional parameters: gonio-spectro-photometry based on the spectral bidirectional reflectance distribution function (sBRDF) [9,10], direct measure of the gloss at various geometries [11,12], and versatile optomechanical designs for measurements at several geometries [13]. Despite the good performance of commercial and experimental goniospectrophotometers, the data generally result from integrating the information of a few square millimeters of the target object. Consequently, they lack spatial resolution. For this reason, these devices can be considered to not properly estimate perceptual aspects of a surface as psychophysical experiments with real observers. At this point, the combination in hyperspectral imaging of colorimetric and textural assessments required for 110 the special visual attributes of these coatings was considered 111 to be the best approach to overcome these constraints. 112

The combination of gonio-spectrophotometers and spectral 113 imaging systems has generated a new kind of instruments 114 known as gonio-spectral imaging systems or multi-angle 115 spectral imaging systems, with the main objective to obtain 116 spectral images at different geometries. The first approaches 117 to gonio-spectral imagery focused on the analysis of three-118 dimensional pieces of artwork [14-16], and later extended 119 to two-dimensional objects such as paper and cloth samples 120 [17,18]. The illumination system consisted of a wide spectrum 121 light source and sets of interference filters resulting in a large 122 and mechanically complex structure. However, it is now pos-123 sible to obtain the spectral sampling directly from the light 124 source without added elements by means of light-emitting di-125 odes (LEDs). The advantages of LEDs are widely known: they 126 are very efficient, present a long life cycle, evolve constantly, are 127 comparatively economical, and have a small size. In addition, 128 these diodes have a narrow spectral emission, and they are avail-129 able at several wavelength peaks along different spectral ranges 130 (ultraviolet, UV; visible, VIS; and infrared, IR). Another rel-131 evant advantage of LED technology is the modulation of their 132 emission as a function of the forward current. 133

In the existing literature, goniochromatic pigments have only been evaluated in the VIS range of the electromagnetic spectrum, since it is the region where the main appearance shifts occur [19-21]. However, an analysis of the angular dependence at deeper layers through IR illumination would further elucidate the behavior of these pigments. Furthermore, ultraviolet lighting can contribute to a better insight into possible fluorescence. Thus, an extended spectral inspection might provide valuable information on the performance of these coatings in a broad range of bands of the electromagnetic spectrum.

This paper presents the validation of GOHYLED, a new 145 gonio-hyperspectral imaging system based on LEDs, developed 146 for the spectral and colorimetric evaluation of automotive 147 coatings. This initial verification will establish the basis for 148 future work on spatially resolved assessments. GOHYLED is 149 specifically intended to work in an extended range from the 150 UV to IR by using commercial, high power LEDs, in contrast 151

#### **Research Article**

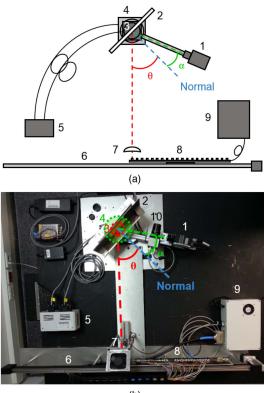
152 with conventional gonio-spectral systems that only use wide 153 spectrum light sources that exclusively cover the VIS range.

#### 154 **2. EXPERIMENTAL SETUP**

155 The experimental setup was based on the requirements for the study of automotive coatings in a wide spectral and angular 156 range specified by the DIN 6175-2, ASTM E2194-09, and 157 158 ASTM E2539-08 standards [6–8]. However, it might be useful for other applications and configurations. Essentially, the 159 GOHYLED is composed of a spectral light source, two cameras 160 (UV-VIS and IR) that cover the 368-1309 nm range, and two 161 rotation stages with a total rotation angle of 180° in both 162 observation and illumination directions (Fig. 2). All elements 163 were controlled through a purpose-built graphical user interface 164 developed with MATLAB R2013a, which allows the individual 165 and synchronized use of the light source, cameras, and motor-166 ized rotation stages. 167

#### 168 A. Light Source

The light source consists of 28 high power surface-mounteddevice (SMD) LED clusters of different peak wavelengths that spectrally illuminate the sample and a linear actuator that sequentially positions each cluster in front of it. A white



(b)

F2:1 Fig. 2. Developed gonio-hyperspectral imaging system based on F2:2 LEDs represented in (a) a layout and in (b) a picture: 1, UV-VIS camera; 2, sample holder; 3, 8MR191-30 rotation stage; 4, 8MR191-30-F2:3 28 rotation stage; 5, rotation stages controller; 6, linear actuator; 7, F2:4 F2:5 lens; 8, LED clusters; 9, light source controller and power supply; 10, IR camera, which is not represented in (a).  $\theta$  refers to the illumi-F2:6 nation angle controlled by the 8MR151-30 rotation stage and  $\alpha$  to the F2:7 F2:8 observation angle handled by the 8MR191-30-28 rotation stage.

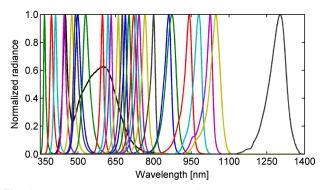


Fig. 3. Normalized spectral radiance of the LEDs included in the<br/>GOHYLED system.F3:1<br/>F3:2

LED cluster was also incorporated for the subsequent spatial evaluation of texture, which is not included in this work. 174 The clusters are composed of three or six LEDs, depending on the radiance emitted. A lens to increase the amount of light over the sample was also incorporated. Figure 3 shows the normalized spectral radiance, and Table 2 contains the part number and peak wavelengths of the whole set of LEDs. 179

The LEDs were purchased from Roithner LaserTechnik 180 GmbH (Part numbers RLCU and SMB1N) and Lumileds 181 Holding B.V. (Part numbers LX). The UV-VIS LEDs 182 (368-774 nm) presented a mean spectral step between con-183 secutive peak wavelengths of around 20 nm, whereas in the 184 IR (807-1309 nm), this value increased to 40 nm. The 185 FWHM in the UV-VIS range varies from 10 to 37 nm and 186 from 30 to 80 nm in the IR. The higher FWHM and the sub-187 sequent overlapping of the spectra in the IR range partially 188 compensated the larger distance among peak wavelengths. 189 Even though it causes a coarser sampling, the broader 190 FWHM is a typical feature of current IR solid-state technology 191 that is still unsolved. Moreover, IR LEDs present less variety of 192 wavelengths, especially those of high power-thus the signifi-193 cant gap before the spectrum with a peak wavelength of 194 1309 nm in Fig. 3. 195

Table 2. Part Numbers and Peak Wavelengths ( $\lambda_p$ ) of the 28 Types of LEDs

Part Number	$\lambda_p$ [nm] Part Number		$\lambda_p$ [nm]
RLCU-440-365	368	SMB1N-700	709
RLCU-440-390	397	RLCU-440-720	724
RLCU-440-410	411	SMB1N-735	735
LXML-PR01-0500	446	SMB1N-750	748
LXML-PB01-0040	476	SMB1N-770	774
SMB1N-490	489	SMB1N-810D	807
LXML-PE01-0070	498	SMB1N-850D	867
LXML-PM01-0100	528	SMB1N-870	885
LXML-PL01-0060	601	SMB1N-940D	952
LXM2-PH01-0070	622	RLCU-440-970	984
LXM2-PD01-0050	634	RLCU-440-1020	1033
LXM3-PD01	663	RLCU-440-1050	1052
SMB1N-670D	678	SMB1N-1300	1309
SMB1N-690D	693	LXW8-PW40	449/599 <sup>a</sup>

"Peak wavelengths of the two peaks for the white LEDs.

#### Vol. 56, No. 29 / / Applied Optics

The use of high power LEDs was driven by the aperture 196 angles recommended by the standards. To achieve such small 197 angles, the illuminating and sensing areas should have been 198 extremely reduced, limiting the evaluation to a minute fraction 199 200 of the samples. However, one of the objectives of this work was 201 to evaluate bigger areas than current devices and to obtain spatially resolved images. To this end, the LEDs were placed at a 202 203 distance of 580 mm in order to leave enough free space for the rotation of the acquisition arm around the sample. But the long 204 distance and the angle of emission of the LEDs (120°) resulted 205 in a low illumination of the sample. To solve this issue, a plano-206 convex lens from Edmund Optics (stock #67-228) with a focal 207 length of 75 mm, a diameter of 50 mm, and a transmittance of 208 209 90% from 200 to 1300 nm was selected. The relative position between the LEDs and the lens was out of focus to avoid an 210 image of the LED chips to form on the sample. The lens back 211 surface was finally placed 25 mm from the LEDs; this was 212 experimentally determined and ensured a uniform illumination 213 over the sample. This configuration of the light source pro-214 duced an aperture angle of 4.69°, which was below the maxi-215 mum tolerance of the ASTM E2194 and E2539 (8°) and DIN 216 6175-2 (5°) standards, considering for the latter the illumina-217 tion beam as the constant direction. 218

219 The linear actuator ZLW-0630-02-B-60-L-1000 from 220 Igus S.L., and a stepper motor SY42STH47-1206A from Changzhou Songyang Machinery & Electronics Co., Ltd., 221 222 executed the sequential positioning of the LED clusters, resulting in a minimum step of 140 µm. Each LED cluster was 223 switched on only when it was placed in front of the sample 224 and behind the lens. The images were then acquired by the 225 camera, the LEDs were switched off, and the next cluster 226 was placed in the same position to repeat the process. With 227 228 this method, only one LED cluster was switched on at a time.

#### 229 B. Imaging Sensors

Table 3 contains the technical features of the two cameras used. 230 The acquisition unit included a CM-140 GE-UV monochro-231 matic CCD camera from JAI AS, with enhanced UV sensitivity, 232 and a GMUV42528C 2.8/25 mm quartz lens from GOYO 233 OPTICAL Inc. selected specifically for its high transmittance 234 from 200 to 1300 nm. The InGaAs camera was a Hamamatsu 235 C10633-23 with a lower spatial resolution and exposure time 236 and no available gain factor. A Kowa LM12HC-SW 1.4/ 237 12.5 mm SWIR lens with high transmission from 800 to 238 239 2000 nm was coupled to this camera. The spatial resolution of the IR camera did not pose a problem since the validation 240 of the proposed system was performed by means of averaged 241 reflectances of the images. However, it can limit future spatial 242 evaluations. 243

The acquisition was made in a two-step process. The UV-VIS camera was employed to acquire images when using

Table 3. Technical Features of the Cameras

Camera	UV-VIS	IR	
Spectral range [nm]	200-1000	900-1650	
Sensor size [px]	$1392 \times 1040$	320 × 250	
Bit depth	10	14	

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the LED clusters with peak wavelengths from 368 to 952 nm, and the IR camera for peak wavelengths from 984 to 1309 nm. The images for the whole set of measurement geometries were first captured with the UV-VIS and second with the IR camera.

The aperture angles of the observation stage also conformed to the standards. The minimum distance between the sample and the cameras was based on the maximum diameter of the entrance pupil. Since it can be obtained dividing the focal length by the minimum F-number, the lenses of both cameras presented the same value of 8.93 mm. However, the distance to the sample was different for each camera because the position of the entrance pupil was different for each lens, at 14.1 mm for the UV-VIS lens and at 10.7 mm for the IR lens, both inward. Consequently, the minimum distances between the sample and the outer part of the cameras' lenses were 113.8 mm for the UV-VIS and 117.1 mm for the IR. Finally, the UV-VIS camera was positioned at 218 mm from the sample to increase the area observed; this resulted in one aperture angle of 2.20°. The IR camera was located at 129 mm from the sample to avoid any collision with the sample holder; this distance variation generates an aperture angle of 3.66°. A longer distance was not used for this camera because of its wider field of view and lower spatial resolution. Both cameras conformed to the tolerance of the ASTM E2194 and E2539 (8°) and DIN 6175-2 (4°) standards, considering for the latter the observation beam as the variable direction. Although these standards only regulate the measurement of goniochromatic pigments in the VIS range, the same conditions were applied to the IR due to the lack of regulations in this range.

To capture images within the dynamic range of the cameras, exposure time and gain varied throughout the measurement geometries and for the different acquisition channels. Besides the emission power of each LED cluster, the spectral sensitivity of the cameras and the angular distance between the illumination and observation direction also conditioned these parameters.

## **C. Motorized Rotation Stages**

The changeable angular positioning was obtained using two 283 motorized rotation stages manufactured by STANDA Ltd, 284 the 8MR151-30 and the 8MR191-30-28. Both have a rotation 285 range of 360°, an angular resolution of 0.01°, and a central 286 aperture of 30 mm. At the top, the 8MR151-30 stage controls 287 the illumination angle by rotating the sample, while at the bot-288 tom, the 8MR191-30-28 controls the observation direction by 289 positioning the cameras around the sample. Figure 2 shows a 290 graphical description of the angular positioning of each stage. 291

#### 3. METHODS

#### A. Samples

A total of 30 pearlescent, 30 metallic, and 30 solid samples were 294 selected; they presented a rectangular size between 90 mm × 295 150 mm and 100 mm × 200 mm. The 90 samples originated 296 from AUDI AG, BASF SE, and PPG Industries Inc. commer-297 cial car paints. In addition to the measurements carried out 298 with the GOHYLED system, these samples were measured 299 with the BYK-mac (BYK-Gardner GmbH) and X-Rite 300 MA98 (X-Rite Inc.) gonio-spectrophotometers and also the 301

for further comparisons.

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**B. Multi-Angle Color Measurement** 

305 The GOHYLED system was designed and built considering the measurement geometries, aperture angles, and CIE stan-306 307 dard observer recommended by the DIN 6175-2, ASTM E2194-09, and ASTM E2539-08 standards (Table 4). The 308 aperture angle for the UV-VIS camera was eventually smaller 309 because the diaphragm size of the camera lens was diminished 310 (f/11) to enhance the focus at the 368–952 nm spectral range. 311 In contrast, the IR camera used a greater diaphragm (f/2.8) to 312 ensure a good signal-to-noise ratio, since IR LEDs had lower 313 power than VIS LEDs. Furthermore, the focus was less critical 314 than in the UV-VIS region because the IR camera operated 315 with LEDs in a range of only 300 nm. The measurement area 316 317 or region of interest (ROI) was determined for the UV-VIS camera because its field of view was more limited. 318

SPECTRO 320 spectrometer (Instruments Systems GmbH)

The major benefit of conforming to ASTM and DIN spec-319 ifications is the possibility of performing a precise comparison 320 of readings among instruments of different optical design. The 321 measurements obtained with the GOHYLED system were 322 compared to those of the BYK-mac and X-Rite MA98 gonio-323 spectrophotometers. These devices are calibrated for all the 324 geometries against ceramic standards of the British Ceramic 325 Research Association, known as BCRA tiles. The BYK-mac 326 conforms only to the DIN 6175-2 and ASTM E2194 stan-327 dards, whereas the X-Rite MA98 and the GOHYLED conform 328 to the three standards (DIN 6175-2, ASTM E2194, and 329 ASTM E2539). With a fixed illumination direction, the 330 BYK-mac is particularly suitable for the evaluation of metallic 331 pigments, but it cannot characterize the changes of hue and 332 333 chroma that appear in pearlescent pigments for different illumination directions. Similarly to the GOHYLED, the BYK-334 335 mac performs the spectral sampling by means of LEDs and can evaluate sparkle and graininess, both textural effects of 336 goniochromatic pigments. On the other hand, the X-Rite 337 MA98 can produce complete assessments of pearlescent and 338 metallic pigments since it includes the 45° and 15° illumination 339 angles required by the standards. It also includes other obser-340 vation angles outside the conventional plane of illumination/ 341 observation, and a diffraction grating performs the spectral 342 sampling. Besides the standard, the BYK-mac and X-Rite 343 MA98 also perform evaluations at the  $45^{\circ} \times :-60^{\circ}$  measure-344 345 ment geometry. Therefore, the spectral and colorimetric results obtained with the GOHYLED system were fully comparable to 346 those of the X-Rite MA98, whereas only the geometries sug-347 gested by the DIN 6175-2 and ASTM E2194 standards, 348 45° × : -30°, 45° × : -20°, 45° × :0°, 45° × :30°, and 45° × :65°, 349

Table 4. F-Number, Aperture Angles  $(2\sigma)$ , Spatial Resolutions (SR), and Regions of Interest (ROI) for Each Camera

T4:1	Camera	F-Number	<b>2σ</b> [°]	SR [px/mm]	ROI [mm]
T4:2	UV-VIS	<i>f</i> /11	0.56	28	50 × 37
T4:3	IR	<i>f</i> /2.8	1.83	3	50 × 37

plus  $45^{\circ} \times :-60^{\circ}$ , were used to compare with the results of the 350 BYK-mac. 351

# C. Measurement Stability and Repeatability

The stability and repeatability of the measurement procedure were also evaluated through the acquisition of images of a white reference BN-R98-SQ10C from Gigahertz Optik GmbH at the geometry of  $45^{\circ} \times :0^{\circ}$  with both cameras and the quantification of the mean digital level variation.

First, the stability of all the spectral channels was examined by switching every LED cluster on and off 10 times and each time capturing 10 images, which were subsequently averaged. The purpose of these tests was to accurately reproduce the final measurement mechanism, in which the LED clusters were used as flashes of light. Next, the influence of the sample positioning on the holder was evaluated. This study encompassed the comparison of measurements with and without the replacement of the sample among repetitions.

In order to reduce other sources of bias such as temporal noise, sets of three, five, and 10 averaged frames were tested for the two cameras at the geometries of  $45^{\circ} \times :-60^{\circ}$ ,  $45^{\circ} \times :-30^{\circ}$ ,  $45^{\circ} \times :-20^{\circ}$ ,  $45^{\circ} \times :0^{\circ}$ ,  $45^{\circ} \times :30^{\circ}$ , and  $45^{\circ} \times :65^{\circ}$ , using the white reference mentioned before.

The proposed system also dealt with spatial noise removal, in this case by applying Eq. (1) to each acquired image:

$$I_{C}(i,j) = k \frac{I(i,j) - I_{B}(i,j)}{I_{U}(i,j) - I_{B}(i,j)},$$
(1)

where  $I_C(i, j)$ , I(i, j),  $I_B(i, j)$ , and  $I_U(i, j)$  correspond to the 374 digital levels of the corrected, raw, background or dark, and 375 uniform field or white reference images, respectively; k is 376 the calibrated reflectance of the reference provided by the 377 manufacturer. I(i, j),  $I_B(i, j)$ , and  $I_U(i, j)$  images were always 378 acquired in the same conditions of exposure time and gain, 379 which change for each acquisition channel and measurement 380 geometry. Images of the calibrated white reference were cap-381 tured and used as uniform field targets, as well as dark or back-382 ground images with all LEDs turned off. The results derived 383 from Eq. (1) were directly expressed as reflectance images. 384

The evaluation of the positioning repeatability of the rota-385 tion stages was carried out by means of the UV-VIS camera 386 attached to the 8MR191-30-28 stage through the acquisition 387 arm at the distance previously calculated (218 mm from the 388 sample). A graph paper divided into 1 mm squares was used 389 as the sample to quantify the deviation of the image recorded. 390 Positioning tests were performed for rotations of 30°, 10°, and 391 5°, first with one of the two elements fixed and afterwards mov-392 ing both; each rotation displacement was assessed three times. 393

# D. Extraction of Reflectance Spectra and Colorimetric Data

The spectral and color appearance data were retrieved by means of a purpose-developed image processing program using MATLAB R2013a. Its main functions were to calculate the reflectance spectra, spectral fitting metrics, chromatic coordinates, and color differences.

Reflectance images were obtained by means of Eq. (1). Throughout the whole spectral range of the GOHYLED system (368–1309 nm), the average reflectance values were also

determined for three ROIs: the ROI detailed in Table 4 and the 404 ROIs of the BYK-mac and the X-Rite MA98 gonio-spectro-405 photometers with diameters of 23 and 12 mm, respectively. 406 Although the ROIs of the GOHYLED system are square or 407 408 rectangular and those of the two gonio-spectrophotometers 409 are circular, the differences were considered negligible. These spectra were finally interpolated from 400 to 700 nm with a step 410 of 10 nm by applying a cubic spline algorithm [22,23], on 411 account of the input spectral range needed for calculating the 412 colorimetric values and color differences with respect to those 413 of the BYK-mac and X-Rite MA98. Regarding the IR range, 414 the spectra were validated with the measurements carried out 415 with the SPECTRO 320 spectrometer and the telescopic optical 416 417 probe TOP 100 from Instrument Systems GmbH and a halogen lamp at the geometries of  $45^{\circ} \times :30^{\circ}$ ,  $45^{\circ} \times :0^{\circ}$ , and  $15^{\circ} \times :0^{\circ}$ . 418 419 This device and all its accessories are calibrated against standards 420 of the National Institute of Standards and Technology (NIST) and the Physikalisch-Technische Bundesanstalt (PTB). The 421 spectral range went from 700 to 1309 nm with a step of 422 10 nm. No additional geometries were assessed since these were 423 424 considered sufficiently representative and also due to the lack of automation of the measurement process. 425

426 Additionally, the comparison of the spectra between the GOHYLED system and the BYK-mac, the X-Rite MA98, 427 and the SPECTRO 320 was completed through the mean ab-428 429 solute error (MAE), root mean square error (RMSE) [24,25], and goodness-of-fit coefficient (GFC) [26,27]. These metrics 430 431 were chosen because they are commonly used when comparing reconstructed spectral data [25,27,28]. Moreover, the combi-432 nation of the MAE and RMSE is useful to detect whether 433 values are caused by generalized large errors (RMSE ~ MAE) 434 or by a few errors greater than MAEs, such as outliers 435 (RMSE > MAE); both parameters are in the same units as 436 the analyzed data. On the other hand, the GFC is a relative 437 measure between 0 and 1 based on Schwartz's inequality, com-438 439 monly used when comparing spectra and, especially, color 440 differences [Eq. (2)]. According to the scale commonly linked to this parameter [27], a GFC  $\geq$  0.9950 is considered 441 "colorimetrically accurate," a GFC  $\geq 0.9990$  a "good spectral" 442 fitting," and a GFC  $\geq$  0.9999 an "excellent spectral fitting": 443

$$GFC = \frac{\left|\sum_{i}^{n} r_{o}(\lambda_{i}) r_{e}(\lambda_{i})\right|}{\sqrt{\sum_{i}^{n} [r_{o}(\lambda_{i})]^{2} \sum_{i}^{n} [r_{e}(\lambda_{i})]^{2}}},$$
(2)

444 where  $r_o(\lambda_i)$  is the original spectrum and  $r_e(\lambda_i)$  is the estimated 445 spectrum, both evaluated at the same wavelength  $\lambda_i$ ; *n* is the 446 total amount of wavelengths considered.

The colorimetric evaluations were performed under the
CIELAB color space [29,30]. The CIE standard illuminant selected was D65, similarly to BYK-mac and X-Rite MA98.
Color differences between these devices and the GOHYLED
were calculated with the CIEDE2000 [31,32] and AUDI2000
[33] color-difference formulas. The CIEDE2000 colordifference formula is defined as

$$\Delta E_{00} = \left[ \left( \frac{\Delta L'}{k_L S_L} \right)^2 + \left( \frac{\Delta C'}{k_C S_C} \right)^2 + \left( \frac{\Delta H'}{k_H S_H} \right)^2 + R_T \left( \frac{\Delta C'}{k_C S_C} \right) \left( \frac{\Delta H'}{k_H S_H} \right)^{\frac{1}{2}}, \quad (3)$$

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where  $\Delta L'$ ,  $\Delta C'$ , and  $\Delta H'$  are differences of lightness, chroma, and hue between two colors, respectively. This formula included parametric factors  $k_L$ ,  $k_C$ , and  $k_H$  for weighting lightness, chroma, and hue differences, respectively, according to the application. These three parameters are equal to 1 under the reference conditions proposed by the CIE [34,35]. In addition, three weighting functions,  $S_L$ ,  $S_C$ , and  $S_H$  for each lightness, chroma, and hue, were also included. Finally, the rotation term  $R_T$  was added to improve the performance for blue colors. The improved performance for objects that exhibit lightness values higher than 100 was a decisive factor, since this phenomenon is very common in goniochromatic pigments, especially under direct illumination conditions.

On the other hand, the AUDI color-difference formula was specially developed for the approval of goniochromatic paint batches as follows:

$$dE_{\gamma}' = \left[ \left( \frac{dL_{\gamma}^*}{k_{dL}s_{dL_{\gamma}}} \right)^2 + \left( \frac{dC_{\gamma}^*}{k_{dC}s_{dC_{\gamma}}} \right)^2 + \left( \frac{dH_{\gamma}^*}{k_{dH}s_{dH_{\gamma}}} \right)^2 \right]^{\frac{1}{2}}.$$
 (4)

The main difference with respect to the CIEDE2000 is that, in this case, the weighting functions  $(s_{dL_{\gamma}}, s_{dC_{\gamma}}, s_{dH_{\gamma}})$  depend on the measurement geometry.

#### 4. RESULTS AND DISCUSSION

The spectral reconstruction of the 90 samples comprised the entire spectral range of the GOHYLED system, from 368 to 1309 nm, with 28 acquisition channels, eight color measurement geometries, and three ROIs. Figure 4 shows two reflectance images of a pearlescent pigment at the geometries of  $45^{\circ} \times :-30^{\circ}$  and  $45^{\circ} \times :-20^{\circ}$  and for the LED cluster with a peak wavelength of 476 nm. The illumination gradient was not removed when dividing by the image of the white reference because it has a matte finish, whereas the automotive coatings were glossy. At this stage, a glossy white reference was not used to reach a more precise comparison with the BYK-mac and the X-Rite MA98, which also employ a matte white reference.

Figure 5 exhibits the reflectance spectra, and Fig. 6 the  $C^*$  versus  $L^*$  of three samples where the pearlescent, metallic, and solid effects were more noticeable. Measured samples showed the expected theoretical behavior that was also confirmed by the commercial devices. Chroma shifts were more evident in pearlescent samples due to variations of the reflectance spectrum in relation to wavelength and to the interference and aspecular lines. Luminance changes in goniochromatic samples

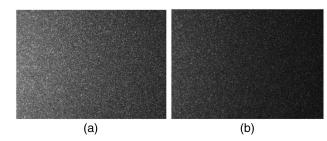
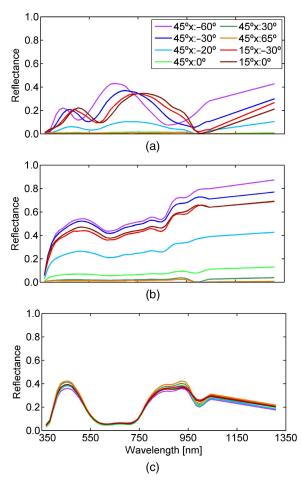


Fig. 4.Reflectance images of a pearlescent pigment at the geometries of (a)  $45^{\circ} \times : -30^{\circ}$  and (b)  $45^{\circ} \times : -20^{\circ}$  for the LED cluster withF4:1a peak wavelength of 476 nm.F4:3

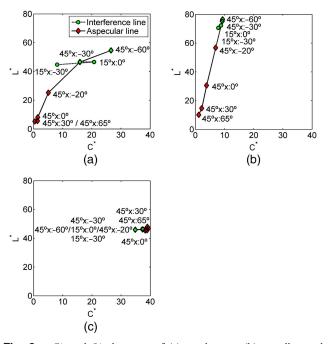


F5:1**Fig. 5.** Reflectance spectra of (a) pearlescent, (b) metallic, andF5:2(c) solid samples at  $45^{\circ} \times : -60^{\circ}, 45^{\circ} \times : -30^{\circ}, 45^{\circ} \times : -20^{\circ}, 45^{\circ} \times :0^{\circ},$ F5:3 $45^{\circ} \times :30^{\circ}, 45^{\circ} \times :65^{\circ}, 15^{\circ} \times : -30^{\circ}, and 15^{\circ} \times :0^{\circ}.$ 

were recorded as variations in reflectance [Figs. 5(a) and 5(b)] 494 and lightness [Figs. 6(a) and 6(b)]. Although this phenomenon 495 is the main attribute of metallic samples, it was also observed in 496 pearlescent samples because pearlescent pigments employed in 497 automotive coatings are commonly mixed with metallic par-498 ticles to integrate the two effects in one single paint. With 499 regard to solid samples, the spectral reflectance, chroma, and 500 501 luminance remained stable in the eight geometries with only minor fluctuations [Figs. 5(c) and 6(c)] 502

Figures 5(a), 5(b), 6(a), and 6(b) show that reflectance and 503 lightness values, respectively, were higher at the geometries 504 adjacent to the specular reflection  $(45^{\circ} \times :-60^{\circ}, 45^{\circ} \times :-30^{\circ},$ 505  $15^{\circ} \times :-30^{\circ}$ , and  $15^{\circ} \times :0^{\circ}$ ) and decreased drastically in the case 506 of the furthest geometries. On the other hand, the most signifi-507 cant changes in the spectral profile emerged when comparing 508 the measurements of geometries with the illuminant at differ-509 ent positions:  $45^{\circ} \times :-60^{\circ}$  and  $45^{\circ} \times :-30^{\circ}$  versus  $15^{\circ} \times :-30^{\circ}$ 510 511 and  $15^{\circ} \times :0^{\circ}$ . These geometries are recommended for the evaluation of color change due to pearlescent pigments [8]. 512

513 The following results are based on the average reflectance of 514 the images for a more precise comparison with the BYK-mac 515 and X-Rite MA98, since they do not offer pixel-wise reflectance 516 data. At this stage, the spatially resolved images were not



**Fig. 6.**  $C^*$  and  $L^*$  diagrams of (a) pearlescent, (b) metallic, andF6:1(c) solid samples at  $45^\circ \times :-60^\circ$ ,  $45^\circ \times :-30^\circ$ ,  $45^\circ \times :-20^\circ$ ,  $45^\circ \times :0^\circ$ ,F6:2 $45^\circ \times :30^\circ$ ,  $45^\circ \times :65^\circ$ ,  $15^\circ \times :-30^\circ$ , and  $15^\circ \times :0^\circ$ .F6:3

exploited because the main objective of this work was to 517 perform a preliminary spectral and colorimetric validation of 518 performance by means of comparing the new system against 519 two commercial gonio-spectrophotometers. The next stage will 520 focus on spatial features of goniochromatic pigments such as 521 sparkle, graininess, and mottling under broad-band and nar-522 row-band light sources. The deeper penetration of IR light will 523 provide a more accurate analysis of the goniochromatic particles 524 located at deeper layers of the coating and will also contribute 525 to quantify their influence on the total appearance of the pig-526 ment. Preliminary results have revealed a better discrimination 527 of some spatial attributes in the IR range due to the removal of 528 sparkle at this spectral region and for coatings of different 529 thickness.

#### A. Stability and Repeatability Performance

The results for stability assessments demonstrated excellent performance of all spectral channels with differences among repetitions below 5.75% for the UV-VIS camera and under 1.97% for the IR camera. The most outstanding shifts due to the influence of the sample positioning appeared when replacing it, but they were considered minor fluctuations because the deviation values never exceeded 4%.

Temporal noise analysis led to maximum differences below 1% when comparing the mean digital levels of the three sets of frames. This percentage was calculated with respect to the maximum digital level of each camera: 1023 for the UV-VIS and 16383 for the IR. The minimum number of frames (three) was selected for each acquisition.

The positioning repeatability evaluation of the rotation stages revealed a maximum positioning deviation under 1%, which confirmed the accuracy of both stages. 530 531

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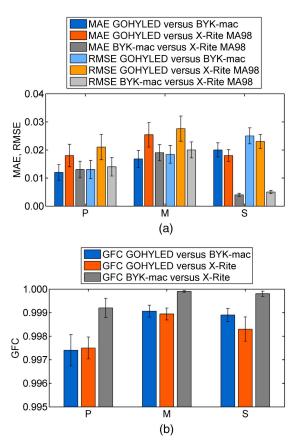
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#### 548 **B. Spectral Performance in the Visible Range**

The first data evaluated were the spectral reconstructions from 549 400 to 700 nm by means of the MAE, RMSE, and GFC. We 550 should stress that the MAEs and the RMSEs are expressed as 551 reflectance differences. These three metrics were computed for 552 the three ROIs and the three pigment categories. The perfor-553 mance among ROIs was very similar and validated the use 554 of the maximum measurement area without undermining 555 the fitting; therefore, only the results for the full ROI are 556 shown. Figure 7 plots the mean values considering the different 557 geometries for the three types of samples; each bar includes the 558 standard error as a measure of uncertainty. 559

The precise reconstructions obtained with the developed 560 system revealed that all the mean values of MAE and 561 RMSE were below 0.03 and very similar, which means that 562 very few outliers were found. The mean GFCs, all above 563 0.9900, also proved the color accuracy. The GOHYLED sys-564 tem and the BYK-mac exhibited slightly more similar behavior 565 than the X-Rite; in terms of MAE and RMSE this result was 566 similar to the result of comparing the two commercial devices. 567 568 With regard to the scale for the GFC, the evaluation of pearlescent and solid pigments can be considered "colorimetrically 569 accurate" since the mean values of this parameter were above 570



F7:1 Fig. 7. Mean values of (a) MAEs and RMSEs and (b) GFCs for the
F7:2 spectral reconstruction of the GOHYLED system with respect to the
F7:3 BYK-mac and the X-Rite MA98 and the comparison between two
F7:4 gonio-spectrophotometers. The three metrics were plotted for pearlF7:5 escent (P), metallic (M), and solid (S) samples. The error bars represent
F7:6 the standard error.

0.9950, while metallic pigments attained "good spectral fitting" 571 with values slightly above 0.9990. These last subsets of pig-572 ments also achieved correlations very similar to the correlations 573 between the two gonio-spectrophotometers. In agreement with 574 previous studies [36,37], the measurement geometries closer to 575 the specular reflection  $(45^{\circ} \times : -60^{\circ}, 45^{\circ} \times : -30^{\circ}, 15^{\circ} \times :30^{\circ},$ 576 and  $15^{\circ} \times :0^{\circ}$ ) resulted in larger differences. At these geometries, 577 the amount of light reflected is very high and any small varia-578 tion in position or configuration can produce substantial 579 deviations of the results. 580

Color differences again showed better correlations between the GOHYLED system and the BYK-mac, although the deviations with respect to the X-Rite MA98 were less noticeable than in the fitting metrics (Fig. 8). The greatest spectral and colorimetric match obtained for the GOHYLED system and the BYK-mac was probably due to the use of the same spectral filtering technique, i.e., LEDs, with similar spectral features such as the peak wavelength and the FWHM.

In general, the mean CIEDE2000 values were below 2 units with all instruments and for the three kinds of samples. These colorimetric differences remained within the ranges proposed in a previous study [38], where the authors suggested to widen color tolerances when using newer versions of standardized color-difference formulas such as the CIEDE2000; this study did not cover non-standard color-difference equations such as the AUDI2000. This tolerance proposal was based on the large numbers of factors that determine the reproduction of automotive coatings: add-on parts, closeness to the specular angle,  $L^* > 100$ , and visual texture. Considering all these circumstances, they recommended to apply a multiplication factor between 1.5 and 3 with respect to the visual discrimination threshold, traditionally equal to 1.

In contrast, the AUDI2000 color differences were larger, particularly for solid samples. It is known that this colordifference formula is stricter than the CIEDE2000, particularly for solid pigments, because their appearance is considered less complex and easier to reproduce than for goniochromatic pigments. Since the solid samples employed in this study

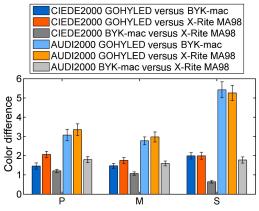


Fig. 8.Mean CIEDE2000 and AUDI2000 color differencesF8:1of the GOHYLED system with respect to the BYK-mac and theF8:2X-Rite MA98 and also the comparison between the two gonio-F8:3spectrophotometers for the full ROI. Both metrics were plotted forF8:4pearlescent (P), metallic (M), and solid (S) samples. The error barsF8:5represent the standard error.F8:6

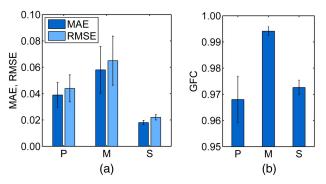
showed surfaces with more gloss than the pearlescent and
metallic, any minor variation in the configuration could cause
considerable variations among instruments. With regard to
Fig. 8, the values shown were calculated considering the whole
set of measurement geometries.

The comparisons with the GOHYLED system were very 614 similar to the comparison between the two commercial 615 616 gonio-spectrophotometers, especially for pearlescent and metallic pigments in terms of MAE, RMSE, and CIEDE2000. 617 We can thus infer that the BYK-mac and X-Rite MA98 present 618 differences of a magnitude similar to the GOHYLED. 619 However, the correlation of their measurements for solid pig-620 ments was better than with the proposed instrument. Indeed, 621 622 solid pigments showed a very glossy surface, to which the GOHYLED system seemed to be more sensitive than the 623 gonio-spectrophotometers. Since the ROIs employed were 624 the same as those of the commercial devices, the illumination 625 path might be considered responsible for these differences. A 626 collimated beam and/or a smaller aperture could increase the 627 fitting with the reference devices. Finally, even though the cor-628 relations presented provide valuable information, further vali-629 dation by means of psychophysical experiments is still needed. 630

### 631 C. Spectral Performance in the Infrared Range

Figure 9 shows the results of the validation of the IR range from 632 700 to 1309 nm. In this case, only the spectral fitting metrics 633 (MAE, RMSE, and GFC) were computed. Besides the full 634 ROI, the ROI of 12 mm was also analyzed, since it was the 635 most appropriate according to the measurement area of the 636 TOP 100 from the SPECTRO 320 spectrometer. Similarly 637 to the performance in the VIS range, no remarkable differences 638 were detected between the different ROIs in the IR range. 639 640 Consequently, only the results related to the full ROI are shown. 641

These results also proved the good performance of the developed system in the IR range, although they were less accurate
than in the VIS range due to the lower density of spectral bands,
the greater spacing among them, and their wider FWHMs.
Focusing on the results, the mean values of the MAEs and
the RMSEs were below 0.07 and especially small in the case
of the solid samples. The mean GFCs were above 0.9500, with



F9:1 Fig. 9. Mean values of (a) MAEs and RMSEs and (b) GFCs for the
spectral reconstruction of the GOHYLED system for the full ROI
F9:3 with respect to the SPECTRO 320. The three metrics were plotted
for pearlescent (P), metallic (M), and solid (S) samples. The error bars
F9:5 represent the standard error.

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the higher values obtained for the metallic samples just below 0.9950; therefore, the highest categories of the GFC scale were not reached in the IR. Results from the two ROIs revealed similar outcomes. Additionally, the geometries nearer to the specular reflection again caused the larger differences  $(45^{\circ} \times :-30^{\circ}, 15^{\circ} \times :0^{\circ})$ . Similarly, the values shown in Fig. 9 were calculated from the three measurement geometries.

Although the evaluation of goniochromatic pigments in the IR range is not common practice, it can provide useful spectral data on deeper layers of coatings, as well as additional information about visual effects that do not produce glint, such as graininess and mottling. Preliminary data obtained with the developed system have revealed that sparkling effects are extremely diminished in this region of the electromagnetic spectrum, and, therefore, they would not interfere with the assessment of other spatial phenomena such as those previously mentioned. For instance, IR light could also be used for the study of graininess instead of or in addition to diffuse VIS light.

#### 5. CONCLUSIONS

A gonio-hyperspectral imaging system based on LEDs has been developed and validated for the analysis of automotive coatings. The design conforms to the standards DIN 6175-2, ASTM E2194, and ASTM E2539 for multi-angle color measurement of goniochromatic pigments.

The system provided precise reconstructions of spectral reflectances when compared to commercial devices in the IR (SPECTRO 320) and especially in the VIS range (BYK-mac and X-Rite). The differences would decrease if both spectral ranges had similar density of spectral bands, similar spectral steps, and similar FWHMs. Unfortunately, current solid-state technology does not provide LEDs above 800 nm with these features. Similarly, color differences were smaller compared with the BYK-mac, although deviations with respect to the X-Rite were lower than for the previous metrics. In general, the mean CIEDE2000 values were within recommended tolerance ranges and smaller than the higher values of the AUDI2000 due mainly to the solid pigments.

A thorough examination of the correlations obtained with the whole spectral range revealed that the different ROIs showed analogous results. Another shared outcome was that the most sensitive geometries were those closer to the specular reflection,  $45^{\circ} \times :-60^{\circ}$ ,  $45^{\circ} \times :-30^{\circ}$ ,  $15^{\circ} \times :-30^{\circ}$ , and  $15^{\circ} \times :0^{\circ}$ for the VIS and  $45^{\circ} \times :-30^{\circ}$  and  $15^{\circ} \times :0^{\circ}$  for the IR.

Lastly, one of the main advantages of the GOHYLED 692 system is the inclusion of the spectral analysis in the two ranges 693 of the electromagnetic spectrum, VIS and IR, and for all 694 the measurement geometries recommended for the characteri-695 zation of goniochromatic pigments [6-8]. Currently, the 696 GOHYLED system is the only instrument with these attrib-697 utes. Ongoing research focuses on the assessment of spatial 698 effects such as sparkle, graininess, and mottling under white 699 light and narrow-band light sources. The higher spatial resolu-700 tion offered by the GOHYLED system in comparison with 701 other instruments makes it particularly suitable for this task. 702 Further studies will compare these results with those obtained 703 by means of psychophysical experiments to accurately validate 704 the performance of the GOHYLED system. 705

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