

1 **Life Cycle Assessment of high rate algal ponds for wastewater**
2 **treatment and resource recovery**

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25 **Abstract**

26 The aim of this study was to assess the potential environmental impacts associated with
27 high rate algal ponds (HRAP) systems for wastewater treatment and resource recovery
28 in small communities. To this aim, a Life Cycle Assessment (LCA) was carried out
29 evaluating two alternatives: i) a HRAP system for wastewater treatment where
30 microalgal biomass is valorized for energy recovery (biogas production); ii) a HRAP
31 system for wastewater treatment where microalgal biomass is reused for nutrients
32 recovery (biofertilizer production). Additionally, both alternatives were compared to a
33 typical small-sized activated sludge system. An economic assessment was also
34 performed. The results showed that HRAP system coupled with biogas production
35 appeared to be more environmentally friendly than HRAP system coupled with
36 biofertilizer production in the climate change, ozone layer depletion, photochemical
37 oxidant formation, and fossil depletion impact categories. Different climatic conditions
38 have strongly influenced the results obtained in the eutrophication and metal depletion
39 impact categories. In fact, the HRAP system located where warm temperatures and high
40 solar radiation are predominant (HRAP system coupled with biofertilizer production)
41 showed lower impact in those categories. Additionally, the characteristics (e.g. nutrients
42 and heavy metals concentration) of microalgal biomass recovered from wastewater
43 appeared to be crucial when assessing the potential environmental impacts in the
44 terrestrial acidification, particulate matter formation and toxicity impact categories. In
45 terms of costs, HRAP systems seemed to be more economically feasible when
46 combined with biofertilizer production instead of biogas. On the whole, implementing
47 HRAPs instead of activated sludge systems might increase sustainability and cost-

48 effectiveness of wastewater treatment in small communities, especially if implemented
49 in warm climate regions and coupled with biofertilizer production.

50

51 **Keywords:** Biogas; Environmental impact assessment; Fertilizer; Life Cycle
52 Assessment; Microalgae; Resource recovery

53 **1. Introduction**

54 High rate algal ponds (HRAPs) for wastewater treatment were introduced around 50
55 years ago and used since then not only to grow microalgae biomass but also to treat a
56 wide variety of municipal and industrial wastewaters (Cragg et al., 2014; Oswald and
57 Golueke, 1960). These systems are shallow, paddlewheel mixed, raceway ponds where
58 microalgae assimilate nutrients and produce oxygen, which is used by heterotrophic
59 bacteria to oxidise organic matter improving water quality (Craggs et al., 2014; Park et
60 al., 2011). Since mechanical aeration is not required, energy consumption in these
61 systems is much lower compared to a conventional wastewater treatment plant (e.g.
62 activated sludge system) (around 0.02 kWh m^{-3} of water vs. 1 kWh m^{-3} of water,
63 respectively) (Garfí et al., 2017; Passos et al., 2017). Moreover, HRAPs are less
64 expensive and require little maintenance compared to conventional systems (Cragg et
65 al., 2014; Garfí et al., 2017; Molinos-Senante et al., 2014). Due to their low cost and
66 low energy consumption, HRAP systems could have a wide range of applications in
67 Mediterranean regions, which present suitable climatic conditions for microalgae
68 growth (e.g. high solar radiation). However, to achieve a satisfactory performance, large
69 land area is required compared to conventional systems (around $6 \text{ m}^2 \text{ p.e.}^{-1}$ vs. 0.5 m^2
70 p.e.^{-1} for HRAP and activated sludge systems, respectively), making them more suitable
71 for small communities (up to 10,000 p.e.).

72 Nowadays, there is an important need to shift the paradigm from wastewater
73 treatment to resource recovery to alleviate negative effects associated with human
74 activities, such as pollution of water bodies, greenhouse gas (GHG) emissions and
75 scarcity of mineral resources. In this context, microalgae grown in HRAPs can be
76 harvested and reused to produce biofuels or other non-food bioproducts. In particular,

77 intensive research has been developed during the last years to investigate the potential
78 of microalgae to produce biofuels such as biogas. Indeed, the biogas produced from
79 microalgal biomass was found to contain high energy value, making microalgae
80 anaerobic digestion an attractive alternative for biofuel production (Chew et al., 2017;
81 Jankowska et al., 2017; Montingelli et al., 2015; Uggetti et al., 2017). On the other
82 hand, microalgae also offer the potential to recover nutrients from wastewater and,
83 subsequently, to be applied as a sustainable fertilizer. During the last decade, this
84 alternative has been described by several authors, considering the fact that microalgae
85 contain high amounts of proteins rich in essential amino acids, as well as
86 phytohormones that stimulate plant growth (Coppens et al., 2016; García-Gonzalez and
87 Sommerfeld, 2016; Jäger et al., 2010; Uysal et al., 2015).

88 Recent studies have employed the Life Cycle Assessment (LCA) methodology
89 to assess the environmental impact of HRAP systems for wastewater treatment. They
90 demonstrated that HRAPs might help to reduce environmental impacts and costs
91 associated with wastewater treatment compared to conventional systems (e.g. activated
92 sludge system), especially in small communities (Garfí et al., 2017; Maga, 2016). These
93 studies also highlighted that the LCA methodology is an appropriate tool to support
94 early-stage research and development of novel technologies and processes (Fang et al.,
95 2016; Garfí et al., 2017). Indeed, LCA methodology takes into account and quantifies
96 all environmental exchanges (i.e. resources, energy, emissions, waste) occurring during
97 all stages of the technology life cycle (Ferreira et al., 2014; Ferreira et al., 2017; ISO,
98 2000).

99 Nevertheless, to the best of the authors' knowledge, there are no studies
100 assessing the environmental impacts of HRAP system for wastewater treatment
101 considering different configurations for resource and energy recovery.

102 The objective of this work was to evaluate the potential environmental impacts
103 associated with HRAP systems for wastewater treatment taking into account two
104 resource recovery strategies. To this aim a LCA was carried out comparing the
105 following alternatives: (i) a HRAP system for wastewater treatment where microalgal
106 biomass is valorised for energy recovery (biogas production); (ii) a HRAP system for
107 wastewater treatment where microalgal biomass is reused for nutrients recovery
108 (biofertilizer production). For the sake of comparison, both scenarios were compared to
109 a typical small-sized activated sludge system. Additionally, an economic evaluation was
110 addressed in order to assess the feasibility of the HRAP alternatives based on the costs
111 and benefits related to each of them.

112 This paper is organized as follows: Section 2 describes the wastewater treatment
113 systems, as well as the methodology used for the LCA and the economic analysis; in
114 Section 3 the results of the comparative LCA and the economic analysis are described;
115 finally, in Section 4 the main conclusions are highlighted.

116

117 **2. Material and Methods**

118 ***2.1 Wastewater treatment systems description***

119 The HRAP systems were hypothetical wastewater treatment plants based on
120 extrapolation from lab-scale and pilot-scale studies (up to 100 m²). The systems were
121 designed to serve a population equivalent of 10,000 p.e. and treat a flow rate of 1,950

122 $\text{m}^3 \text{d}^{-1}$. The HRAP system coupled with biogas production was considered to be
123 implemented in Catalonia (Barcelona, Spain), where the mean temperature and global
124 solar radiation are 15.5°C and $4.56 \text{ kWh/m}^2\text{d}$, respectively (AEMET, 2017). For this
125 case study, the design parameters were calculated taking into account the experimental
126 results obtained in lab-scale and pilot systems (up to 5 m^2) located at the Universitat
127 Politècnica de Catalunya-BarcelonaTech (UPC) (Barcelona, Spain) (García et al., 2000;
128 García et al., 2006; Gutiérrez et al., 2016; Passos and Ferrer, 2014, Solé-Bundó et al.,
129 2015; Solé-Bundó et al., 2017). This system comprises a primary settler (Hydraulic
130 Retention Time (HRT) = 2.5 h) followed by four HRAPs (Table 1). From these units,
131 wastewater goes through a secondary settler (HRT = 3 h) where microalgal biomass is
132 harvested and separated from wastewater. Treated water is then discharged into a
133 surface water body. Part of the harvested microalgal biomass (2 and 10 % on a dry
134 weight basis in summer and winter, respectively) is recycled in order to enhance
135 spontaneous flocculation (bioflocculation) and increase microalgae harvesting
136 efficiency (Gutiérrez et al., 2016). The remaining harvested biomass is thickened (HRT
137 = 24 h), thermally pretreated (75°C , 10 h) and co-digested with primary sludge (35°C ,
138 20 days). The biogas produced is then converted in a combined heat and power (CHP)
139 unit, while the digestate is transported and reused in agriculture. In this context, the
140 HRT of each HRAP has to be modified over the year (8, 6 and 4 days) in accordance
141 with the weather conditions (i.e. solar radiation and temperature) in order to accomplish
142 wastewater treatment and meet effluent quality requirements for discharge (García et al.,
143 2000; Gutiérrez et al., 2016). For this reason, it was considered that during summer
144 months (from May to July) only two HRAPs work in parallel (HRT = 4 days), whereas
145 all of them are operated during winter months (from November to April) (HRT = 8

146 days). During the rest of the year (from August to October), the HRT is 6 days (3
147 HRAPs working in parallel).

148 The HRAP system coupled with biofertilizer production was considered to be
149 implemented in Andalucía (Almeria, Spain), where the mean temperature and global
150 solar radiation are 19.1°C and 5.29 kWh/m²d, respectively (AEMET, 2017). For this
151 case study, the designed parameters were determined using the results obtained in a pilot
152 system located at the Las Palmerillas Experimental Station (Almeria, Spain) (100 m²)
153 (Morales-Amaral et al., 2015a). This system consists of two HRAPs operating in
154 parallel and followed by a settler (HRT = 3 h) where microalgal biomass is separated
155 using an organic flocculant (Table 2). From this unit, treated wastewater is discharged
156 into a surface water body, while harvested microalgae biomass is dewatered on-site
157 using a centrifuge and later sold to a local company to produce a biofertilizer (NPK = 5-
158 1-0.75). The biofertilizer produced from the dewatered biomass is then transported and
159 reused in agriculture. In this case, due to the more favourable climatic conditions for
160 microalgae growth compared to Catalonia, the HRT was the same over the year (HRT =
161 3 days). It has to be noted that, for the same reason, the microalgal biomass production
162 is considerably higher in the system implemented in Andalucía with respect to the one
163 located in Catalonia (3-26 g_{TSS} m⁻² d⁻¹ vs. 15-30 g_{TSS} m⁻² d⁻¹, respectively) (Gutiérrez et
164 al., 2016; Morales-Amaral et al., 2015a).

165 For the sake of comparison, the potential environmental impacts of the HRAP
166 systems were compared to those generated by a conventional small-sized wastewater
167 treatment plant (10,000 p.e.). For that purpose, the design of a usual small-scale
168 activated sludge system implemented in Spain was taken into account (Gallego et al.,
169 2008; Garfí et al., 2017; Lorenzo-Toja et al., 2015). It comprises a primary settler,

170 followed by an activated sludge reactor with extended aeration and a secondary settler
171 (Table 3). Treated water is discharged into the environment and the sludge is
172 conditioned, thickened, centrifuged on-site and then transported to an incineration
173 facility.

174 Figure 1 shows the flow diagrams of the treatment alternatives. Table 1, 2 and 3
175 show the characteristics and design parameters of the HRAP and activated sludge
176 systems.

177 **Please insert Figure 1**

178 **Please insert Table 1**

179 **Please insert Table 2**

180 **Please insert Table 3**

181

182 ***2.2 Life Cycle Assessment***

183 The LCA was conducted following the ISO standards (ISO, 2000; ISO, 2006) in order
184 to evaluate and quantify the potential environmental impact of the investigated
185 scenarios. It consisted of four main stages: i) goal and scope definition, ii) inventory
186 analysis, iii) impacts assessment and iv) interpretation of the results (ISO, 2006). The
187 following sections describe the specific content of each phase.

188

189 ***2.2.1 Goal and scope definition***

190 The goal of this study was to determine the potential environmental impact of HRAP
191 systems for wastewater treatment and resource recovery. In particular, two
192 configurations were compared:

193 a) a HRAP system for wastewater treatment where microalgal biomass is

194 valorised for energy recovery (biogas production) (Scenario 1);
195 b) a HRAP system for wastewater treatment where microalgal biomass is reused
196 for nutrients recovery (biofertilizer production) (Scenario 2).

197 Moreover, both scenarios were compared to a typical small-sized activated sludge
198 system implemented in Spain (Scenario 3). The functional unit (FU) for this study was
199 set as 1 m³ of treated water, since the main function of the technologies proposed is to
200 treat wastewater.

201 The cradle-to-grave boundaries included systems construction, operation and
202 maintenance over a 20-years period (Garfí et al., 2017; Pérez-López et al., 2017;
203 Rahman et al., 2016) (Figure 1). Input and output flows of materials (i.e. construction
204 materials and chemicals) and energy resources (heat and electricity) were systematically
205 studied for all scenarios. Direct GHG emissions and NH₄⁺ volatilization associated with
206 wastewater treatment were also included in the boundaries. As treated water is
207 discharged into the environment, direct emissions to water were also taken into account.
208 Regarding digestate and biofertilizer reuse in agriculture in Scenarios 1 and 2,
209 transportation (20 km) (Hospido et al., 2004) and direct emissions to soil (heavy
210 metals), as well as direct GHG emissions, were accounted for. In the case of the
211 activated sludge system (Scenario 3), inputs and outputs associated with sludge disposal
212 (i.e. incineration) were also included in the boundaries. An average distance of 30 km
213 was considered for sludge transportation to incineration facilities, based on
214 circumstances generally observed in our zone. The end-of-life of infrastructures and
215 equipment were neglected, since the impact would be marginal compared to the overall
216 impact.

217 Since the studied scenarios would generate by-products (i.e. biogas,

218 biofertilizer), the system expansion method has been used following the ISO guidelines
219 (Guinée, 2002; ISO, 2006). In this method, by-products are supposed to avoid the
220 production of conventional products. Thus, the impact related to conventional products
221 is withdrawn from the overall impact of the system (Collet et al., 2011; ISO, 2006; Sfez
222 et al., 2015). In this study, the digestate and the biofertilizer produced in HRAP systems
223 coupled with biogas and biofertilizer production (Scenarios 1 and 2, respectively) were
224 considered as substitutes to chemical fertilizer. Moreover, the avoided burdens of using
225 heat and electricity produced in Scenario 1 (HRAP systems coupled with biogas
226 production), instead of heat from natural gas and electricity supplied through the grid,
227 were also considered.

228

229 *2.2.2 Inventory analysis*

230 Inventory data for the investigated scenarios are summarized in Table 4, 5 and 6. In the
231 case of HRAP systems coupled with biogas and biofertilizer production (Scenarios 1
232 and 2), inventory data regarding construction materials and operation were based on the
233 detailed engineering designs performed in the frame of this study. Treated wastewater
234 characteristics were estimated considering the removal efficiencies and experimental
235 results obtained in the pilot systems implemented at the Universitat Politècnica de
236 Catalunya-BarcelonaTech (UPC) (5 m²) (Gutiérrez et al., 2016) and at the Las
237 Palmerillas Experimental Station (100 m²) (Morales-Amaral et al., 2015a) for Scenarios
238 1 and 2, respectively. NH₄⁺ volatilization was estimated through nitrogen mass balance.
239 NH₃ and N₂O emissions due to the application of digestate and biofertilizer on
240 agricultural land were calculated using emissions factors from the literature (Hospido et
241 al., 2008; IPCC, 2006; Lundin et al., 2000). In this case, CH₄ emissions were not

242 considered since anaerobic decompositions do not occur if liquid fertilizer is used and
243 the climate is predominantly dry (Hobson, 2003; Lundin et al., 2000). Heavy metals and
244 nutrients (avoided Total Nitrogen (TN) and Total Phosphorous (TP)) content of the
245 digestate and biofertilizer were gathered from experimental results obtained in the
246 above-mentioned pilot systems (Morales-Amaral et al., 2015a; Solé-Bundó, et al.,
247 2017). In order to estimate electricity and heat production from biogas cogeneration in
248 Scenario 1 (HRAP systems coupled with biogas production), biogas production
249 obtained in lab-scale experiments was taken into account (Solé-Bundó et al., 2015;
250 Passos et al., 2017).

251 As mentioned above, data regarding the typical small-sized activated sludge
252 system implemented in Spain (Scenario 3) were gathered from the literature (Gallego et
253 al., 2008; Garfí et al., 2017; Lorenzo-Toja et al., 2015).

254 Background data (i.e. data of construction materials, chemicals, energy
255 production, avoided fertilizer, transportation and sludge incineration process) were
256 obtained from the *Ecoinvent 3.1* database (Moreno-Ruiz et al., 2014; Weidema et al.,
257 2013). The Spanish electricity mix was used for all electricity requirements (Red
258 Eléctrica Española, 2016).

259

260 **Please insert Table 4**

261 **Please insert Table 5**

262 **Please insert Table 6**

263

264 ***2.2.3 Impact assessment***

265 The LCA was performed using the software *SimaPro*[®] 8 (Pre-sustainability, 2014).

266 Potential environmental impacts were calculated by the ReCiPe midpoint method
267 (hierarchist approach) (Goedkoop et al., 2009). In this study, characterisation phase was
268 performed considering the following impact categories: Climate Change, Ozone
269 Depletion, Terrestrial Acidification, Freshwater Eutrophication, Marine Eutrophication,
270 Photochemical Oxidant Formation, Particulate Matter Formation, Metal Depletion,
271 Fossil Depletion, Human Toxicity and Terrestrial Ecotoxicity. These impact categories
272 were selected according to the most relevant environmental issues related to wastewater
273 treatment and used in previous LCA studies (Corominas et al., 2013; Fang et al., 2016;
274 Gallego et al., 2008; Garfí et al., 2017; Hospido et al., 2008). Normalisation was carried
275 out in order to compare all the environmental impacts at the same scale. This provides
276 information on the relative significance of the indicator results, allowing a fair
277 comparison between the impacts estimated for each scenario (ISO, 2006). In this study,
278 the European normalisation factors have been used (Europe ReCiPe H) (Goedkoop et
279 al., 2009).

280

281 **2.3. Sensitivity analysis**

282 In order to evaluate the influence of the most relevant assumptions have on the results, a
283 sensitivity analysis was performed considering the following parameters: NH₃
284 emissions due to the application of digestate and biofertilizer on agricultural land
285 (Scenario 1 and 2); N₂O emissions due to the application of digestate and biofertilizer
286 on agricultural land (Scenario 1 and 2); digestate and biofertilizer transportation
287 distance (Scenario 1 and 2). A variation of ± 10% was considered for all parameters and
288 the sensitivity coefficient was calculated using Eq. (1) (Dixon et al., 2003):

289

$$\text{Sensitivity Coefficient (S)} = \frac{(\text{Output}_{\text{high}} - \text{Output}_{\text{low}})/\text{Output}_{\text{default}}}{(\text{Input}_{\text{high}} - \text{Input}_{\text{low}})/\text{Input}_{\text{default}}} \quad (1)$$

290

291 where Input is the value of the input variable (e.g. NH₃ and N₂O emissions) and Output
292 is the value of the environmental indicator (e.g. Climate Change).

293

294 ***2.4 Seasonality***

295 Annual averages of potential environmental impacts from HRAPs scenarios (Scenario 1
296 and 2) were compared to those obtained considering the microalgal biomass production
297 achieved in summer and winter months (highest and lowest production, respectively;
298 Table 1 and 2) to assess their fluctuations over the year. In particular, the microalgal
299 biomass production considered for Scenario 1 (HRAP systems coupled with biogas
300 production) was 5 and 25 g_{TSS} m⁻² d⁻¹ for winter and summer months, respectively. On
301 the other hand, for Scenario 2 (HRAP systems coupled with biofertilizer production) a
302 microalgal biomass production of 15 and 30 g_{TSS} m⁻² d⁻¹ was considered for winter and
303 summer months, respectively.

304

305 ***2.5 Economic assessment***

306 The economic assessment was performed comparing the capital cost and the operation
307 and maintenance cost of Scenarios 1 and 2 (HRAP systems coupled with biogas and
308 biofertilizer production, respectively). The capital cost included the cost for
309 earthmoving and construction materials purchase. On the other hand, operation and
310 maintenance cost comprised costs associated with energy (electricity and heat)
311 consumption and chemicals purchase. In both scenarios, prices were provided by local
312 companies. For Scenario 1 (HRAP systems coupled with biogas production), the surplus
313 electricity generated from biogas cogeneration was supposed to be sold back to the grid.

314 Thus, the price of electricity sold to the grid was withdrawn from the overall operational
315 and maintenance cost of the system. For Scenario 2 (HRAP systems coupled with
316 biofertilizer production), the dewatered microalgae biomass is sold to a local company
317 (BIORIZON BIOTECH S.L.) to produce the biofertilizer (Romero-García et al., 2012).
318 Therefore, its price was withdrawn from the overall operational and maintenance cost of
319 the system. Other costs (e.g. labour costs, transportation) were assumed to be similar in
320 both scenarios and, thus, were not included in the analysis.

321

322 **3. Results and Discussion**

323 *3.1 Life Cycle Assessment*

324 *3.1.1 Characterization*

325 The potential environmental impacts associated with each alternative are shown in
326 Figure 2. Comparing HRAP scenarios (Scenarios 1 and 2), the results show that
327 Scenario 2 is the most environmentally friendly alternative in 7 out of 11 impact
328 categories. As far as Climate Change, Ozone Depletion, Photochemical Oxidant
329 Formation and Fossil Depletion Potentials are concerned, the potential environmental
330 impact of Scenario 1 was lower than Scenario 2. This was mainly due to the offset
331 energy generated from biogas cogeneration and the avoided fertilizer (Figure 2). In
332 particular, the electricity generated by biogas cogeneration (avoided electricity) was
333 around 9 times higher than that consumed for system operation in Scenario 1 (Table 4).
334 It means that the surplus electricity could be sold to the grid. This is in accordance with
335 previous studies that observed that, in a HRAP system for wastewater treatment, the
336 energy balance is always positive when microalgal biomass is co-digested with primary
337 sludge and the biogas is used to cogenerate electricity and heat (Passos et al., 2017).

338 Moreover, it has to be noticed that the contribution of the avoided fertilizer to the
339 overall impact was higher in Scenario 1 than Scenario 2 (Figure 2), since TN avoided
340 was higher in the former compared to the latter (25.9 vs. 5.77 g m⁻³ of water; Table 4
341 and 5). This can be explained by the fact that, despite TN content was higher in the
342 biofertilizer (5 g_{TN} kg_{biofertilizer}⁻¹) than in the digestate (1.89 g_{TN} kg_{digestate}⁻¹), a lower
343 amount of biofertilizer is produced in Scenario 2 (1.15 kg_{biofertilizer} m⁻³ of water)
344 compared to Scenario 1 (13.7 kg_{digestate} m⁻³ of water). Indeed, the total solids (TS)
345 content of the microalgal biomass obtained in Scenario 1 (2% TS) is lower compared to
346 Scenario 2 (20% TS) due to its dewatering step (i.e. centrifugation). Nevertheless, it has
347 to be mentioned that the biofertilizer is a higher quality product compared to the
348 digestate, since it contains high amounts of proteins rich in essential amino acids, as
349 well as phytohormones that stimulate plant growth and improve soil quality (Coppens et
350 al., 2016; García-Gonzalez and Sommerfeld, 2016; Jäger et al., 2010; Uysal et al.,
351 2015). However, these benefits were not taken into account in this study. Regarding
352 Terrestrial Acidification and Particulate Matter Formation Potentials, Scenario 2 showed
353 lower risks to endanger the environment because this configuration causes fewer
354 emissions to air (i.e. NH₃ emissions) derived from biofertilizer application to
355 agricultural soil compared to digestate from Scenario 1 (Table 4 and 5). With regards to
356 Freshwater and Marine Eutrophication Potentials, Scenario 1 showed higher
357 environmental impacts compared to Scenario 2. It is explained by the quality of treated
358 effluent (i.e. lower TN and TP removal efficiencies in Scenario 1 than in Scenario 2;
359 Table 4 and 5). The reason for this difference could be primarily due to the distinct
360 climatic conditions, since the average temperature and global solar radiation in
361 Catalonia (Scenario 1), as previously mentioned, are lower than in Andalucía (Scenario

362 2). Indeed, previous studies reported that nutrient removal efficiencies are improved
363 with higher temperature and solar radiation (Craggs et al., 2012; Mehrabadi et al.,
364 2016). Concerning Metal Depletion Potential, Scenario 1 would impair abiotic
365 resources more likely than Scenario 2. Since Metal Depletion Potential is mainly
366 influenced by construction materials, the lower environmental performance of Scenario
367 1 is owing to the larger surface area required for its implementation compared to
368 Scenario 2 ($4 \text{ m}^2 \text{ p.e.}^{-1}$ vs. $3 \text{ m}^2 \text{ p.e.}^{-1}$, respectively). As mentioned above, in the system
369 implemented in Catalonia (Scenario 1), a higher HRT is needed (especially during
370 winter months) compared to that implemented in Andalucía (Scenario 2) in order to
371 obtain a effluent quality suitable for discharge (García et al., 2000; Gutiérrez et al.,
372 2016, Morales-Amaral et al. 2015a; Morales-Amaral et al. 2015b). The influence of the
373 geographical location on the performance of HRAPs was also addressed in previous
374 studies, in which the use of this technology is not encouraged in northern regions, where
375 the climatic conditions are not favourable to promote efficient wastewater treatment and
376 biomass productivity (Grönlund and Fröling, 2014; Pérez-López et al., 2017).
377 According to this, it is noteworthy to mention that, since in this study the two HRAP
378 systems (Scenarios 1 and 2) were assumed to be implemented in locations with distinct
379 climatic conditions, it is not possible to define the best biomass valorisation strategy
380 (i.e. biogas vs. biofertilizer production). In fact, HRAP systems operating under similar
381 conditions should be considered in order to enable a better comparison. In regard to
382 Human toxicity and Terrestrial Ecotoxicity Potentials, Scenario 1 showed higher
383 environmental impacts compared to Scenario 2 due to the higher concentration of heavy
384 metals in the digestate than in the biofertilizer (Table 4 and 5).

385 According to the results presented in Figure 2, Scenarios 1 and 2 showed lower

386 environmental impacts in 6 out of 11 impact categories (i.e. Climate Change, Ozone
387 Depletion, Freshwater and Marine Eutrophication, Photochemical Oxidant Formation,
388 Fossil Depletion) compared to Scenario 3. This was primarily due to the lower energy
389 consumption needed for system operation in HRAP scenarios (Scenario 1 and 2) than in
390 the activated sludge system (Scenario 3) (Table 4, 5 and 6). On the other hand, HRAP
391 scenarios (Scenario 1 and 2) showed lower environmental performance in Metal
392 Depletion category (Figure 2), since a higher amount of construction materials are
393 needed for their implementation compared to the activated sludge system (Scenario 3).
394 Indeed, even if HRAP systems have low raw materials requirements for their operation,
395 a large amount of raw materials is needed for their construction. This fact could make
396 HRAP systems less favourable than conventional technologies (e.g. activated sludge
397 systems) in the abiotic resources depletion impact categories. Nevertheless, this
398 drawback can be overcome by implementing HRAP systems in smaller agglomerations
399 than that considered in this study (e.g. around 2,000 p.e.) (Garfí et al., 2017). As far as
400 Terrestrial Acidification, Particulate Matter Formation, Human Toxicity and Terrestrial
401 Ecotoxicity Potentials are concerned, the potential environmental impacts of HRAPs
402 scenarios (Scenario 1 and 2) were higher than that caused by the activated sludge
403 system (Scenario 3). It was mainly due to the NH_3 air emissions derived from NH_4^+
404 volatilization in HRAPs and to the heavy metals content in the digestate/biofertilizer
405 (emissions to soil). The results are consistent with previous studies that reported
406 increased toxicity in a comparative LCA by integrating a sidestream process into a
407 conventional wastewater treatment facility where microalgae are cultivated, harvested
408 and then used for fertigation (Fang et al., 2016). Furthermore, it was observed that the
409 higher impacts on terrestrial environments are unavoidable in cases where sludge and

410 nutrients from wastewater are recycled and reused in agriculture (Tangsubkul et al.,
411 2005). In order to address this issue, improved technologies to separate better heavy
412 metals from recycled sludge should be encouraged (Tangsubkul et al., 2005). In regard
413 to Freshwater Eutrophication Potential, the activated sludge system (Scenario 3) showed
414 higher potential environmental impact compared to Scenario 2, but lower impact than
415 Scenario 1. This was because of the higher outlet Phosphorous concentration in
416 Scenario 1 compared to the other scenarios, which might be related to the lower
417 nutrients removal efficiency caused by less favourable climatic conditions. Previous
418 studies observed that eutrophication and toxicity impact categories were mainly affected
419 by water discharge emissions and sludge management, indicating that the best
420 alternatives seem to be the ones that provide lower nutrients and heavy metals emissions
421 (Corominas et al., 2013). This corroborates with the results obtained with this study,
422 where the configuration with higher nutrients concentration in the effluent and higher
423 levels of heavy metals in the recycled biomass (Scenario 1) showed higher impacts in
424 those categories.

425 On the whole, HRAP systems coupled with biogas and biofertilizer production
426 (Scenario 1 and 2) showed similar environmental performance if compared to the
427 activated sludge system (Scenario 3). In particular, HRAPs environmental performance
428 is better than the conventional system in the climate change, ozone layer depletion,
429 photochemical oxidant formation, and fossil depletion impact categories. It was in
430 accordance with previous studies, which stated that, compared to a typical medium-
431 sized conventional wastewater treatment plant, a HRAP system coupled with biogas
432 production could offer clear benefits with regard to the protection of climate, protection
433 of fossil resources and ozone depletion (Maga, 2016). In order to reduce the

434 environmental impacts of HRAP systems for wastewater treatment and resource
435 recovery, the following improvements should be addressed and further assessed: i)
436 reducing NH_4^+ volatilization in HRAPs by controlling the pH through CO_2 injection; ii)
437 ensuring higher nutrients removal efficiencies by selecting a favourable geographical
438 location to implement the HRAP systems; iii) studying improved technologies to
439 separate heavy metals from recycled microalgal biomass; iv) improving HRAP design
440 in order to decrease the amount of construction materials used (e.g. excavation instead
441 of concrete structure).

442

443 **Please insert Figure 2**

444

445 ***3.1.2 Normalization***

446 The normalised results show that Freshwater Eutrophication, Marine Eutrophication,
447 Terrestrial Acidification and Human Toxicity Potentials are the most significant impact
448 categories for all the scenarios considered (Figure 3). These results are in accordance
449 with previous LCAs on wastewater treatment (Fang et al., 2016; Gallego et al, 2008;
450 Hospido et al., 2004). In these impact categories, Scenario 2 showed to be the most
451 environmentally friendly alternative.

452

453 **Please insert Figure 3**

454

455 ***3.2 Sensitivity analysis***

456 The results of the sensitivity analysis are shown in Table 7, where the most sensitive
457 inventory components are indicated by bold type.

458 The results showed that Terrestrial Acidification and Particulate Matter
459 Formation Potentials are somewhat sensitive to NH₃ emissions due to the application of
460 digestate on agricultural land in Scenario 1 (sensitivity coefficient around 0.3 for both
461 environmental indicators). Indeed, a 10% increase of this parameter would increase
462 these indicators by around 3%.

463 Similarly, Climate Change Potential showed to be somewhat sensitive to N₂O
464 emissions due to the application of digestate on agricultural land in Scenario 1
465 (sensitivity coefficient = 0.36). This means that a 10% increase in N₂O direct emissions
466 would increase this environmental indicator by 3.6%.

467 Moreover, Photochemical Oxidant Formation Potential showed to be sensitive to
468 digestate transportation distance in Scenario 1 (sensitivity coefficient = 2.7). Indeed, a
469 10% increase in digestate transportation distance would increase this environmental
470 indicator by 27%. The transport of the sludge to agricultural applications is not a fixed
471 parameter, as it depends on specific needs. However, the sludge is usually applied in
472 soil relatively close to the plant location (Pasqualino et al., 2009).

473 In conclusion, the results were found to be sensitive to digestate transportation
474 distance in Scenario 1. Nevertheless, since it mainly affect only one of the less
475 significant impact categories considered (i.e. Photochemical Oxidant Formation
476 Potential), it can be concluded that the main findings of this study are not strongly
477 dependent on the assumptions considered.

478

479

Please insert Table 7

480

481 **3.3 Seasonality**

482 The seasonal variation of the potential environmental impact for HRAPs scenarios
483 (Scenario 1 and 2) are shown in Figure 4. The potential environmental impacts of
484 Scenario 2 are fairly constant over the year. On the contrary, a strong seasonal variation
485 was observed in Scenario 1. It was due to the fact that the microalgal biomass
486 production range in Scenario 1 ($5\text{-}25 \text{ g}_{\text{TSS}} \text{ m}^{-2} \text{ d}^{-1}$) is lower than Scenario 2 ($15\text{-}30 \text{ g}_{\text{TSS}}$
487 $\text{m}^{-2} \text{ d}^{-1}$) and represents a high variation due to the seasonal fluctuations. It was in
488 accordance with previous studies, which reported that meteorological conditions played
489 a critical role in the LCA results of HRAPs for microalgal cultivation (Pérez-López et
490 al., 2017). The authors highlighted that HRAPs are more suitable for locations where
491 warm temperatures and high solar radiation are predominant (Pérez-López et al., 2017).
492 Moreover, electricity and flocculants consumption, as well as water and biofertilizer
493 characteristics, are fairly constant over the year in Scenario 2, while the biogas
494 production and, consequently, the energy avoided, strongly depend on microalgal
495 biomass production. These facts have a great influence on the environmental impacts
496 seasonality in Scenario 1. As a result, Scenario 2 remained the most environmentally
497 friendly alternative in 7 out of 11 impact categories compared to Scenario 1 over the
498 year. Similarly, HRAPs scenarios (Scenario 1 and 2) still showed lower potential
499 environmental impacts in 6 out of 11 impact categories compared to activated sludge
500 system (Scenario 3) considering seasonal fluctuations.

501

502 **Please insert Figure 4**

503

504 **3.4 Economic assessment**

505 Results of the economic analysis are shown in Table 8. With respect to capital costs,
506 Scenario 2 appeared as the less expensive alternative. It was due to its lower specific
507 area requirement and, thus, lower amount of purchased materials, compared to Scenario
508 1 (3 vs. 4 m² p.e.⁻¹, respectively). Similar capital costs were found in previous studies
509 which carried out an economic analysis of HRAPs for wastewater treatment without any
510 resource recovery strategies (Garfí et al., 2017, Molinos-Senante et al., 2014). In fact, in
511 this study the capital cost for ponds implementation was around 90% of the total capital
512 cost of the overall systems (i.e. primary settler, ponds, secondary settler, digesters).
513 Since the highest cost is due to ponds construction, implementing downstream units for
514 resource recovery strategies (e.g. digester) in a HRAP system for wastewater treatment
515 would slightly increase its capital costs. Regarding the operation costs, Scenario 2
516 showed to be the most expensive alternative, since this configuration requires higher
517 expenses for energy and flocculant purchase. Nevertheless, if the price of the co-
518 products (i.e. electricity sold back to the grid, microalgae biomass to produce the
519 biofertilizer) that the wastewater treatment plant could sell out are considered, Scenario
520 2 would be the most cost-effective alternative (Table 8). The results of the economic
521 assessment are consistent with previous studies, which indicated that recycling valuable
522 compounds from microalgal biomass (such as nutrients and pigments) is likely to be
523 more economically feasible than producing biogas from it, due to the higher added
524 value of the final products (Ruiz et al., 2016; Vulsteke et al., 2017).

525

526

Please insert Table 8

527

528 **4. Conclusions**

529 In this study, the LCA methodology was a useful tool to identify the main
530 environmental bottlenecks to scale-up high rate algal pond (HRAP) systems for
531 wastewater treatment and resource recovery in small communities.

532 Results showed that HRAP system coupled with biogas production showed to be
533 more environmentally friendly than HRAP system coupled with biofertilizer production
534 in the climate change, ozone layer depletion, photochemical oxidant formation, and
535 fossil depletion impact categories. Different climatic conditions have strongly
536 influenced the results obtained in the eutrophication and metal depletion impact
537 categories. In fact, the HRAP system located where warm temperatures and high solar
538 radiation are predominant (HRAP system coupled with biofertilizer production) showed
539 lower impact in those categories due to its higher nutrients removal efficiencies and
540 lower hydraulic retention time (i.e. lower specific area requirement). The characteristics
541 (e.g. total solids, nutrients and heavy metals concentration) of microalgal biomass
542 recovered from wastewater appeared to be crucial when assessing the potential
543 environmental impacts in the terrestrial acidification, particulate matter formation and
544 toxicity impact categories.

545 Normalization identified Freshwater Eutrophication, Marine Eutrophication,
546 Terrestrial Acidification and Human Toxicity as the most significant impact categories
547 for all the scenarios considered. In these categories, HRAP system coupled with
548 biofertilizer production and implemented in warm climate region showed to be the most
549 environmentally friendly alternative.

550 Additionally, HRAP systems coupled with biogas and biofertilizer production
551 showed lower potential environmental impacts compared to an activated sludge system

552 in the climate change, ozone layer depletion, photochemical oxidant formation, and
553 fossil depletion impact categories.

554 The environmental performance of HRAP technology for wastewater treatment
555 and resource recovery in small communities might be improved by: i) reducing NH_4^+
556 volatilization in HRAPs by controlling the pH through CO_2 injection; ii) ensuring
557 higher nutrients removal efficiencies by selecting a favourable geographical location to
558 implement the HRAP systems; iii) studying improved technologies to separate heavy
559 metals from recycled microalgal biomass; iv) improving HRAP design in order to
560 decrease the amount of construction materials used.

561 In terms of costs, HRAP system coupled with biofertilizer production was the
562 most cost-effective alternative, due to the higher added value of the biofertilizer
563 compared to the energy obtained from biogas cogeneration.

564 In conclusion, HRAPs are sustainable and cost-effective technology for
565 wastewater treatment in small communities, especially if implemented in warm climate
566 regions and coupled with biofertilizer production. Their implementation and
567 dissemination can help to support a shift towards resource recovery and a sustainable
568 circular economy.

569

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577

578

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750

751 **Table 1.** Characteristics and design parameters of the HRAP coupled with biogas production (Scenario
 752 1)

<i>System characteristics</i>	<i>Unit</i>			
Inlet BOD ₅ concentration	$mg_{BOD} L^{-1}$	300		
Outlet BOD ₅ concentration	$mg_{BOD} L^{-1}$	<25		
Inlet TSS concentration	$mg_{TSS} L^{-1}$	150		
Outlet TSS concentration	$mg_{TSS} L^{-1}$	<35		
Inlet Total Nitrogen	$mg_{TN} L^{-1}$	39		
Outlet Total Nitrogen	$mg_{TN} L^{-1}$	9.38		
Inlet Total Phosphorous	$mg_{TP} L^{-1}$	5		
Outlet Total Phosphorous	$mg_{TP} L^{-1}$	3.69		
Flow rate	$m^3 d^{-1}$	1,950		
Population equivalent	<i>p.e.</i>	10,000		
Total surface area	m^2	40,000		
Specific area requirement	$m^2 p.e.^{-1}$	4		
<i>HRAPs Design parameters</i>	<i>Unit</i>	Summer	Winter	Rest of the year
OLR	$g_{BOD} m^{-2} d^{-1}$	10		
HRT	<i>d</i>	4	8	6
Number of ponds	-	2	4	3
Channel width	<i>m</i>	12		
Channel length	<i>m</i>	812.5		
Water depth	<i>m</i>	0.4		
Microalgae biomass production	$g_{TSS} m^{-2} d^{-1}$	25.8	3.3	10.5
Annual average microalgae biomass production	$g_{TSS} m^{-2} d^{-1}$	12		

753 *Note: BOD: Biochemical oxygen demand; TSS: Total suspended solids; HRT: Hydraulic Retention Time;*

754 *OLR: Organic Loading Rate. Summer: from May to July; winter: from November to April.*

755

756

757

758 **Table 2.** Characteristics and design parameters of the HRAP coupled with biofertilizer production
 759 (Scenario 2)

<i>System characteristics</i>	<i>Unit</i>			
Inlet BOD ₅ concentration	$mg_{BOD} L^{-1}$	300		
Outlet BOD ₅ concentration	$mg_{BOD} L^{-1}$	<25		
Inlet TSS concentration	$mg_{TSS} L^{-1}$	200		
Outlet TSS concentration	$mg_{TSS} L^{-1}$	<35		
Inlet Total Nitrogen	$mg_{TN} L^{-1}$	50		
Outlet Total Nitrogen	$mg_{TN} L^{-1}$	2		
Inlet Total Phosphorous	$mg_{TP} L^{-1}$	10		
Outlet Total Phosphorous	$mg_{TP} L^{-1}$	1		
Flow rate	$m^3 d^{-1}$	1,950		
Population equivalent	<i>p.e.</i>	10,000		
Total surface area	m^2	30,000		
Specific area requirement	$m^2 p.e.^{-1}$	3		
<i>HRAPs Design parameters</i>	<i>Unit</i>	Summer	Winter	Rest of the year
OLR	$g_{BOD} m^{-2} d^{-1}$	20		
HRT	<i>d</i>	3		
Number of ponds	-	2		
Channel width	<i>m</i>	12		
Channel length	<i>m</i>	1,219		
Water depth	<i>m</i>	0.2		
Microalgae biomass production	$g_{TSS} m^{-2} d^{-1}$	30	15	25
Annual average microalgae biomass production	$g_{TSS} m^{-2} d^{-1}$	23		

760 *Note: BOD: Biochemical oxygen demand; TSS: Total suspended solids; HRT: Hydraulic Retention Time;*

761 *OLR: Organic Loading Rate. Summer: from May to August; winter: from November to March*

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765 **Table 3.** Characteristics and design parameters of the activated sludge system (Scenario 3)

<i>System characteristics</i>	<i>Unit</i>	
Inlet BOD ₅ concentration	$mg_{BOD} L^{-1}$	300
Outlet BOD ₅ concentration	$mg_{BOD} L^{-1}$	<25
Outlet TSS concentration	$mg_{TSS} L^{-1}$	<35
Flow rate	$m^3 d^{-1}$	1,950
Population equivalent	<i>p.e.</i>	10,000
Total surface area	m^2	900
Specific area requirement	$m^2 p.e.^{-1}$	0.6
<i>Design parameters</i>	<i>Unit</i>	
Primary settler HRT	<i>h</i>	2.5
Activated sludge reactor HRT	<i>h</i>	6
Secondary settler HRT	<i>h</i>	2

766 *Note: BOD: Biochemical oxygen demand; TSS: Total suspended solids; HRT: Hydraulic Retention Time;*767 *OLR: Organic Loading Rate.*

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771 **Table 4.** Summary of the inventory for Scenario 1: HRAP system for wastewater treatment where
 772 microalgal biomass is valorised for energy recovery (biogas production). Values are referred to the
 773 functional unit (1 m³ of water)

Inputs	Scenario 1	Units
<i>Construction materials</i>		
<i>Primary settler</i>		
Concrete	2.55E-06	m ³ m ⁻³
Steel	2.04E-04	kg m ⁻³
<i>HRAPs</i>		
Concrete	5.94E-04	m ³ m ⁻³
Steel	4.76E-02	kg m ⁻³
<i>Secondary settler</i>		
Concrete	1.29E-05	m ³ m ⁻³
Steel	1.03E-03	kg m ⁻³
<i>Thickener</i>		
Concrete	1.78E-07	m ³ m ⁻³
Steel	1.42E-05	kg m ⁻³
<i>Thermal pretreatment</i>		
Concrete	2.77E-07	m ³ m ⁻³
Steel	2.22E-05	kg m ⁻³
<i>Digester</i>		
Concrete	9.79E-06	m ³ m ⁻³
Steel	7.83E-04	kg m ⁻³
<i>Operation</i>		
<i>Energy consumption*</i>		
Primary settler	4.41E-03	kWh m ⁻³
HRAPs	1.13E-02	kWh m ⁻³
Secondary settler	2.52E-03	kWh m ⁻³
Thermal pretreatment	1.08E-04	kWh m ⁻³
Digester	4.17E-02	kWh m ⁻³
Total energy consumption	6.00E-02	kWh m ⁻³
Outputs		
<i>Emissions to water*</i>		
Total COD	7.63E+01	g m ⁻³
TSS	2.40E+01	g m ⁻³
TN	9.38E+00	g m ⁻³
TP	3.69E+00	g m ⁻³
<i>Emissions to air*</i>		
<i>NH₄⁺ volatilization in HRAPs</i>		
NH ₃	3.80E+00	g m ⁻³
<i>Digestate application as fertilizer</i>		
NH ₃	6.47E+00	g m ⁻³

N ₂ O	2.59E-01	<i>g m⁻³</i>
<i>Emissions to soil*</i>		
<i>Digestate application as fertilizer</i>		
Cd	3.53E-03	<i>g m⁻³</i>
Cu	2.02E-01	<i>g m⁻³</i>
Pb	9.08E-02	<i>g m⁻³</i>
Zn	9.04E-01	<i>g m⁻³</i>
Ni	4.15E-02	<i>g m⁻³</i>
Cr	5.22E-02	<i>g m⁻³</i>
Hg (value <)	4.52E-04	<i>g m⁻³</i>
<i>Avoided products*</i>		
Electricity (from biogas cogeneration)	5.40E-01	<i>kWh m⁻³</i>
Heat (from biogas cogeneration)	8.49E-01	<i>kWh m⁻³</i>
N as Fertiliser (from digestate reuse)	2.59E+01	<i>g m⁻³</i>
P as Fertiliser (from digestate reuse)	1.31E+00	<i>g m⁻³</i>

774 * Annual averages

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778 **Table 5.** Summary of the inventory for Scenario 2: HRAP system for wastewater treatment where
 779 microalgal biomass is reused for nutrients recovery (biofertilizer production). Values are referred to the
 780 functional unit (1 m³ of water)

Inputs	Scenario 2	Units
Construction materials		
<i>HRAPs</i>		
Concrete	4.32E-04	m ³ m ⁻³
Steel	3.45E-02	kg m ⁻³
<i>Secondary settler</i>		
Concrete	1.29E-05	m ³ m ⁻³
Steel	1.03E-03	kg m ⁻³
<i>Centrifuge</i>		
Steel	3.86E-05	kg m ⁻³
Operation		
<i>Energy consumption*</i>		
HRAPs	1.11E-02	kWh m ⁻³
Secondary settler	5.77E-03	kWh m ⁻³
Centrifuge	1.15E-02	kWh m ⁻³
Biofertilizer production	4.70E-02	kWh m ⁻³
Total energy consumption	7.54E-02	kWh m ⁻³
<i>Chemicals*</i>		
Organic flocculant	1.00E+01	kg m ⁻³
Outputs		
<i>Emissions to water*</i>		
Total COD	1.00E+02	g m ⁻³
TSS	5.00E+01	g m ⁻³
TN	2.00E+00	g m ⁻³
TP	1.00E+00	g m ⁻³
<i>Emissions to air*</i>		
<i>NH₄⁺ volatilization in HRAPs</i>		
NH ₃	5.00E+00	g m ⁻³
<i>Biofertilizer</i>		
NH ₃	1.44E+00	g m ⁻³
N ₂ O	5.77E-02	g m ⁻³
<i>Emissions to soil*</i>		
<i>Biofertilizer</i>		
Cd	3.46E-04	g m ⁻³
Cu	4.62E-02	g m ⁻³
Pb	2.31E-02	g m ⁻³
Zn	1.15E-02	g m ⁻³
Ni	1.15E-02	g m ⁻³

Cr	3.46E-02	$g\ m^{-3}$
Hg (value <)	2.31E-04	$g\ m^{-3}$
Avoided products*		
N as Fertiliser (from biofertilizer)	5.77E+00	$g\ m^{-3}$
P as Fertiliser (from biofertilizer)	1.20E+00	$g\ m^{-3}$

781 * Annual averages

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Table 6. Summary of the inventory for Scenario 3: typical small-sized activated sludge system

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implemented in Spain. Values are referred to the functional unit (1 m³ of water)

Inputs	Scenario 3	Units
<i>Construction materials</i>		
Concrete	1.65E-05	m ³ m ⁻³
Steel	1.32E-03	kg m ⁻³
<i>Operation</i>		
<i>Energy consumption</i>		
Electricity	8.90E-01	kWh m ⁻³
<i>Chemicals</i>		
Polyelectrolyte	1.98E+00	g m ⁻³
Coagulant	3.18E+00	g m ⁻³
Outputs		
<i>Emissions to water</i>		
Total COD	1.25E+02	g m ⁻³
TSS	3.50E+01	g m ⁻³
TN	1.50E+01	g m ⁻³
TP	2.00E+00	g m ⁻³
<i>Emissions to air</i>		
CO ₂	1.70E-01	g m ⁻³
N ₂ O	1.10E-01	g m ⁻³
<i>Waste to further treatment</i>		
Sludge (incineration)	1.24E+00	kg m ⁻³

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789 **Table 7.** Results of the sensitivity analysis for the considered parameters: NH₃ emissions due to the application of digestate and biofertilizer on agricultural land; N₂O
790 emissions due to the application of digestate and biofertilizer on agricultural land; digestate and biofertilizer transportation distance.

<i>Impact categories</i>	<i>Parameters</i>					
	<i>Scenario 1</i>			<i>Scenario 2</i>		
	<i>NH₃ emissions</i>	<i>N₂O emissions</i>	<i>Digestate transportation</i>	<i>NH₃ emissions</i>	<i>N₂O emissions</i>	<i>Biofertilizer transportation</i>
Climate change	±0.000	± 0.367	±0.260	±0.000	±0.068	±0.015
Ozone Depletion	±0.000	±0.000	±0.204	±0.000	±0.000	±0.053
Terrestrial acidification	± 0.337	±0.000	±0.008	±0.213	±0.000	±0.001
Freshwater eutrophication	±0.000	±0.000	±0.001	±0.000	±0.000	±0.000
Marine eutrophication	±0.058	±0.000	±0.001	±0.052	±0.000	±0.000
Photochemical oxidant formation	±0.000	±0.000	± 2.713	±0.000	±0.000	±0.025
Particulate matter formation	± 0.327	±0.000	±0.033	±0.179	±0.000	±0.003
Metal depletion	±0.000	±0.000	±0.019	±0.000	±0.000	±0.002
Fossil depletion	±0.000	±0.000	±0.153	±0.000	±0.000	±0.027
Human toxicity	±0.000	±0.000	±0.021	±0.000	±0.000	±0.011
Terrestrial ecotoxicity	±0.000	±0.000	±0.019	±0.000	±0.000	±0.011

791 *Note: Scenario 1: HRAP system for wastewater treatment where microalgal biomass is valorized for energy recovery (biogas production); Scenario 2: HRAP system*
792 *for wastewater treatment where microalgal biomass is reused for nutrients recovery (biofertilizer production)*

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Table 8. Results of the economic analysis for the HRAPs scenarios.

	Unit	Scenario 1	Scenario 2
Capital cost	€ p.e. ⁻¹	192.55	139.34
Operation and maintenance cost (energy and flocculant consumption)	€ m ⁻³ _{water}	0.007	0.02
Price of electricity sold back to the grid	€ m ⁻³ _{water}	0.014	-
Price of microalgal biomass sold to a company to produce the biofertilizer	€ m ⁻³ _{water}	-	8.08
Profit (calculated considering operation cost only)	€ m ⁻³ _{water}	0.007	8.06

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Note: Scenario 1: HRAP system for wastewater treatment where microalgal biomass is valorised for energy recovery (biogas production); Scenario 2: HRAP system for wastewater treatment where microalgal biomass is reused for nutrients recovery (biofertilizer production)

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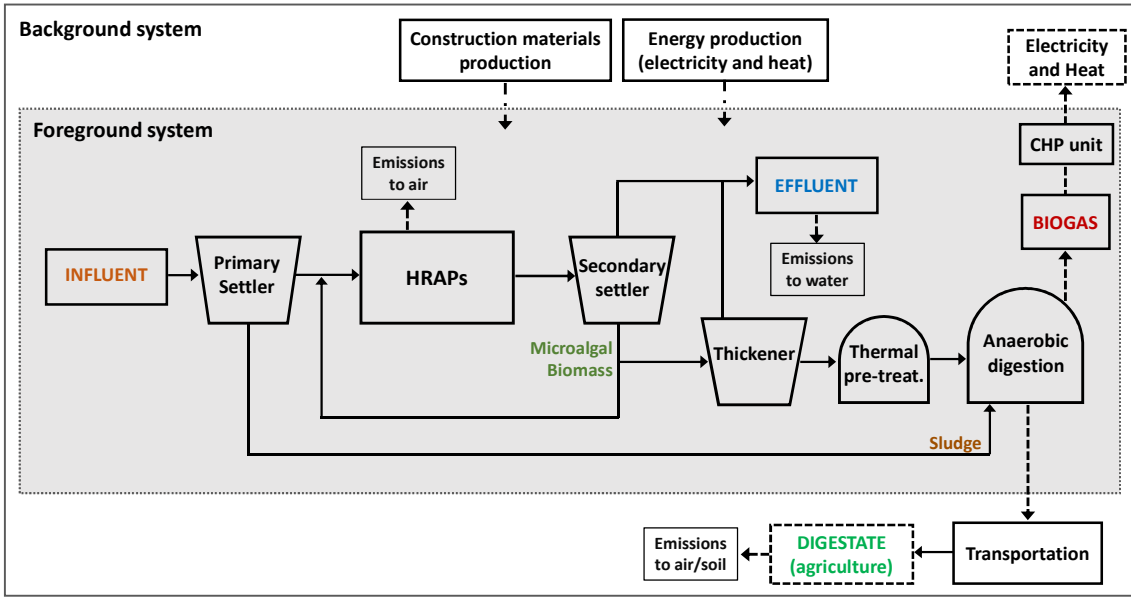
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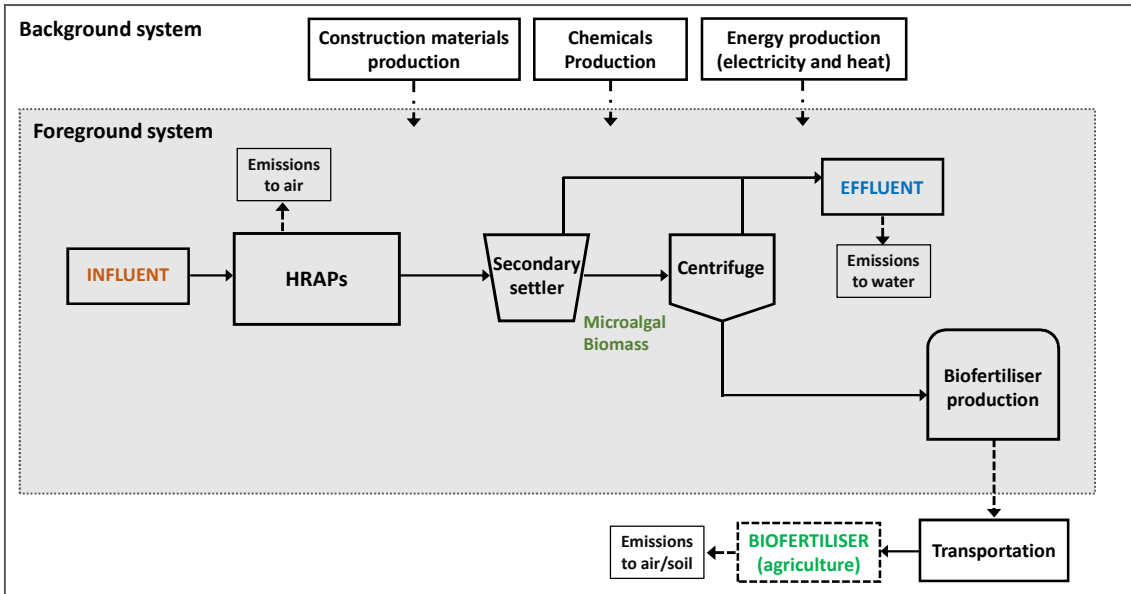


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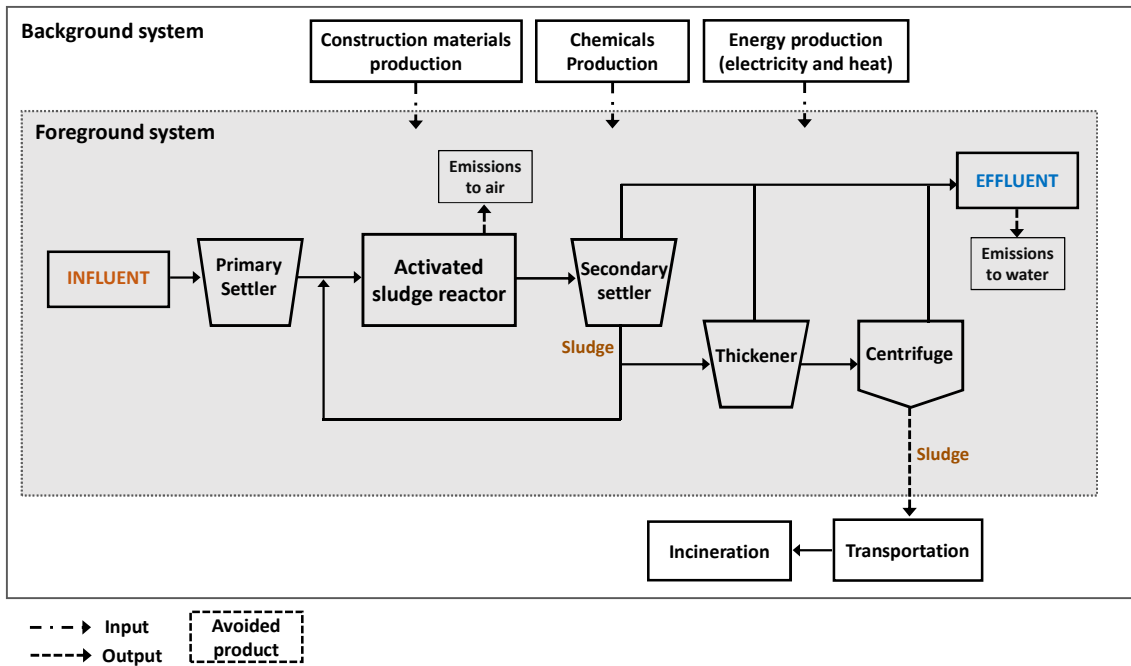


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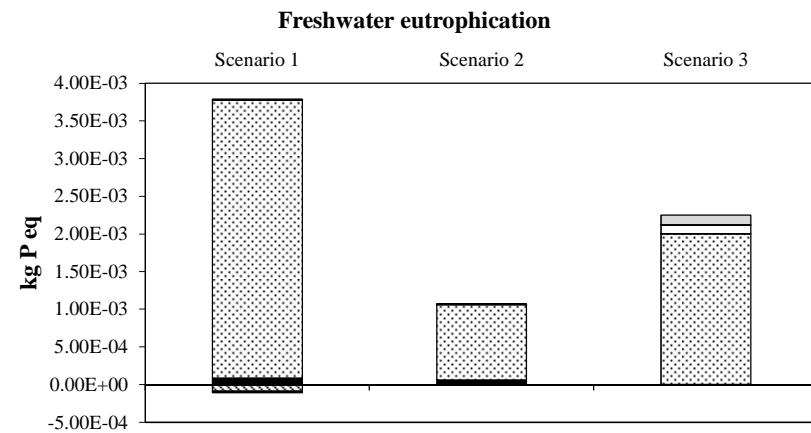
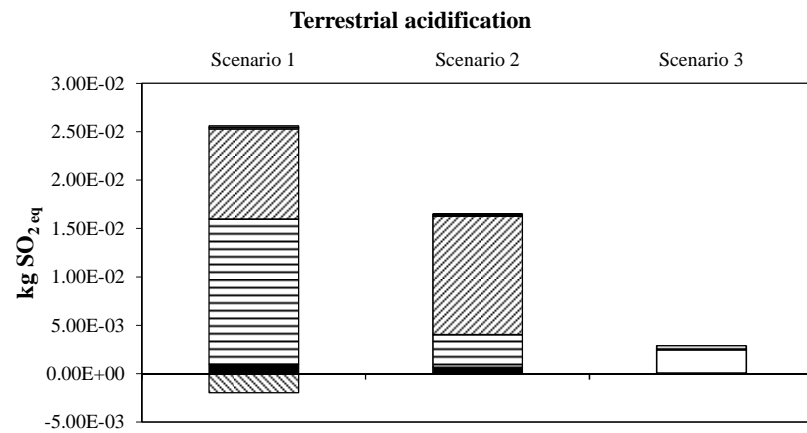
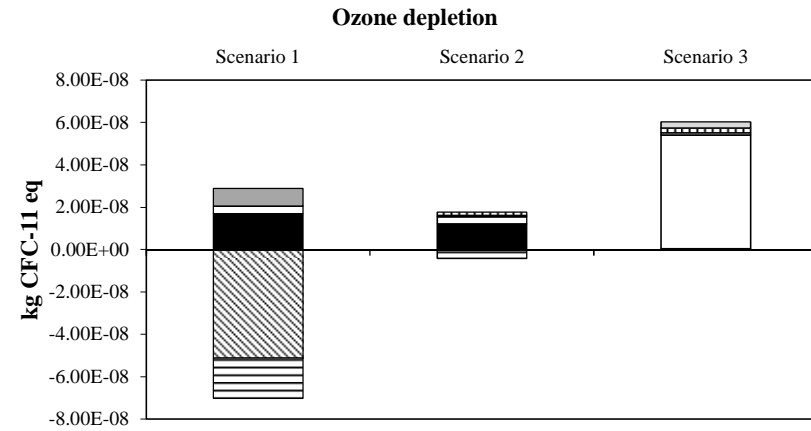
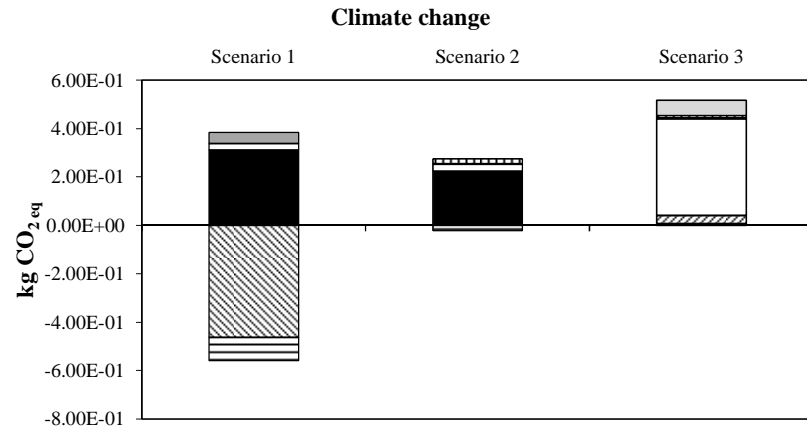
805 **Figure 1.** Flow diagrams and system boundaries of the wastewater treatment
 806 alternatives: a) HRAP system for wastewater treatment where microalgal biomass is
 807 valorised for energy recovery (biogas production) (Scenario 1); b) HRAP system for
 808 wastewater treatment where microalgal biomass is reused for nutrients recovery
 809 (biofertilizer production) (Scenario 2); c) activated sludge system (Scenario 3)

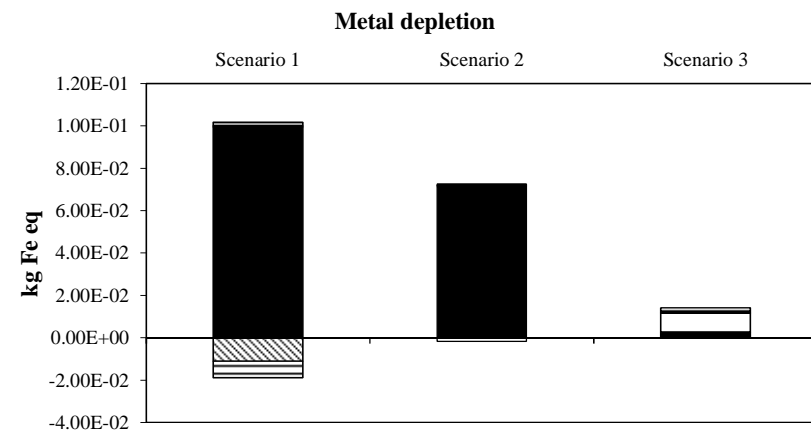
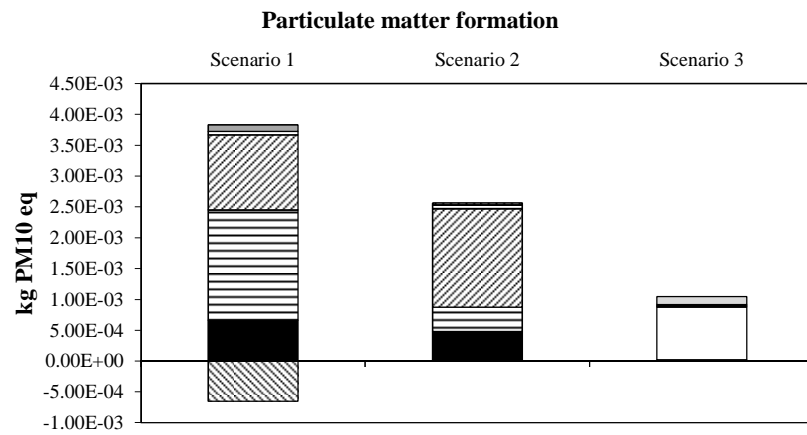
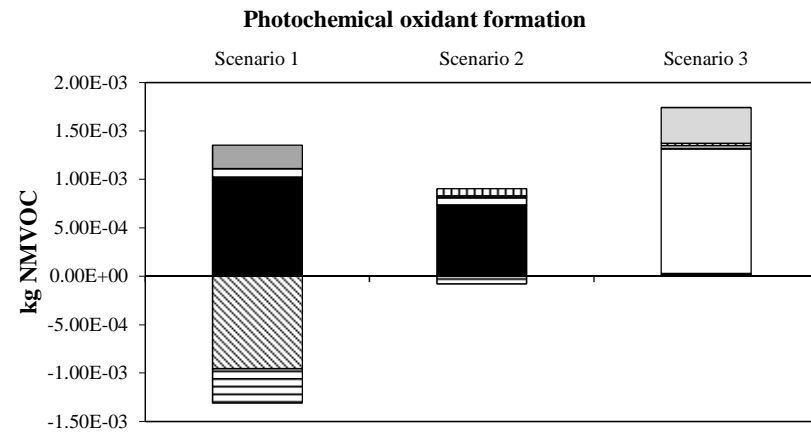
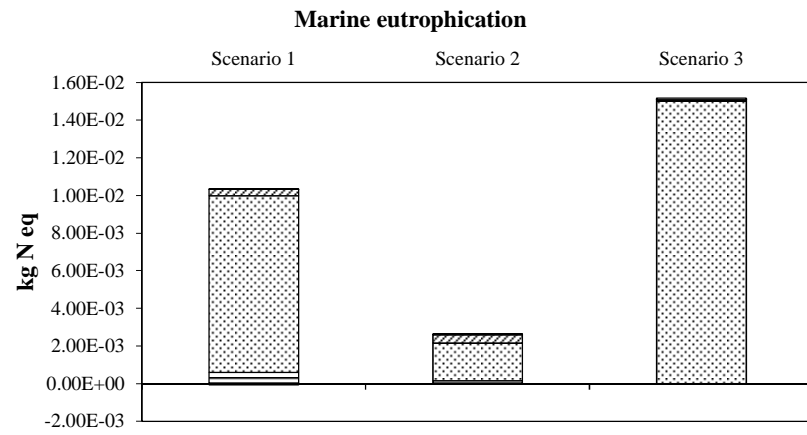
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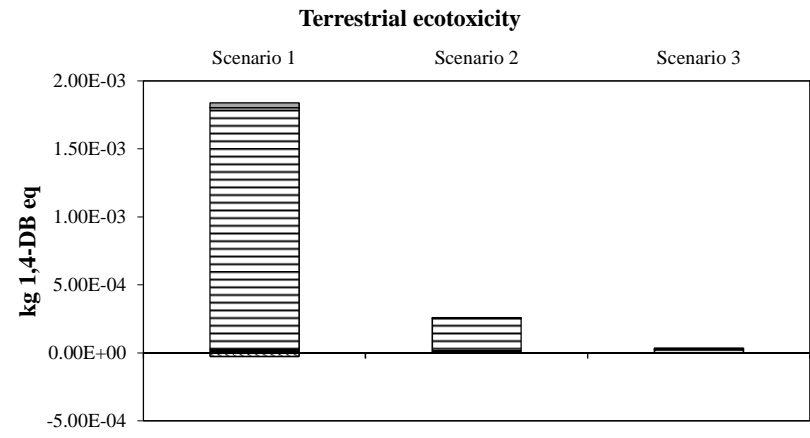
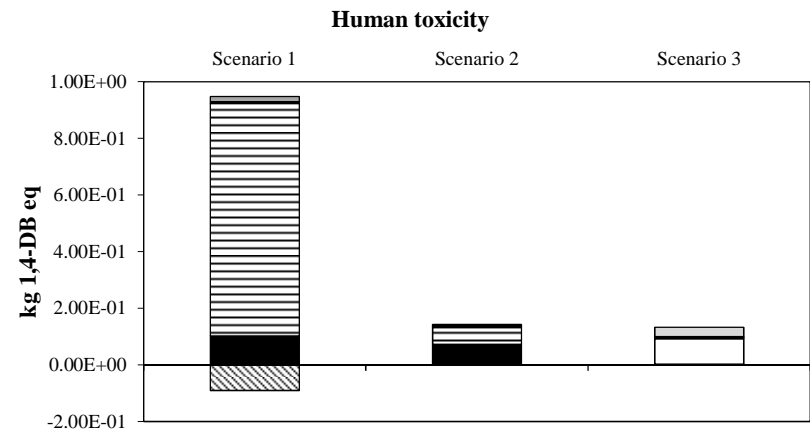
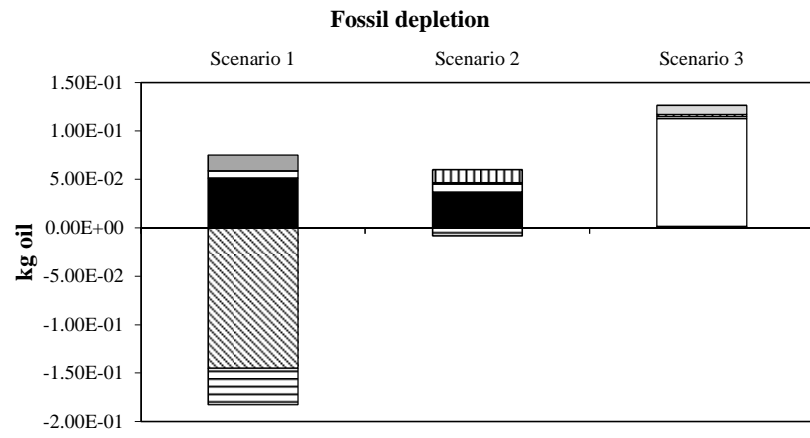
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- Construction materials
- ▣ Digestate and biofertilizer application (including avoided fertilizer)
- ▣ Emissions to air (NH₄⁺ volatilization in HRAP)
- ▣ Digestate, biofertilizer or sludge transportation
- Sludge disposal

- ▣ Biogas cogeneration and avoided energy
- ▣ Emissions to water
- Energy consumption
- ▣ Chemicals

814

815 **Figure 2.** Potential environmental impacts for the three scenarios: a) HRAP system for wastewater treatment where microalgal biomass is
816 valorised for energy recovery (biogas production) (Scenario 1); b) HRAP system for wastewater treatment where microalgal biomass is
817 reused for nutrients recovery (biofertilizer production) (Scenario 2); c) activated sludge system (Scenario 3). Values are referred to the
818 functional unit (1 m³ of water).

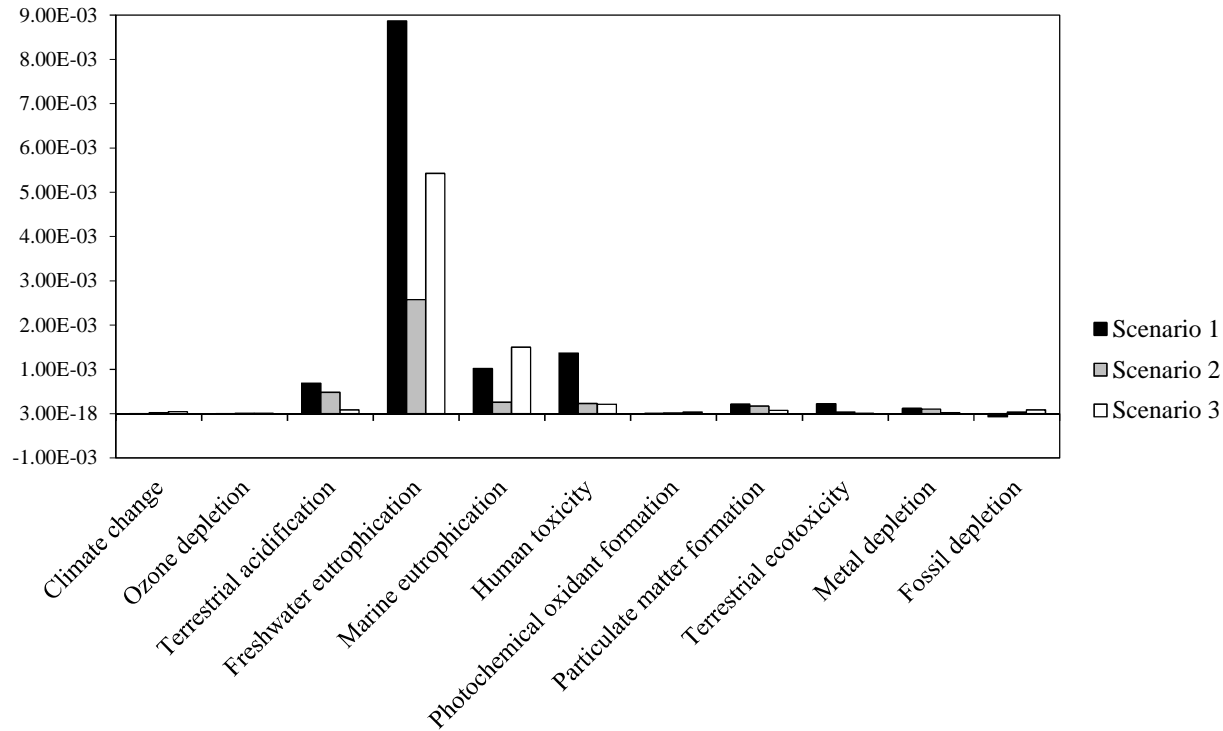
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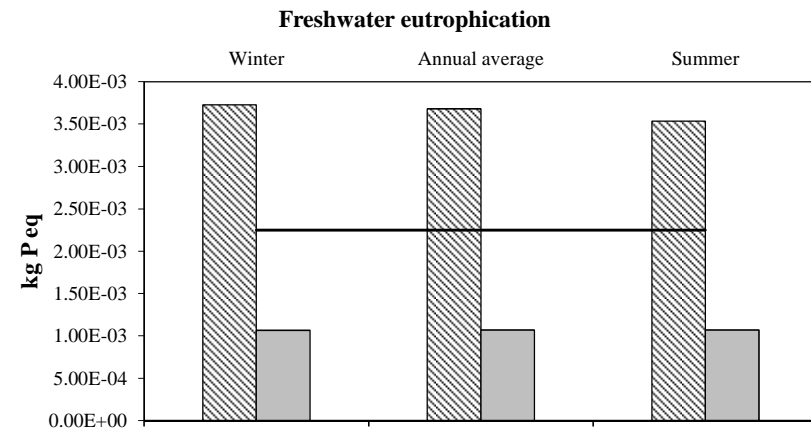
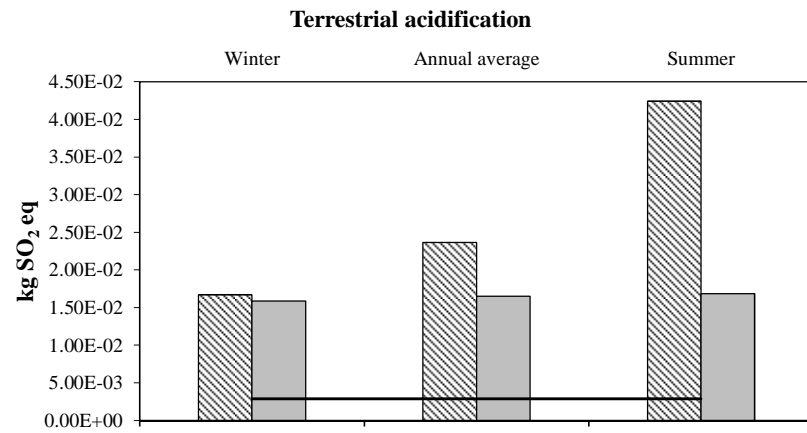
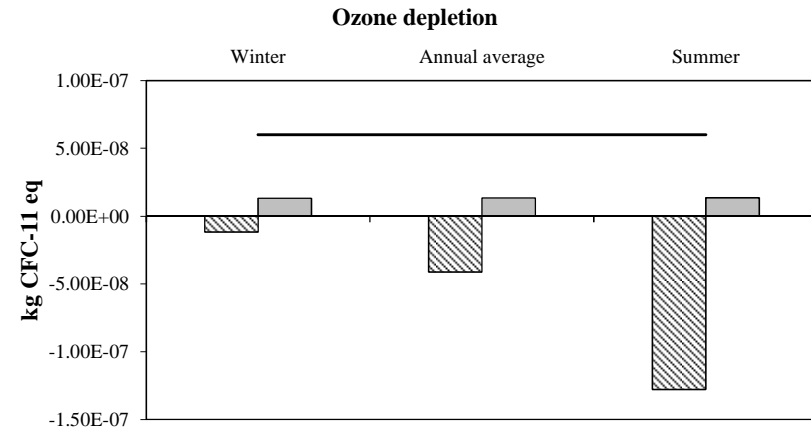
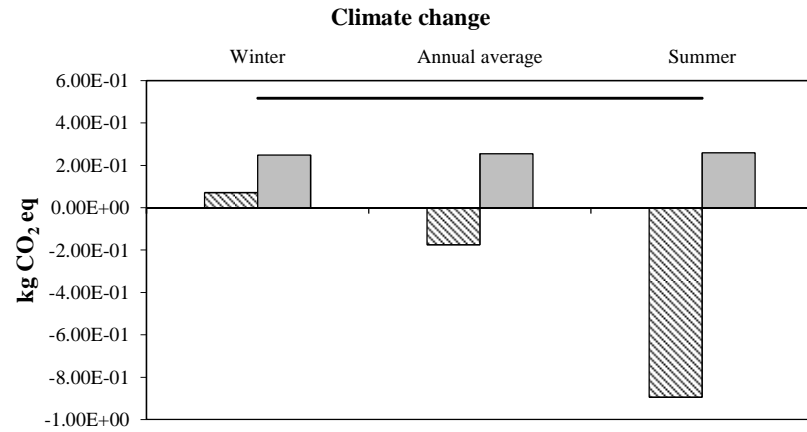
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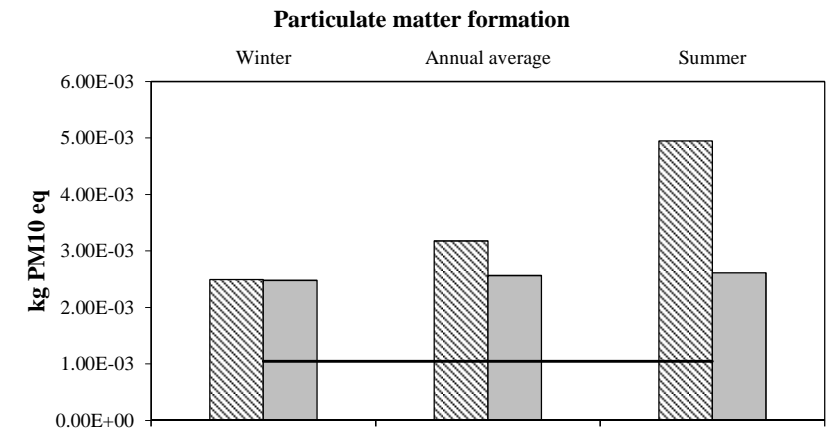
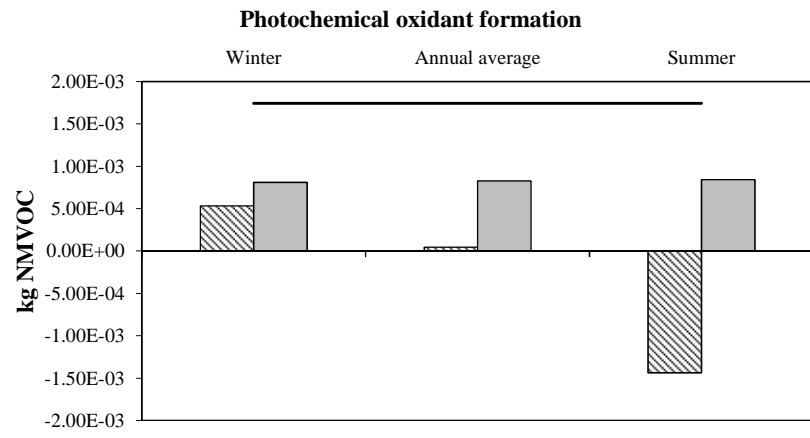
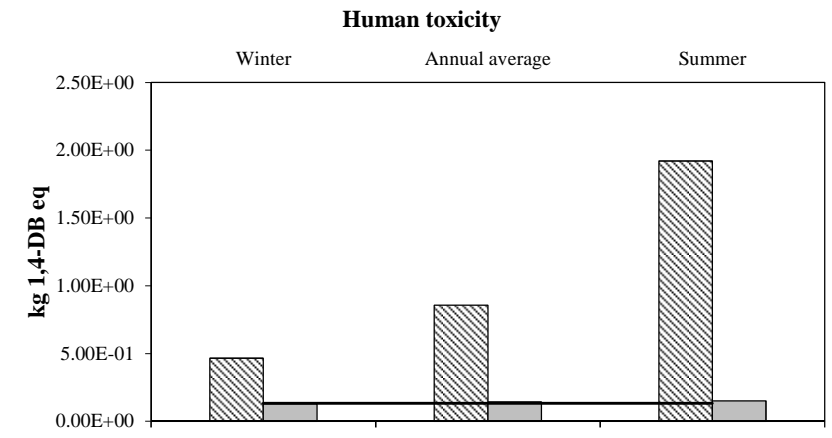
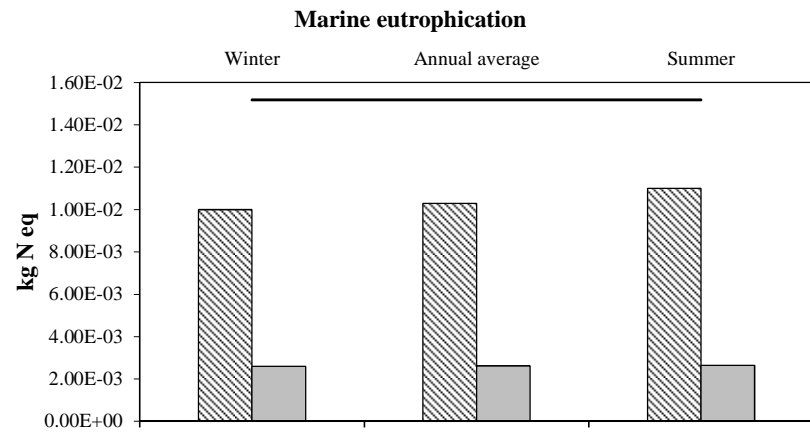


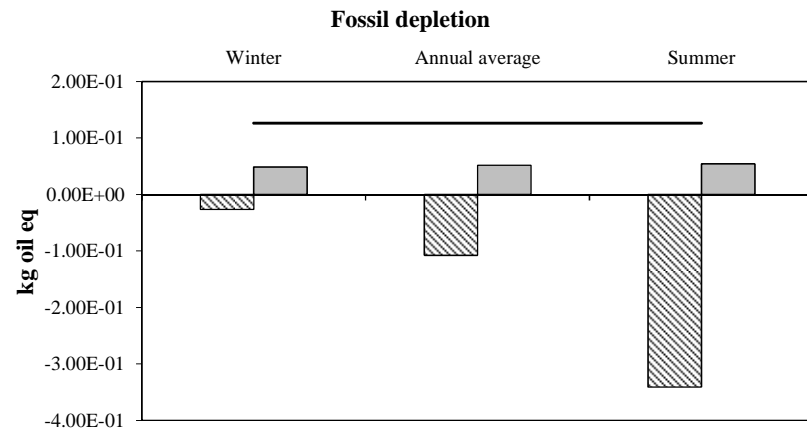
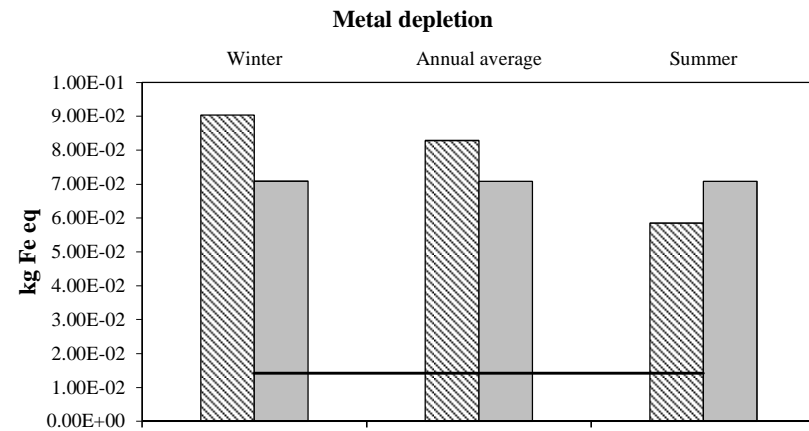
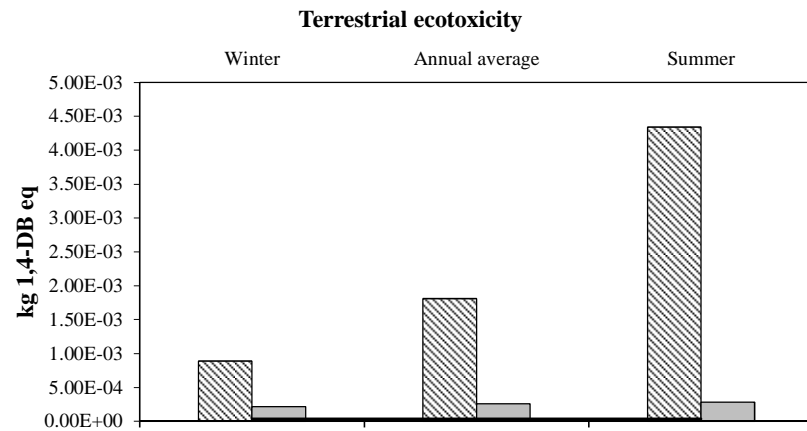
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Figure 3. Normalised potential environmental impacts for the three scenarios: a) HRAP system for wastewater treatment where microalgal biomass is valorised for energy recovery (biogas production) (Scenario 1); b) HRAP system for wastewater treatment where microalgal biomass is reused for nutrients recovery (biofertiliser production) (Scenario 2); c) activated sludge system (Scenario 3).

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830







Scenario 1
 Scenario 2
 Scenario 3

832 **Figure 4.** Seasonal variation of the potential environmental impacts for the three scenarios: a) HRAP system for wastewater treatment
833 where microalgal biomass is valorised for energy recovery (biogas production) (Scenario 1); b) HRAP system for wastewater treatment
834 where microalgal biomass is reused for nutrients recovery (biofertilizer production) (Scenario 2); c) activated sludge system (Scenario 3).
835 Values are referred to the functional unit (1 m³ of water). Potential environmental impacts were calculated considering the microalgal
836 biomass production achieved in summer and winter months (highest and lowest production, respectively).