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# **Effect of the clay-water interaction in the hydration process of compacted bentonite**

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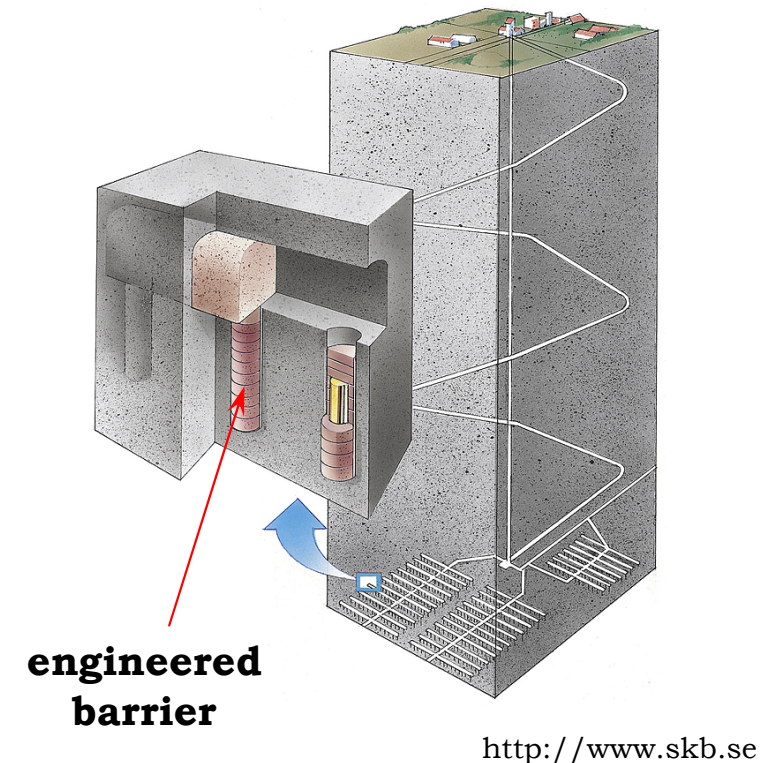
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# INTRODUCTION

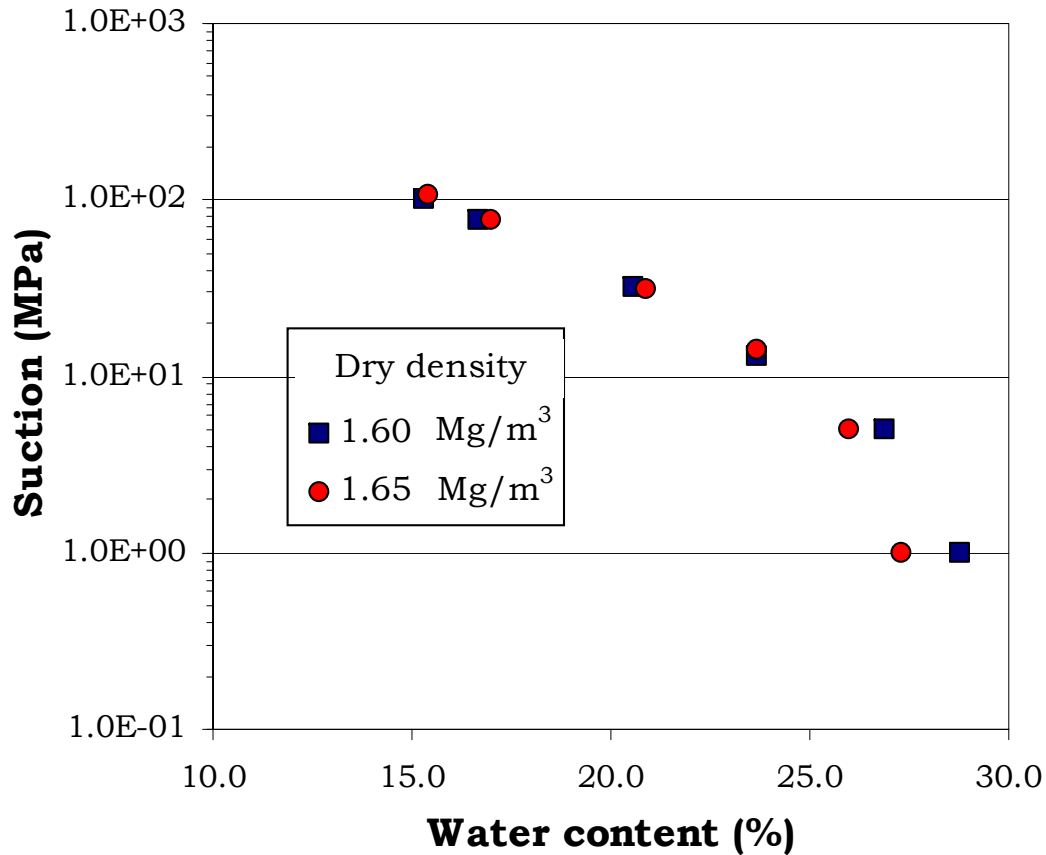
## Motivation

- **Compacted bentonite** is used as engineered barrier in the design of high level radioactive waste repositories.
- In general, **hydration tests** on compacted bentonite samples need **more time** and **water** for saturation than predicted by simulations.
- This effect can be partially attributed to the **interaction** between the **clay minerals** and the **water**.



# INTRODUCTION

## Retention curve of compacted bentonite (constant volume)

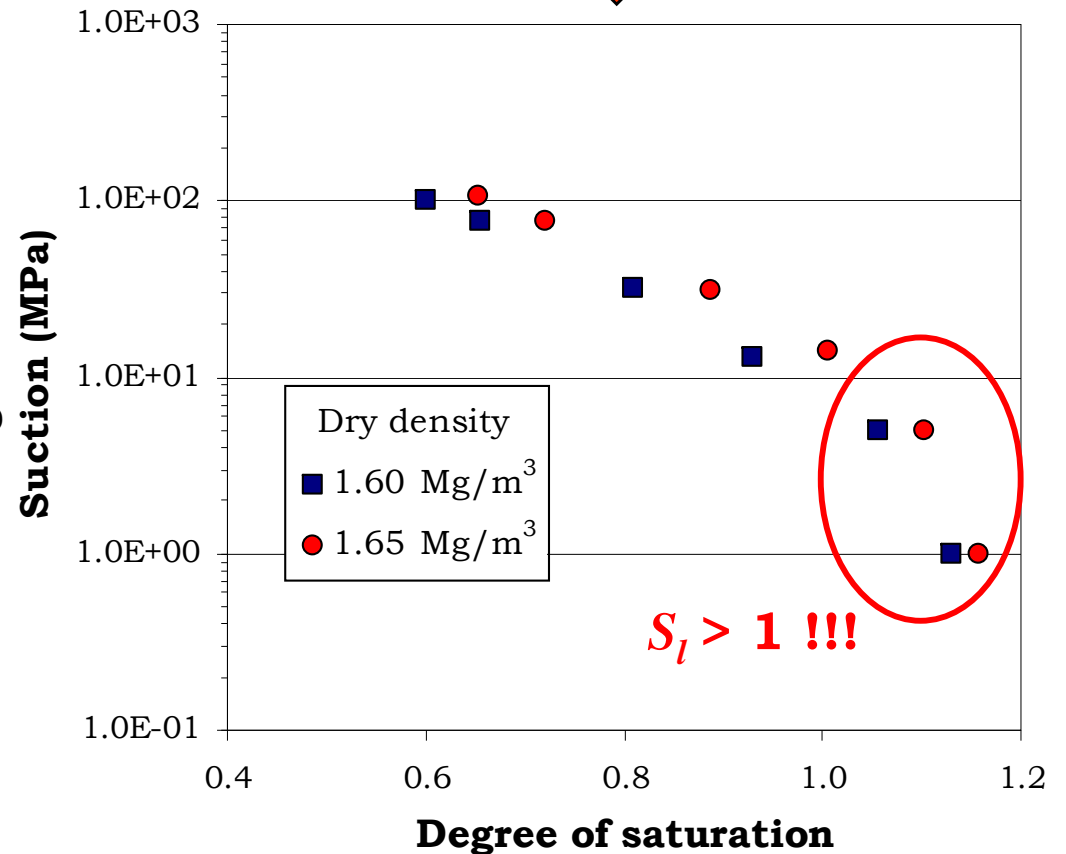


**FEBEX bentonite**

Lloret et al. (2004)

$$S_l = \frac{\rho_s \cdot w}{\rho_w \cdot e}$$

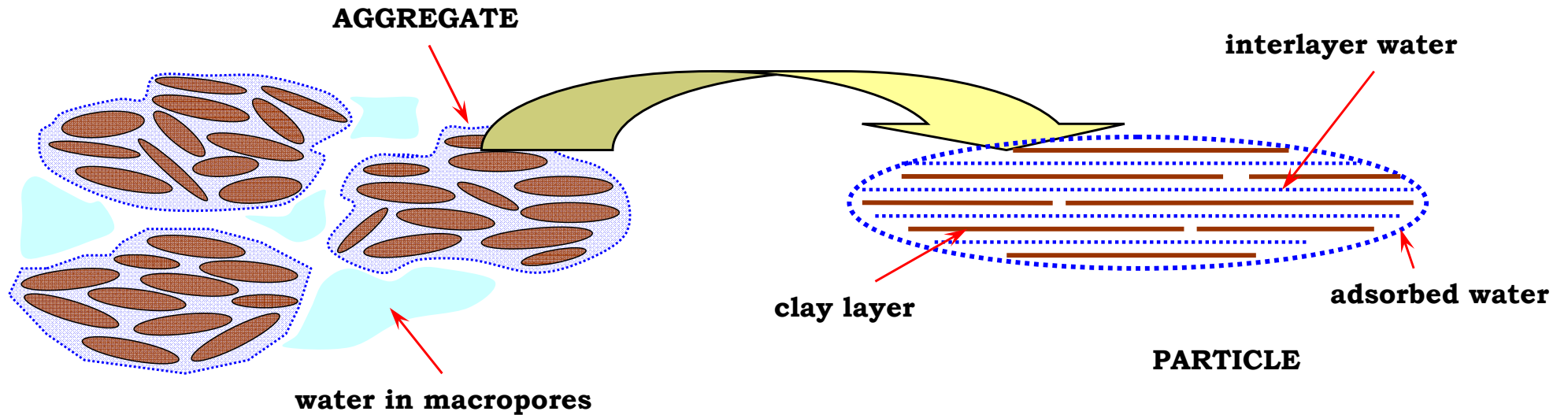
$\rho_w = 1.0 \text{ Mg/m}^3$



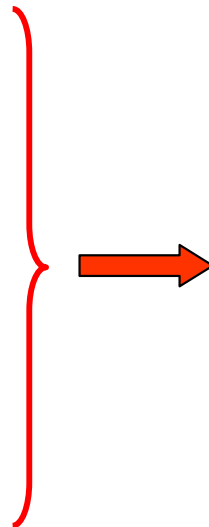
$S_l > 1 \text{ !!!}$

# INTRODUCTION

## Water in compacted bentonite



Low (1979)  
Hawkins & Egelstaff (1980)  
Cariati et al. (1981)  
Derjaguin et al. (1986)  
Push et al. (1990)  
Skipper et al. (1991)



**clay-water interaction**

↓

**water properties are different from those of bulk water**

# WATER DENSITY IN COMPACTED SAMPLES

## Weighted water density

$$w = w_i + w_e + w_f$$

$w$  : total water content

$w_i$  : interlayer water

$w_e$  : adsorbed water on external surfaces

$w_f$  : free water

MX-80 bentonite,  $\rho_d = 1.80 \text{ Mg/m}^3$



$$w_f = 0.011 w$$

Bradbury & Baeyens (2003)

FEBEX bentonite,  $\rho_d = 1.65 \text{ Mg/m}^3$



$$w_f = 0.015 w$$

Fernández et al. (2004)



**It is assumed  $w_f = 0$**

## Weighted water density

$$\rho_w^* = \frac{m_w^i + m_w^e}{V_w^i + V_w^e} = \frac{w}{\frac{w_i}{\rho_w^i} + \frac{w_e}{\rho_w^e}}$$

$m_w^i$  : mass of interlayer water

$m_w^e$  : mass of external water

$V_w^i$  : volume of interlayer water

$V_w^e$  : volume of external water

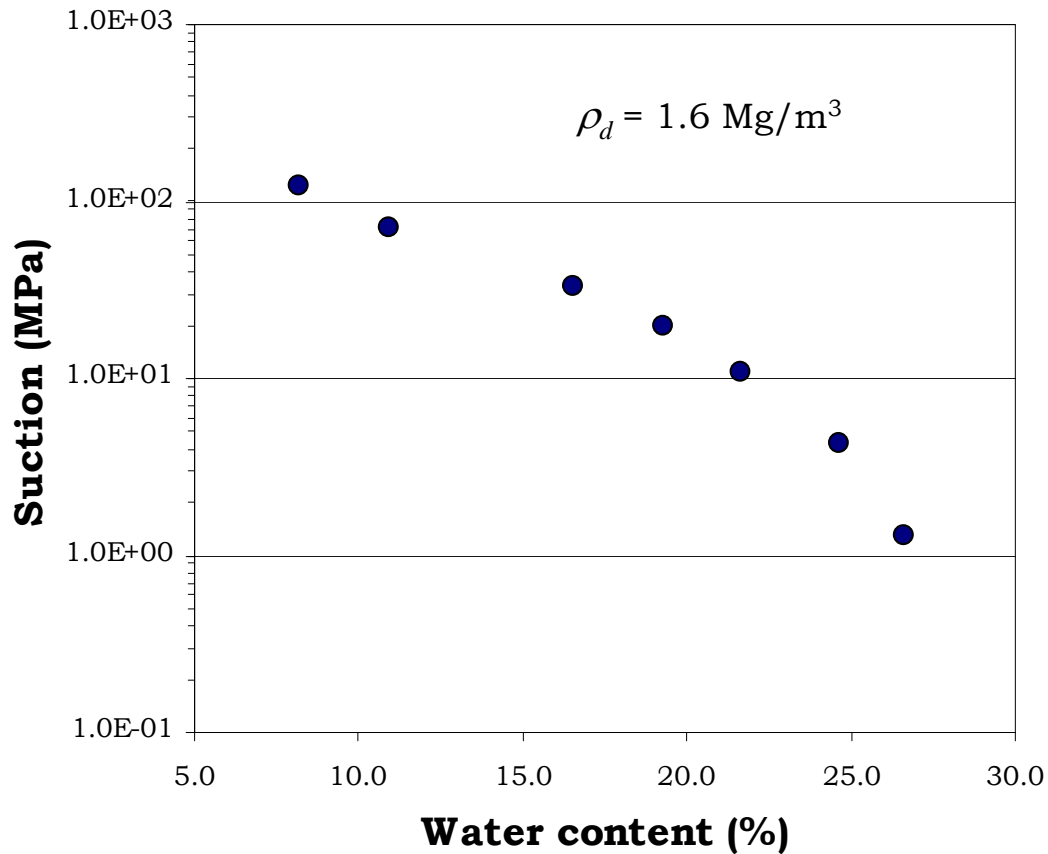
$\rho_w^e = 1.0 \text{ Mg/m}^3$

**unknown:**  $\rho_w^i, w_e, w_i$

Jacinto et al. (2012) - Géotechnique

# WATER DENSITY IN COMPACTED SAMPLES

## Weighted water density

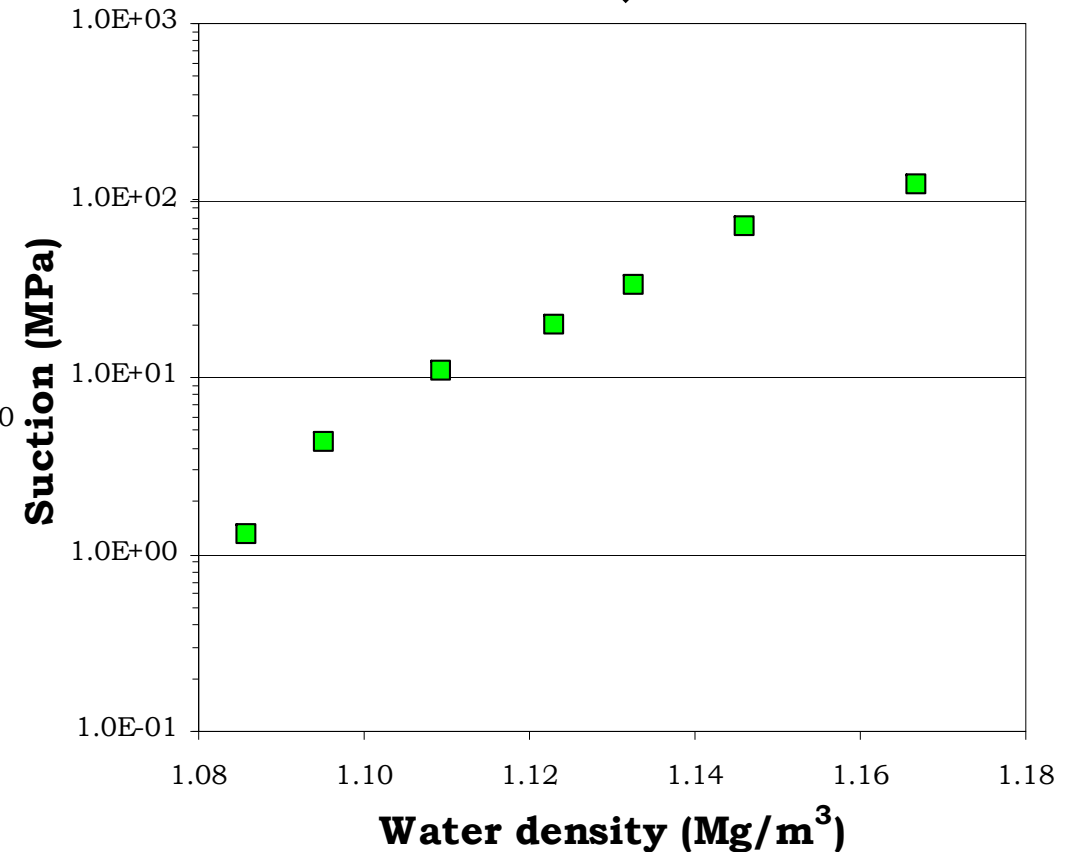


**MX-80 bentonite**

**Villar (2005)**



$$\rho_w^* = \frac{w}{\frac{w_i}{\rho_w^i} + \frac{w_e}{\rho_w^e}}$$



# HYDRATION OF A COMPACTED SAMPLE

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## Application. Experimental set-up

**MX-80 bentonite**

$$\phi = 0.05 \text{ m}$$

$$h = 0.10 \text{ m}$$

$$w_i = 11 \%$$

$$\rho_d = 1.60 \text{ Mg/m}^3$$



**Villar et al. (2006)**



**Final state**

# HYDRATION OF A COMPACTED SAMPLE

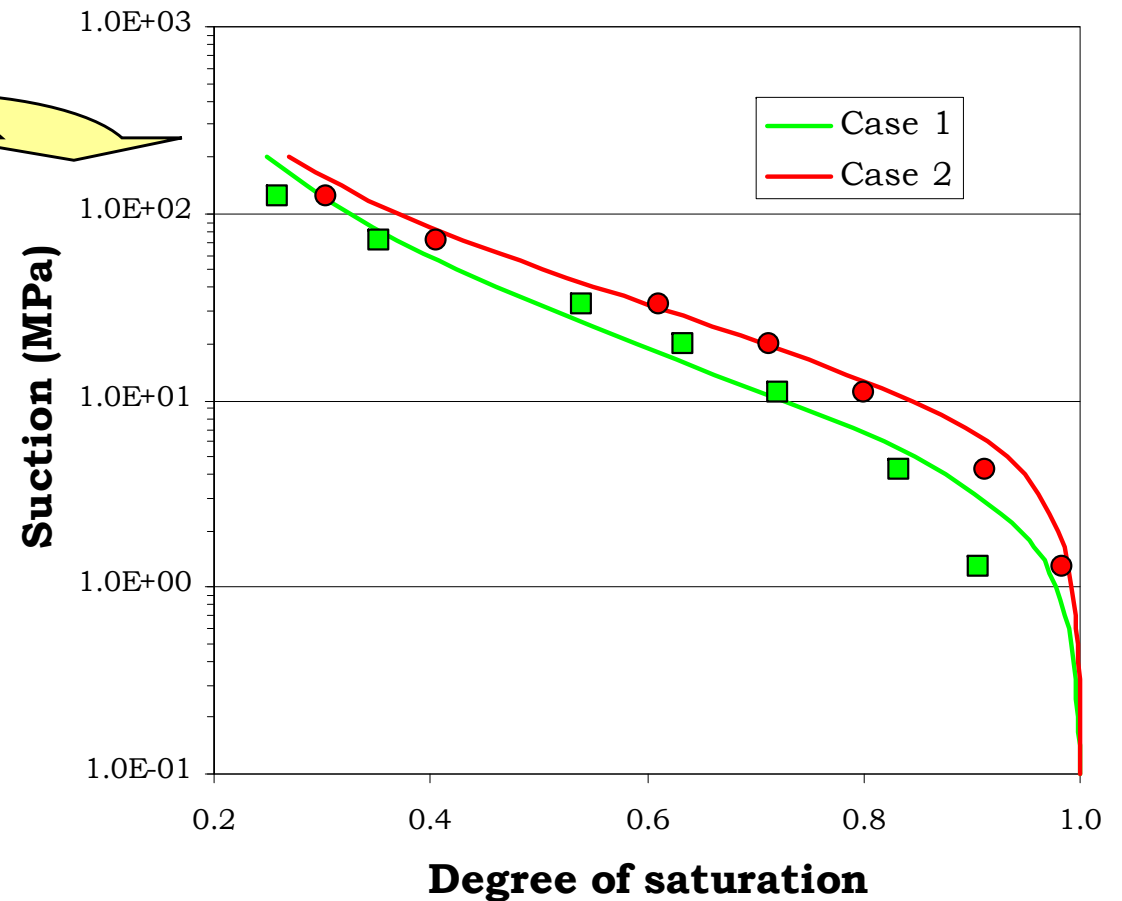
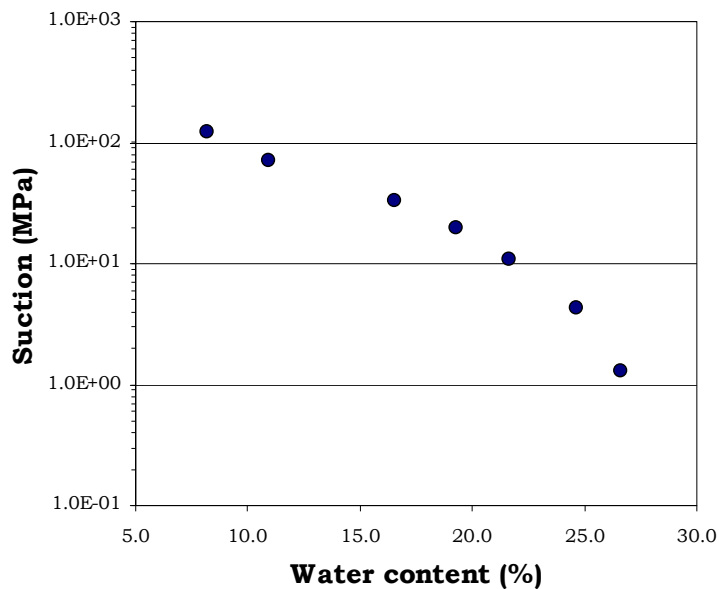
## Application. Numerical analysis

➤ 1D geometry

➤ BE<sub>x</sub>M

➤ Code\_Bright

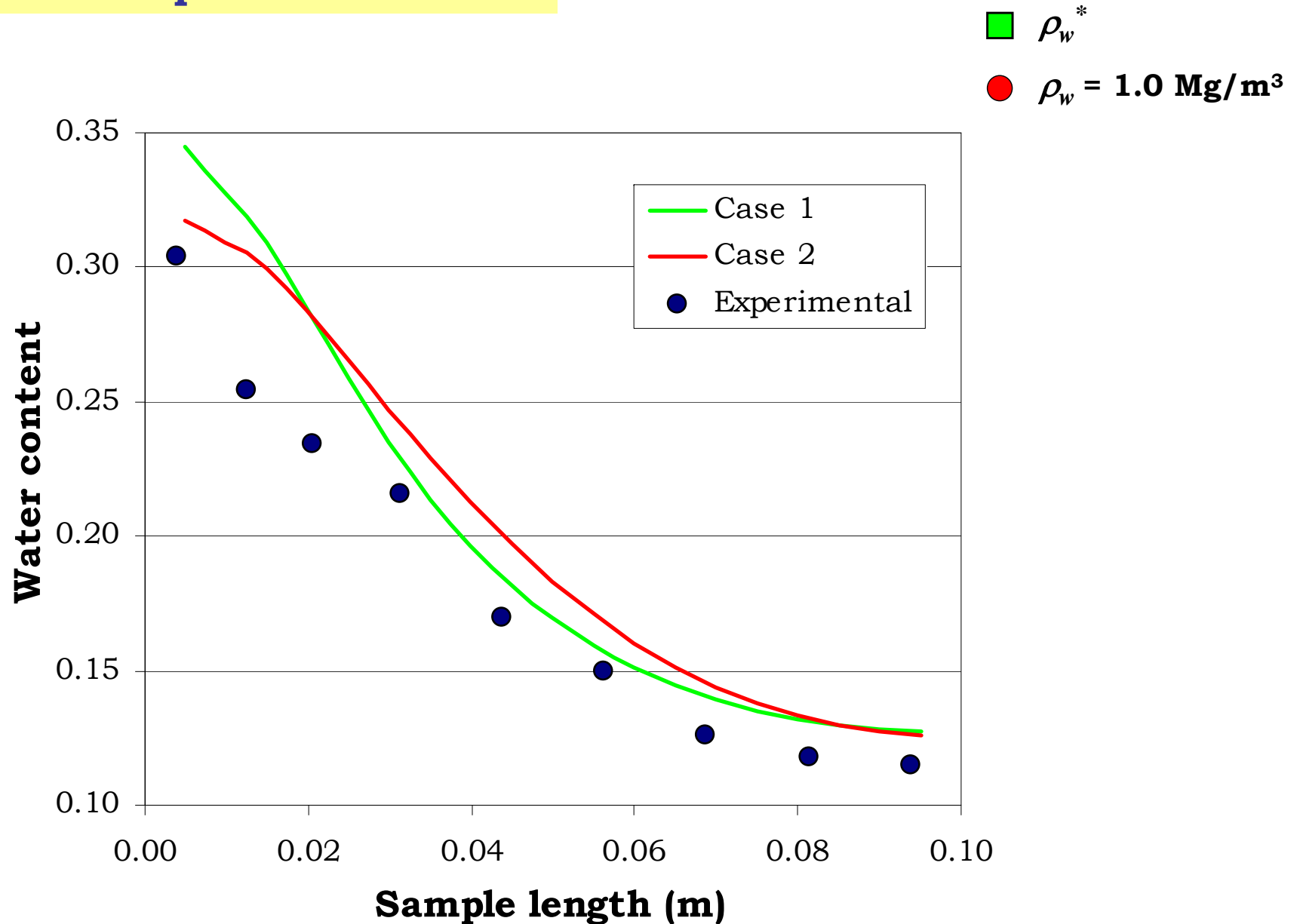
■  $\rho_w^*$   
●  $\rho_w = 1.0 \text{ Mg/m}^3$





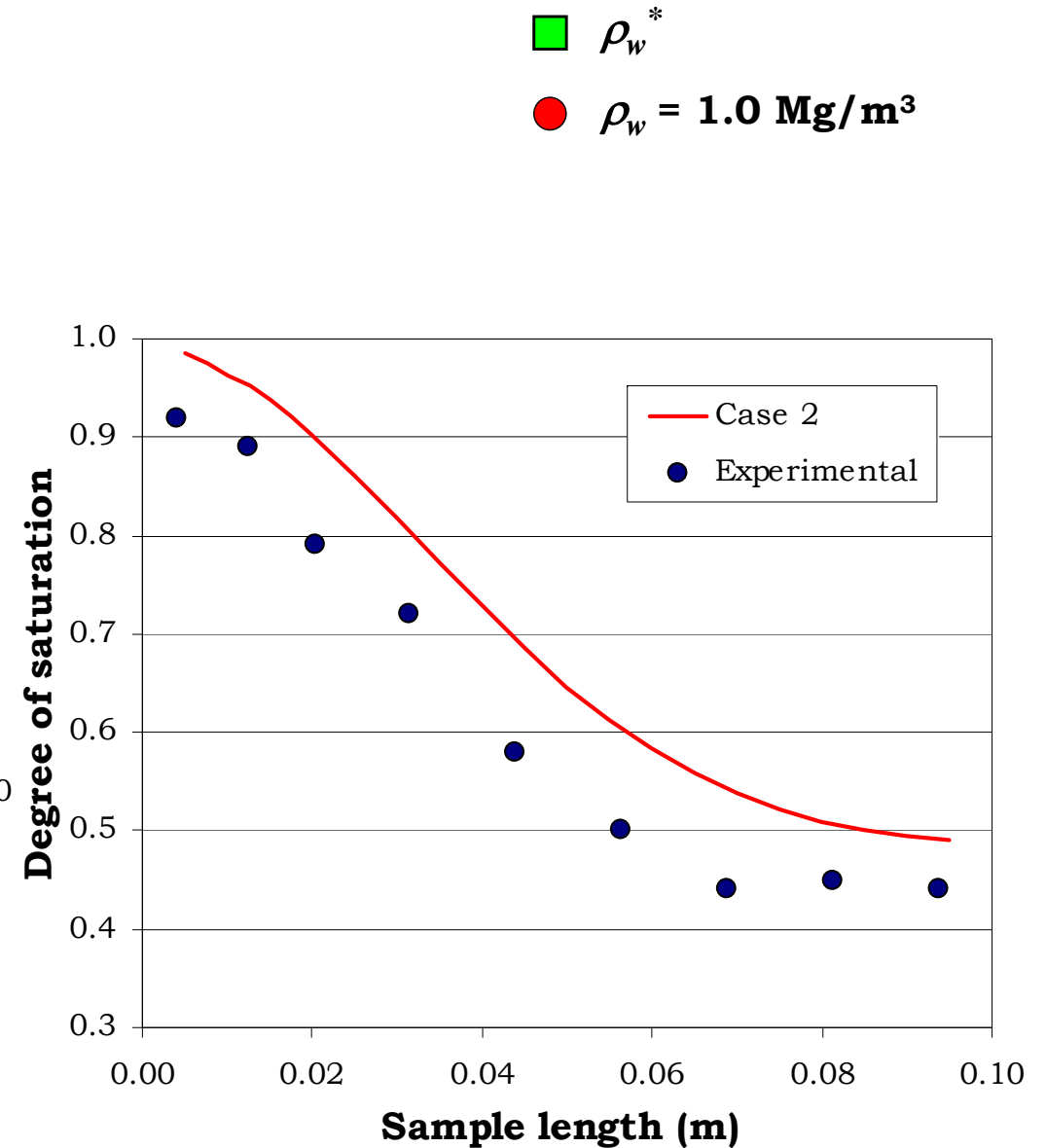
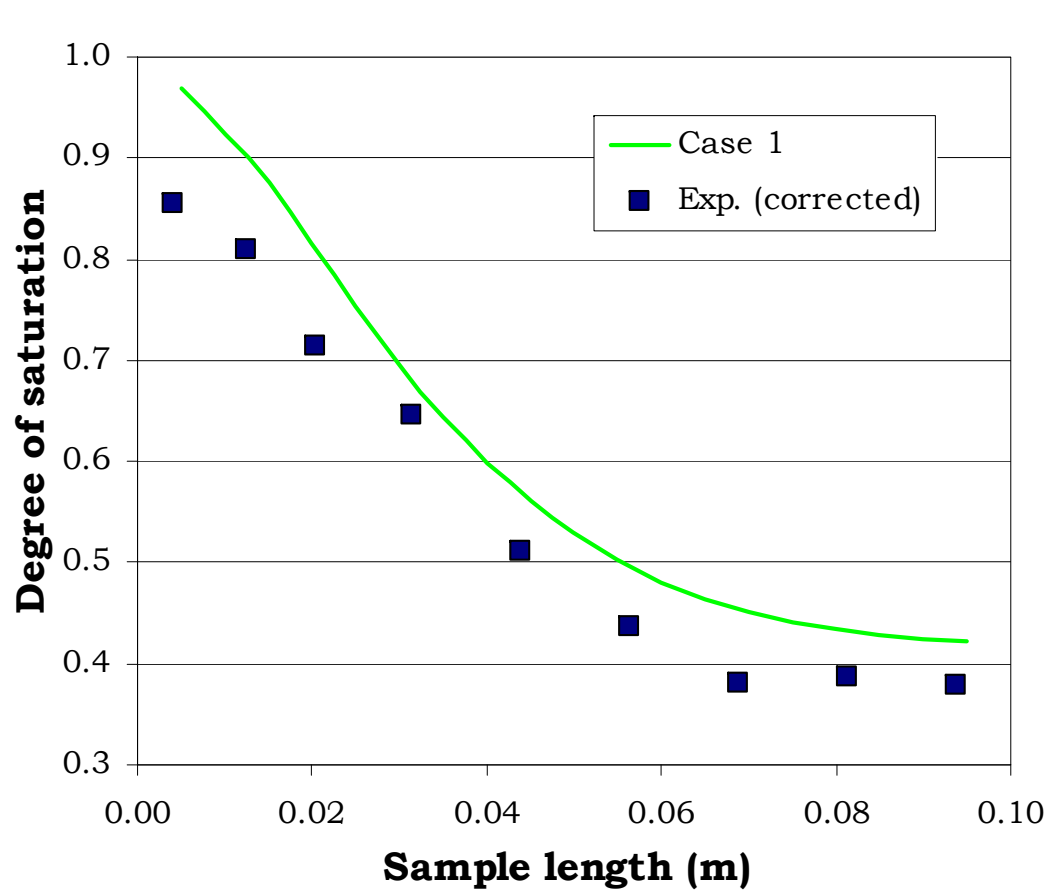
# HYDRATION OF A COMPACTED SAMPLE

## Application. Comparison of results



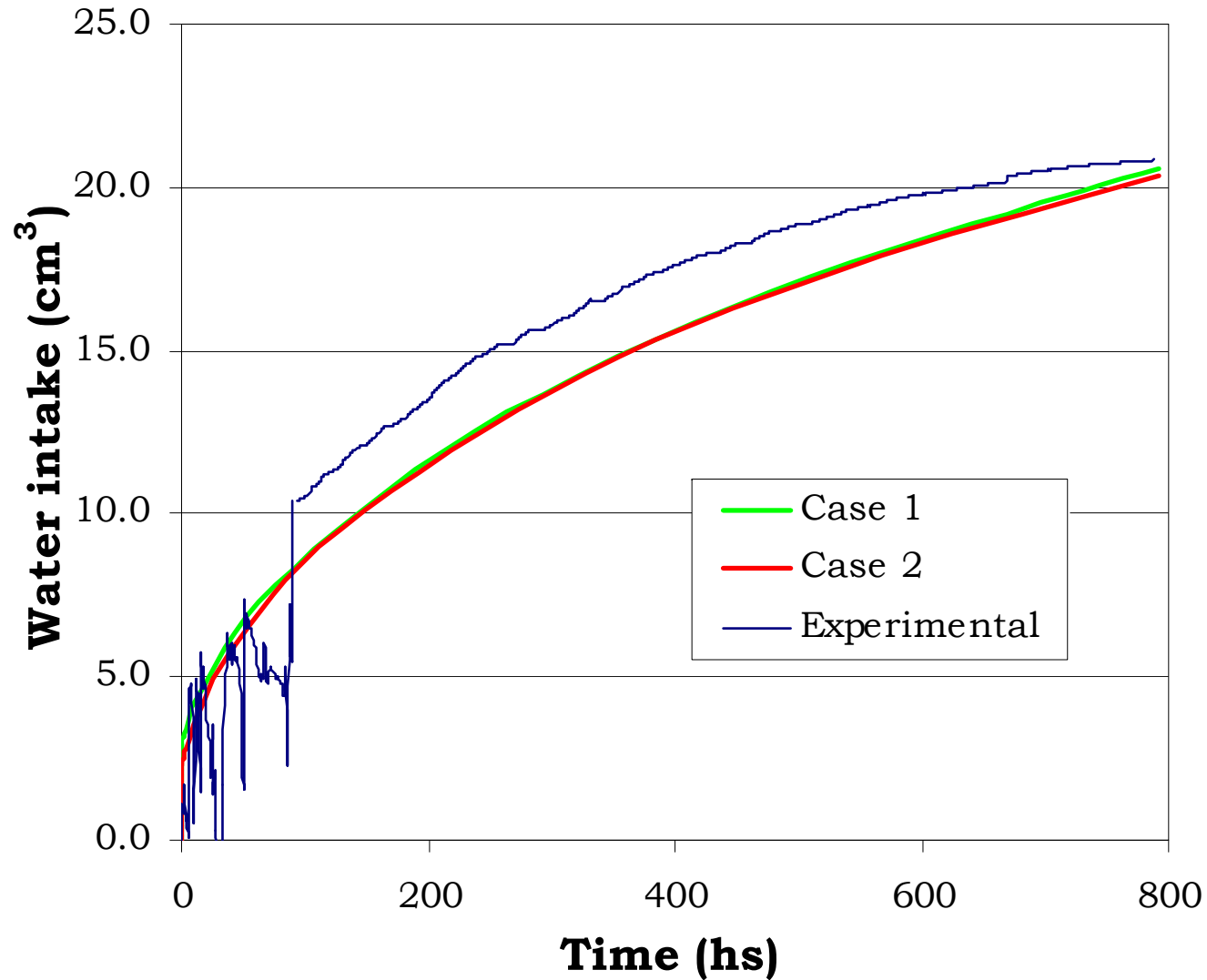
# HYDRATION OF A COMPACTED SAMPLE

## Application. Comparison of results



# HYDRATION OF A COMPACTED SAMPLE

## Application. Comparison of results

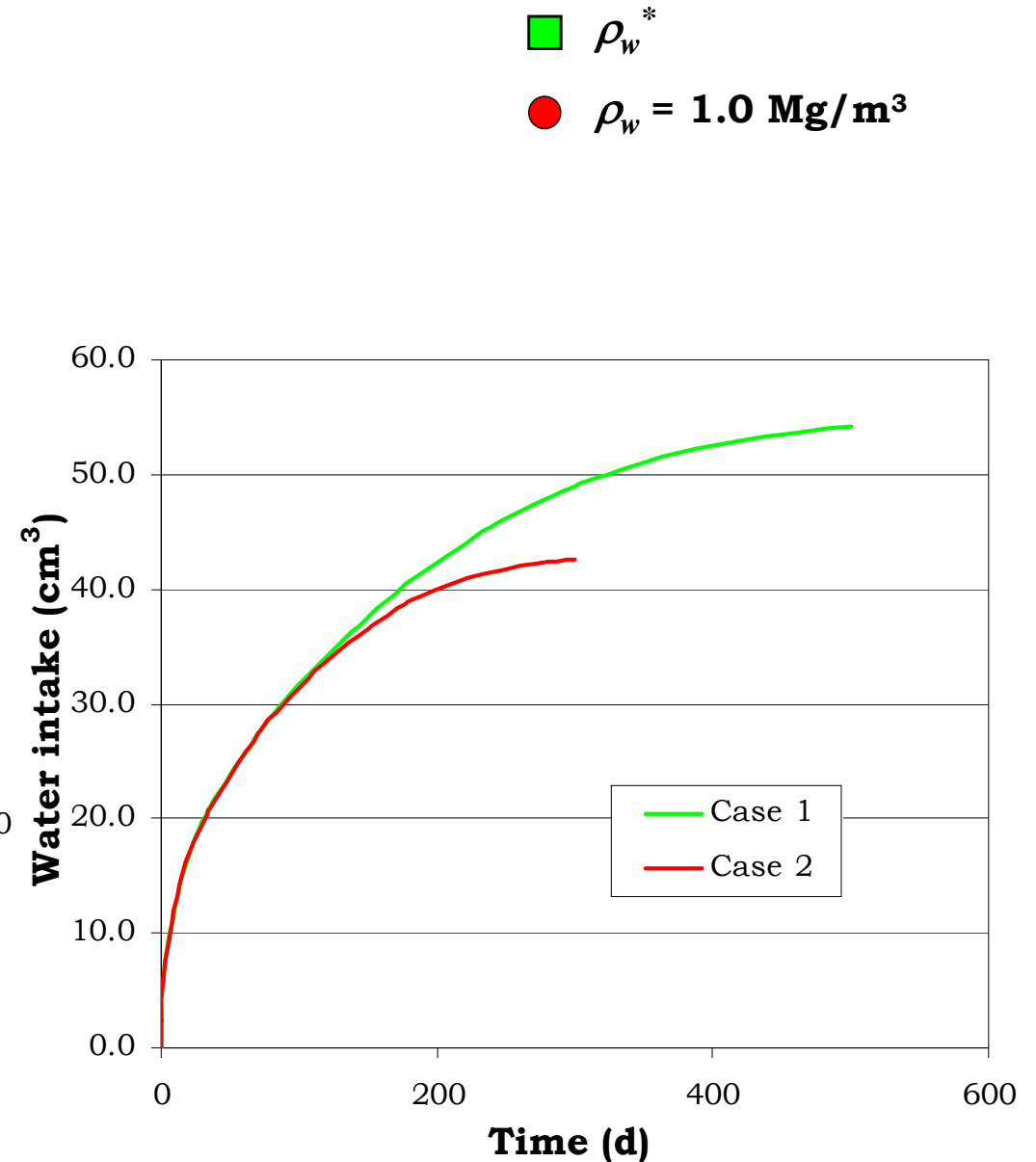
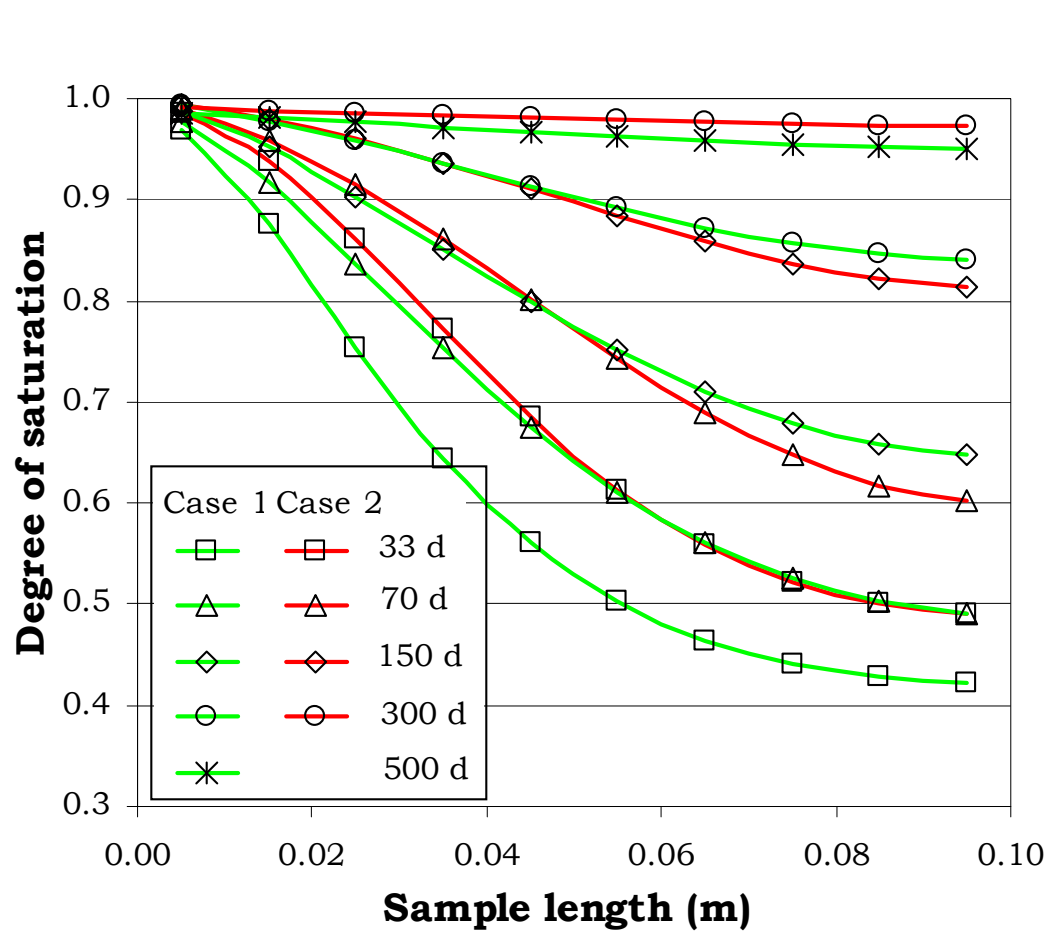


■  $\rho_w^*$

●  $\rho_w = 1.0 \text{ Mg/m}^3$

# HYDRATION OF A COMPACTED SAMPLE

## Application. Numerical test



# CONCLUDING REMARKS

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- Experimental data indicate that **density** of water attached to clay minerals is bigger than  $1.0 \text{ Mg/m}^3$ .
- Experimental results of an hydration test were reproduced using a **weighted water density** that incorporates the **clay-water interaction**.
- Numerical test suggests that full hydration of a compacted bentonite sample requires **more water** and **saturation time** than predicted using the bulk water density.

