

**Single-step pulsed electrodeposition of calcium phosphate coatings on titanium for
drug delivery**

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Abstract

Metallic implants have some limitations related to bioactivity and bacteria colonization leading to infections. In this regard, calcium phosphate coatings can be used as carrier for drug delivery in order to improve the mentioned drawbacks. The present work proposes the introduction of an antibacterial agent in the course of a pulsed and reverse pulsed electrodeposition. Calcium phosphate coatings were prepared in 30 min using different pulse waveforms (unipolar-bipolar), current densities (2-5mA/cm²) and temperatures (40-60°C). Mechanical stability of the as-coated surfaces was studied in order to select the optimal electrodeposition conditions. Subsequently, selected coatings were loaded with an antiseptic agent, Chlorhexidine digluconate (CHX), via a single-step co-deposition procedure. CHX concentration added to the electrolyte was adjusted to 3mM based on the antibacterial efficacy of the loaded coatings evaluated *in vitro* with *Staphylococcus aureus* and *Escherichia coli* bacteria strains. Whereas the same chlorhexidine concentration was added to the electrolyte, results showed that the amount of CHX loaded was different for each condition while release kinetics was maintained. The results of this work demonstrate that a pulsed co-deposition strategy has great potential to modulate local delivery of antibacterial agents such as chlorhexidine digluconate, which may prevent early phase infections of metallic implants after insertion.

Keywords: calcium phosphate, titanium, coating, pulse electrodeposition, antibacterial agent, characterization.

1. Introduction

Titanium and its alloys are the materials of choice for most orthopedic and dental applications due to their good biocompatibility with bone [1]. Poor osseointegration and infection around the implant, however, can affect its successful implantation. Many strategies have been proposed to either improve osseointegration or reduce bacteria colonization on the implant surface [2,3]. Multifunctional coatings, which can integrate both approaches, are a good option in order to enhance cell colonization while minimizing bacteria adhesion and proliferation [4,5]. In this regard, titanium (Ti) implants can be coated with calcium phosphates (CaP), which are recognized to be bioactive, and at the same time, this coating can be used as a drug delivery system [6–9]. Calcium phosphate coatings can be obtained by several techniques, including sol-gel synthesis, electrophoretic deposition, electrochemical deposition, plasma spraying and biomimetic process [10–12]. Among these coating processes, plasma spray deposition is the only technique commercially used for coating implants [13], but it suffers from certain drawbacks such as coating delamination, lack of uniformity and limited control of the layer composition and structure due to the extremely high temperature processing [14]. Due to those limitations, research has been focused on alternative methods of deposition.

In recent years, electrochemical deposition (ECD) has gained much attention due to the ability to deposit coatings on complex shape substrates at low temperature and with accurate control of the thickness and chemical composition, and it is relatively cheaper than other processes [15]. However, during conventional electrochemical deposition hydrogen bubbles (H_2) are produced at the vicinity of the cathode acting as a boundary layer which lowers the throughput of the ions. In order to circumvent this issue, pulsed cathodic electrochemical deposition has been used for coating titanium substrates [16–19]. Indeed the relaxation time (time off) between two unipolar pulses (PP) reduces the emission of H_2 . Furthermore during this period without current, ions diffusion from the solution to the surface of the cathode is

promoted, thus the uniformity of the ion concentration from the bulk solution to the cathode is increased [20–23]. As a result, a pulse cathodic electrochemical deposition process could produce coatings with higher uniformity and less porosity compared to direct current (DC) electrodeposition methods [24,25]. Moreover, coating adhesion to the titanium surface can be improved by using pulse reverse power (PRP). In this regard, changing the polarity of the current for a short time can promote the growth of adherent particles from the coated layer [26–28].

Coated surfaces can prevent initial bacterial adhesion by a local release of an antimicrobial agent [8]. Chlorhexidine digluconate (CHX) is an antiseptic with activity against a wide of microorganisms, including Gram-positive and Gram-negative bacteria, and has a low risk of associated drug resistance [29]. One of the mechanisms that can explain its efficacy is based on the adsorption of cationic CHX molecule to phosphate groups of the bacterial cell wall [30]. CHX can be easily adsorbed on calcium phosphate coatings by soaking the samples in a CHX-loaded solution [31]. However, adsorbed CHX may be prone to be quickly removed by body fluids preventing prolonged drug delivery at the dose needed to avoid post-surgical infection development.

In order to delay the CHX desorption, it has been proposed to cover the CHX-loaded surfaces with a lipid layer [29]. Nevertheless, this hydrophobic layer might also prevent cell adhesion resulting in poor implant stability and osseointegration. An alternative approach for loading the antibacterial agent is by co-deposition with CaP, a methodology that incorporates CHX in the CaP coatings by adding CHX to the electrolyte used in the electrodeposition process [32].

Although many authors have explored the deposition of CaP by pulse electrodeposition, the present study is focused on the fabrication of an adherent CHX-loaded CaP coating by using pulsed and reverse pulsed current, working at low current densities and reduced processing time (30 min). To the best of our knowledge, so far there is no report on co-deposition of

CHX/CaP coatings obtained by pulsed and reverse pulsed electrodeposition. The effect of temperature and current density on the morphology as well as on the coating adhesion to the substrate was evaluated on both unipolar and bipolar current waveforms. Based on the results, process conditions providing improved layer adhesiveness were selected to study the CHX co-deposition. Furthermore, the drug release profiles were modelled and compared. Finally, *in vitro* biological assays were performed to determine both the cell adhesion and the antibacterial response against *S.aureus* and *E.coli*.

2. Materials and Methods

2.1. Sample preparation

Samples were prepared from grade 2 titanium (Ti) disks (10mm diameter, 2mm thickness) polished with silicon carbide papers from 400 to 1200 grit and finally colloidal silica to obtain a mirror finish surface. Polished samples were ultrasonically cleaned in acetone, ethanol and ultrapure water. Before electrodeposition, samples were treated in NaOH 5M solution for 24 hours at 60°C [33], rinsed with ultrapure water and dried in a desiccator.

2.2. Pulsed electrodeposition

Pulsed electrodeposition of calcium phosphate coatings was performed in a solution prepared by mixing 0.042M of $\text{Ca}(\text{NO}_3)_2 \cdot 4\text{H}_2\text{O}$ and 0.025M of $\text{NH}_4\text{H}_2\text{PO}_4$ with a Ca/P molar ratio of 1.67, at pH 4.2 [34]. The reagents were all analytical grade (Sigma-Aldrich, USA). The electrochemical deposition was conducted in an individual cell using a three electrode configuration, in which a platinum electrode acted as an anode, a saturated calomel electrode (SCE) as reference electrode and the titanium sample as cathode. Electrodeposition was carried out using a potentiostat (PARSTAT 2273, Princeton Applied Research, Oak Ridge,

TN, USA) by pulsing the current for 30 min. Two different pulse wave forms were studied: unipolar pulse plating, hereafter termed PP, and bipolar pulse reverse plating where anodic and cathodic pulses are mixed, referred to as PRP (Fig. 1).

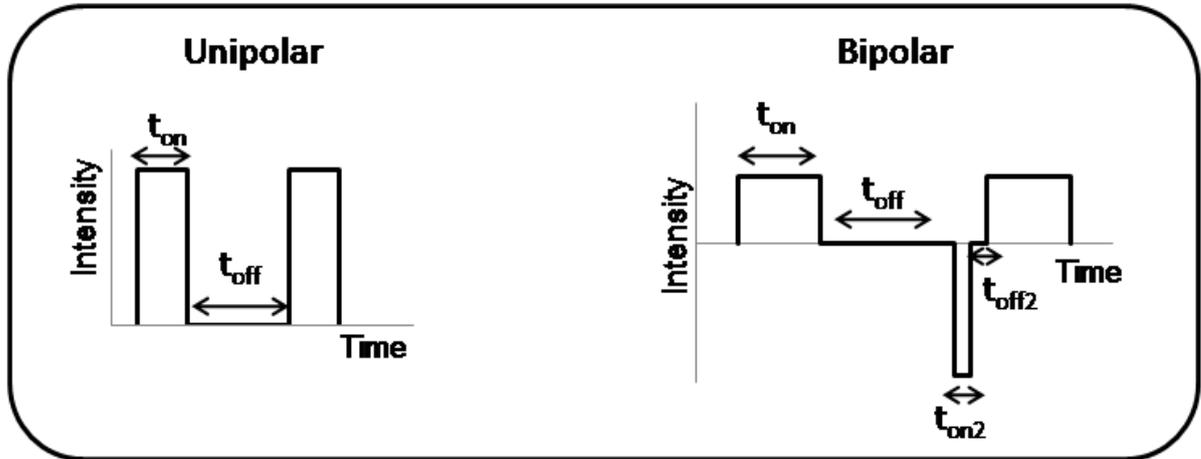


Fig. 1: Schematic representation of unipolar and bipolar pulse waveforms.

Different current densities and process temperatures were evaluated (Table 1).

Table 1: Electrochemical parameters used for calcium phosphate coatings.

Conditions	i_{on1} (mA/cm ²)	t_{on1}/t_{off1} (s)	i_{on2} (mA/cm ²)	t_{on2}/t_{off2} (s)	T (°C)
PP40_2	2	1/2	-	-	40
PP40_5	5	1/2	-	-	40
PP60_2	2	1/2	-	-	60
PP60_5	5	1/2	-	-	60
PRP40_2	2	1/1.6	-4	0.2/0.2	40
PRP40_5	5	1/1.6	-10	0.2/0.2	40
PRP60_2	2	1/1.6	-4	0.2/0.2	60
PRP60_5	5	1/1.6	-10	0.2/0.2	60

Then, chlorhexidine digluconate 20% (w/v) (Sigma-Aldrich) was incorporated into the electrolyte solution at different concentrations: 0.3, 0.6, 1.5, 3, 6 and 12mM, for selected electrodeposition conditions. After the electrodeposition, samples were removed from the electrolytic cell, rinsed with distilled water and dried at room temperature [32].

2.3. Physico-chemical characterization

The microstructure of the coatings was determined by X-ray diffraction (XRD) using a monochromatic Cu K α radiation (Bruker D8 Advance Instrument, Germany) at a scan rate of 1°/s, in the 2 θ range of 4-80°. The incorporation of CHX was confirmed by micro-Raman spectroscopy (LabRam Confocal Raman, Horiba Jobin Yvon, UK) with a 532nm laser, a 600 grating and a x100 magnification objective. Spectra were obtained from three scans of 60s each. Moreover, samples before and after loading were also analyzed by micro-Raman to observe changes on the chemical composition.

The surface morphology of the coatings was examined by Zeiss Neon40 scanning electron microscope (SEM Carl Zeiss NTS GmbH, Jena, Germany) at a potential of 2kV. Furthermore, cross-sectional SEM images of the different calcium phosphate coatings were obtained for the estimation of coating thicknesses by partially covering the surface of the samples during the electrodeposition.

The average surface roughness (R_a) was measured with a white-light profiling system WYKO NT9300 (Veeco Instruments, Plainview, NY, USA) in vertical scanning interferometry (VSI) mode using a 50X objective lens. Ten measurements were acquired for each sample at different positions.

The adhesion strength of the CaP coatings to the substrate was evaluated by tensile test according to the ASTM F1147 international standard. Briefly, the coated Ti disks were bonded to cylindrical sample holders with FM 300K epoxy adhesive film (Cytec Engineered Materials, USA). The epoxy film was cured by heating the specimens up to 175°C in 30min and maintaining this temperature for 60min. The tensile strength test was performed on a universal testing machine (Microtest MT, Microtest, Spain) at a constant cross-head speed of 2.5mm/min. Three samples for each coating condition were tested to obtain average values of

the adhesion strength. Coatings with higher adhesion strength were used to carry out the biological assays.

2.4. Biological characterization

2.4.1. Cell adhesion and coating degradation

Cell adhesion was conducted with Ti disks coated with the previous selected conditions without CHX. The assay was performed with human osteoblast-like SaOS-2 cells (ATCC, USA) cultured in McCoy's 5A medium (Sigma-Aldrich) supplemented with 10v/v% fetal bovine serum (FBS), 50U/mL penicillin, 50 µg/mL streptomycin, 20mM HEPES and 2mM L-glutamine, all from Invitrogen. Seeding was conducted at a density of $2 \cdot 10^4$ cells/well, on triplicate specimens, and incubated for 6h in a 48-well culture plate. Cells were lysed with mammalian Protein Extraction Reagent (m-PER; Pierce, Rockford, IL, USA). The number of attached cells was quantified by using the cytotoxicity detection kit LDH (Roche Applied Science, Germany). The lactate dehydrogenase (LDH) activity was determined by measuring the absorbance using a microplate reader (Synergy™ HTX Multimode reader, USA) at 492nm and then, a calibration curve was used in order to obtain the results as cells number. Uncoated Ti samples were used as controls.

The degradation of the coatings was evaluated by quantifying the calcium and phosphate ions content on the cell adhesion assay supernatants (medium in contact with samples). Calcium concentration was studied by *o*-cresolphthalein complexone method [35,36]. This technique is based on the formation of a colored complex with *o*-cresolphthalein complexone in an alkaline medium. Absorbance was measured at 570nm (Infinite M200 Pro, Tecan, Switzerland). On the other hand, phosphate colorimetric assay kit (Sigma-Aldrich) was used for measuring (650nm) the amount of phosphate present in the sample supernatants.

2.4.2. Bacteria growth curves

The antimicrobial activity was tested against gram positive *S.aureus* (CCUG 15915, Culture Collection University of Göteborg, Sweden) and gram negative *E.coli* (CECT 101, Colección Española de Cultivos Tipo, Spain). Both bacterial strains were grown and maintained in Brain-Heart Infusion (BHI, Scharlab, Spain). Before each assay, bacteria were cultured and incubated overnight. Bacterial growth curve assay was performed in double-well culture plates [37]. Samples were immersed in 2mL of diluted bacterial suspension adjusted to an absorbance of 0.02 ± 0.01 at 600nm (10^6 colony-forming units (CFU)/mL) using a photometer (Laxco MicroSpek™ DSM, USA). The absorbance was monitored for 16 hours by measuring absorbance at 600nm with a multimode microplate reader (Synergy™ HTX Multimode reader, USA). Medium without bacteria and bacterial suspension were used as negative and positive controls, respectively.

2.4.3. Agar diffusion test

The diffusion assay was carried out by adding 100μL of inoculum to agar and BHI poured into petri dishes. Previously, optical density of each bacterial suspension (*S.aureus* and *E.coli*) was adjusted to 0.2 ± 0.01 at 600nm, corresponding approximately to 10^8 CFU/mL. Triplicates of each condition were placed on the surface of the agar plates and incubated for 24h at 37°C. Untreated titanium samples and coated disks without CHX-loading were used as controls. The result of inhibition was calculated by measuring the width of the inhibited zone around each sample.

2.5. *In vitro* drug release

The drug release was performed by immersing samples loaded with CHX (hereafter named PRP40_2CHX and PP60_2CHX respectively) in 1mL of Tris(hydroxymethyl)methylamine buffer solution (TRIS, VWR International Ltd., UK) at physiological pH and 37°C, under sink conditions [38]. At each time point, solution was withdrawn and replaced by fresh TRIS. The

amount of CHX was determined from a calibration curve obtained by monitoring the absorbance of known concentration of CHX in TRIS buffer solution with a UV-spectrophotometer (Shimadzu model 3600, Tokyo, Japan; $\lambda=254\text{nm}$). Triplicates of each condition were used. Moreover, unreleased CHX was quantified by immersing one sample of each condition (from the final time point) in 1mL of HNO_3 0.1M and then measuring the absorbance of the fully dissolved CHX-loaded CaP coating using the corresponding calibration curve [29]. These values added to the total released CHX showed the real amount of CHX loaded into the CaP coating. After release, samples morphology was studied by scanning electron microscope (SEM, Quanta 450, Bruker, USA).

CHX release profiles were fitted to different mathematical models (Korsmeyer-Peppas, Higuchi and Kopcha). Korsmeyer-Peppas model (KP) can provide insights regarding the limiting drug release mechanism. The concentration of drug released was correlated to Eq.1, where M_t is the drug amount released at time t , M_∞ is the maximum amount released from the material in these experimental conditions, k is a constant incorporating characteristics of the network system and the drug, and n is the released exponent that is indicative of the limiting transport mechanism. M_t/M_∞ was calculated for each specimen and averaged for each condition using the concentration and time data of the first 60% of the fractional release in which the equation is valid [39].

$$M_t/M_\infty = kt^n \quad (\text{Eq.1})$$

Higuchi model is represented by Eq.2, where a is the diffusion constant. This model offers a good correlation with release patterns where Fickian diffusion is the predominant mechanism [40].

$$M_t/M_\infty = at^{0.5} \quad (\text{Eq.2})$$

Kopcha model can be used to study the contribution of the diffusion (A) and erosion (B) mechanisms. When the ratio A/B is higher than 1, the contribution of the diffusion is predominant (Eq.3).

$$M_t = At^{0.5} + Bt \quad (\text{Eq.3})$$

Moreover, the release profiles of the two studied conditions have been compared using the difference factor f_1 and the similarity factor f_2 from the model independent approach described by the FDA (Food and Drug Administration) and the EMA (European Medicines Agency). In Eq.4 and Eq.5, n is the number of time points, R_t and T_t are the dissolution values of the reference and the batch respectively, at time t [41].

$$f_1 = \left\{ \frac{\sum_{t=1}^n |R_t - T_t|}{\sum_{t=1}^n R_t} \right\} \cdot 100 \quad (\text{Eq.4})$$

$$f_2 = 50 \cdot \log \left\{ \left[1 + \left(\frac{1}{n} \sum_{t=1}^n (R_t - T_t)^2 \right)^{0.5} \right] \cdot 100 \right\} \quad (\text{Eq. 5})$$

The value of these factors should be between $50 < f_2 < 100$ and $0 < f_1 < 15$ in order to consider the two release profiles comparable, as reported by other authors [42].

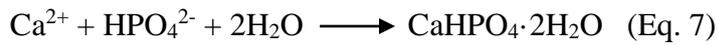
2.6. Statistical analysis

All data presented in this study are given as mean value \pm standard deviation. At least triplicate samples ($n=3$) were used for statistical analysis, except for roughness study where ten samples were analyzed. One-way ANOVA followed by the Student's test was used to analyze the significant differences ($p < 0.05$) between group average values.

3. Results and discussion

3.1. Selection of coating conditions before CHX-loading

Selection of coating conditions was performed with samples without Chlorhexidine. Electrochemical deposition is based on the pH-dependent solubility of CaP. The pH is increased near the cathode due to the presence of hydroxyl ions generated by the reduction of water (Eq.6) [43]. Consequently, acid-base and precipitation reactions lead to the formation of different CaP phases depending on the process conditions (Eq.7 and 8) [20].



Phase composition of the as-coated samples was studied by XRD (Fig. 2). The results confirmed the presence of sharp peaks corresponding to brushite phase (DCPD, $\text{CaHPO}_4 \cdot 2\text{H}_2\text{O}$, according to JCPDS n. 72-0713 brushite standard). Furthermore, the presence of peaks associated with octacalcium phosphate (OCP, $\text{Ca}_8(\text{HPO}_4)_2(\text{PO}_4)_4 \cdot 5\text{H}_2\text{O}$), according to JCPDS n. 79-0423 octacalcium phosphate standard) was confirmed. This can be due to an increase of hydroxyl ions concentration in the electrolyte which promotes the precipitation of OCP [20,44]. These calcium phosphate phases might have an influence in bone growth since they are known as precursors of HA formation [45].

Peaks were also assigned to the alpha titanium substrate (JCPDS card no. 89-2762). It is noteworthy that the peaks relative intensity can differ from standard patterns. This is described in the literature to occur in electrochemical processes due to the favored growth of the crystal perpendicularly to the substrate surface [46,47].

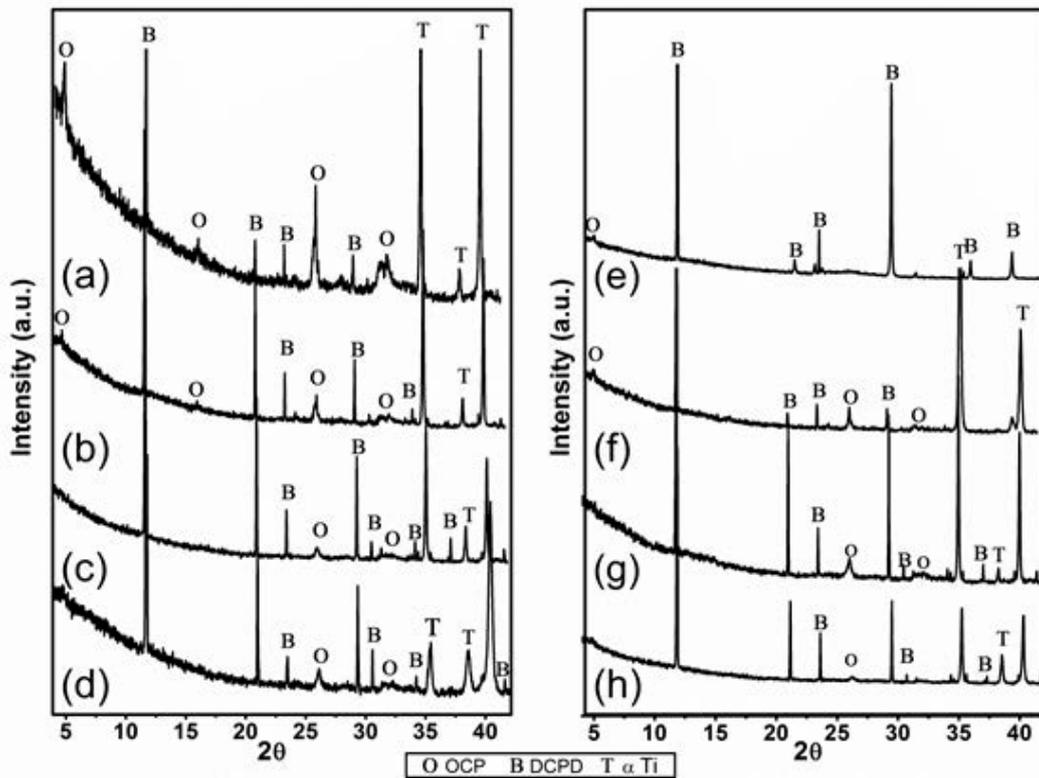


Fig. 2: XRD diagrams of pulsed electrodeposited coatings: a)PP60_5, b)PP60_2, c)PP40_5, d)PP40_2, e)PRP60_5, f)PRP60_2, g)PRP40_5 and h)PRP40_2.

The microstructure of the coatings was observed by SEM. The images showed uniform surfaces without the presence of porosity. This was expected due to the reduction of H₂ bubble formation near the surface of the cathode during the pulse and reverse pulse electrodeposition [48]. To confirm this effect, a cyclic voltammetry test was carried out. As shown in fig. 3, for values under -1.3 V the linear increase in the cathodic current density evidences the electrolysis of water and the formation of hydrogen bubbles [49]. The effect of the H₂ bubbles is evidenced in Fig. 4a, representative of the CaP coating achieved on titanium by direct current (DC) without pulsing, in mean current conditions equivalent to those of samples PP40_5 and PRP40_5. As a comparison, samples treated in pulsed regimes, either without reverse pulse (PP40_5, fig. 4b) or with reverse pulse (PRP40_5, fig. 4c) do not show any of the surface defects evident on the DC-treated sample.

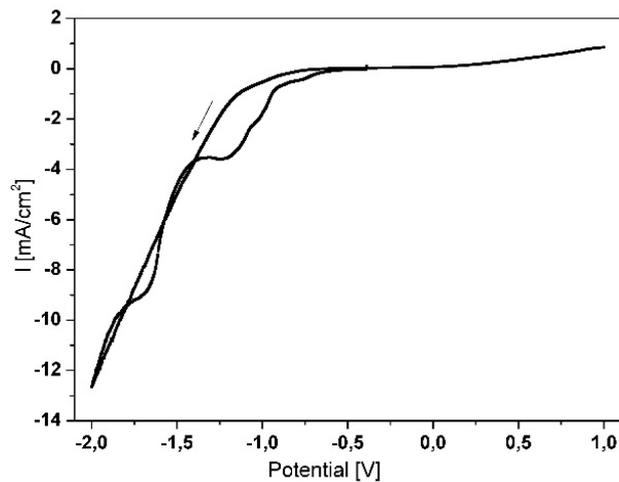


Fig. 3. Cyclic voltammetry under potentiodynamic conditions [scan rate: 2mV/s].

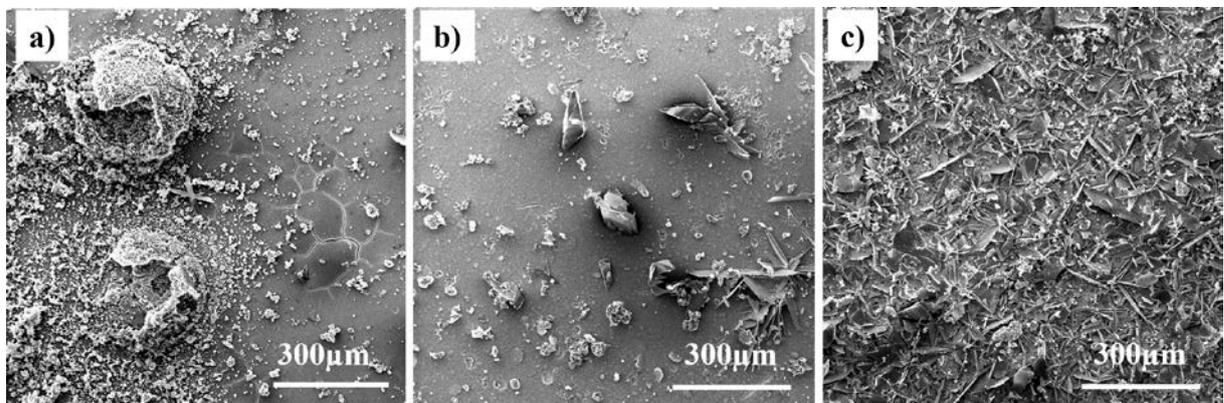


Fig. 4: a) CaP coating on titanium by direct current without pulsing, b) PP40_5 condition, c) PRP40_5 condition.

In the SEM analyses shown in Fig.5, two crystal morphologies are observed for all treated surfaces: a region composed of large platelet-like crystals of approximately 30 μ m in length and a region composed of needle-like crystals of around 5 μ m in length. The pulse waveform and current density do not seem to present a significant effect on the coating morphology. Conversely, the smaller crystals exhibit morphologic differences when the temperature of the process is modified. As the temperature is increased, the platelet-like morphology observed at 40°C (Fig. 5c,d,g,h) is replaced with a needle-like morphology (Fig. 5a,b,e,f). This can be attributed to the increased diffusion rate of the ions in the electrolyte when temperature increases, promoting the nucleation and growth of needle-like crystals.

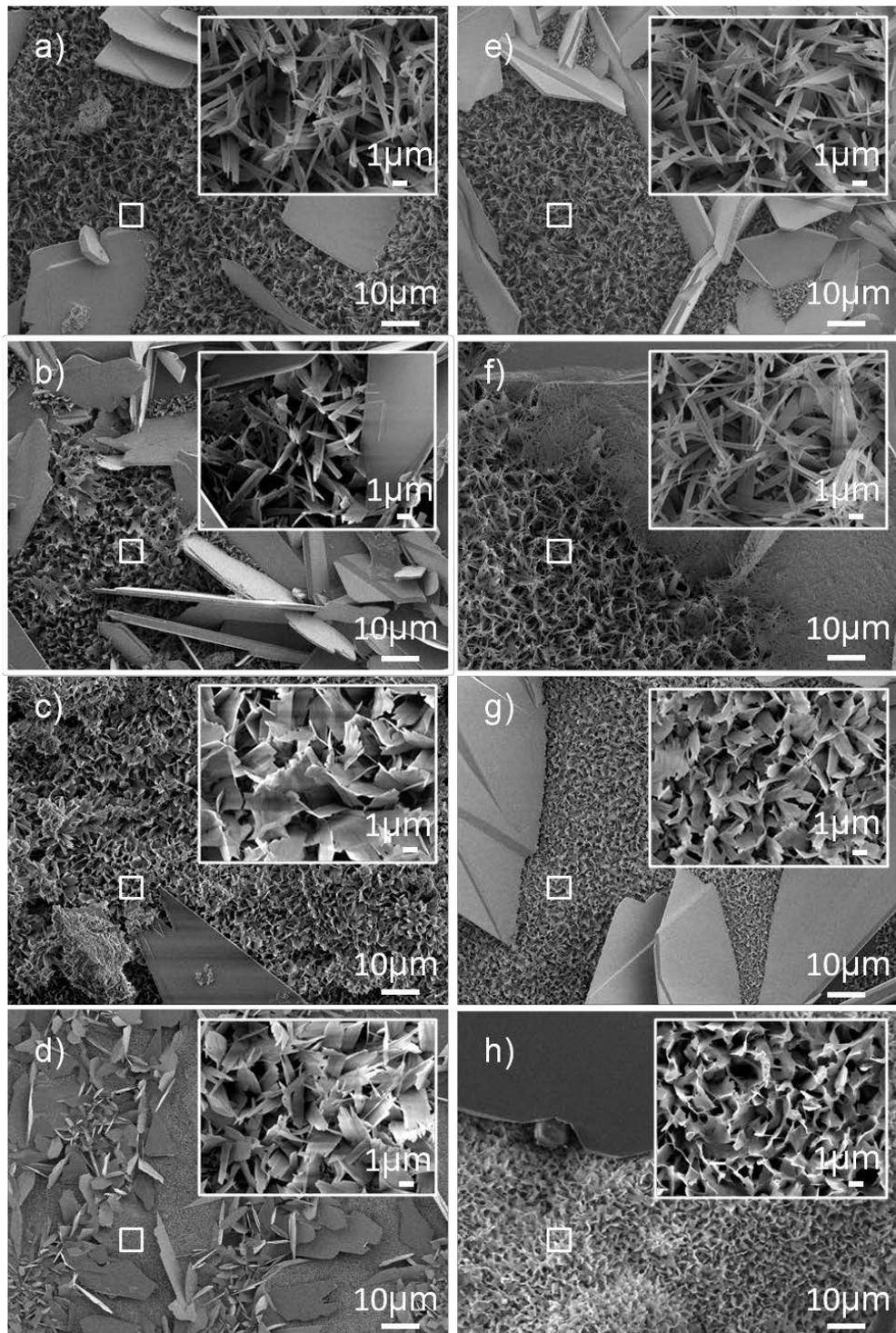


Fig. 5: SEM micrographs showing crystal morphology of calcium phosphate coatings on titanium substrates obtained by pulse plating at 40°C and 60°C: a) PP60_5, b) PP60_2, c) PP40_5 and d) PP40_2 and by pulse reverse plating at 40 °C and 60°C: e) PRP60_5, f) PRP60_2, g) PRP40_5 and h) PRP40_2. A more detailed view (at higher magnification) is presented in each insert.

Coating thickness of samples obtained in different conditions were evaluated based on cross-section SEM images, with values ranging from 10 to 24 μm (Table 2).

Table 2: Coating thickness and adhesion strength values of different electrodeposition conditions. Samples with the same symbol indicate no statistically differences ($p < 0.05$).

Conditions	PP40_2	PP40_5	PRP40_2	PRP40_5	PP60_2	PP60_5	PRP60_2	PRP60_5
Thickness (μm)	11 \pm 1*	15 \pm 1 ^{#,&}	12 \pm 1 ^{*,#}	17 \pm 2 ^{&,\$}	17 \pm 2 ^{&}	22 \pm 1 ^{∞}	14 \pm 1 ^{*,#,&}	21 \pm 2 ^{§,∞}
Adhesion strength (MPa)	30 \pm 1*	27 \pm 3 ^{*,#}	36 \pm 4*	32 \pm 1*	35 \pm 1*	24 \pm 1 ^{*,#}	29 \pm 3 ^{*,#}	14 \pm 9 [#]

Results showed that, with increasing temperature up to 60°C, the coating thickness increases. This is attributed to change of diffusion and reaction rate that can promote the layer formation [50]. Correspondingly, the thickness of the deposited films was increased by raising the current density (Fig. 6). This result was expected since the change of polarity may act as a stripping time in the PRP cycle, which selectively redissolve less adhered CaP particles [26].

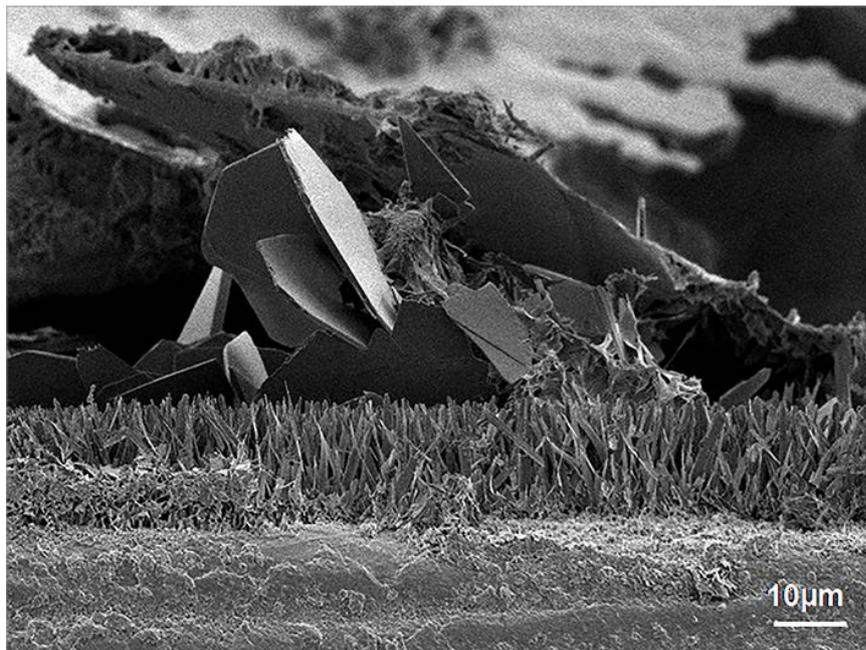


Fig. 6: SEM micrograph of PP60_2 coating cross-section.

Adhesion of the CaP coatings to the substrate is of the utmost importance for the implant to function properly in physiological conditions. The adhesion strength for PRP40_2 coating obtained by combining reverse pulses with low temperature and low current density was about 36 ± 4 MPa. Similarly, coatings obtained in PP60_2 conditions showed an adhesion strength of 35 ± 1 MPa (Table 2). Both conditions exceed the 22MPa in tensile strength required by FDA Guidance for Metallic Plasma Sprayed Coatings on orthopedic implants [51]. Conversely, thicker coatings obtained in PP60_5 and PRP60_5 conditions present both lower adhesion strength, probably due to coating delamination [11]. According to these results, the best electroplating deposition conditions were established to be at PRP at 40°C and 2mA/cm² and PP at 60°C and 2mA/cm². In this regard, both coating conditions were selected for incorporating CHX and studying drug release and biological response.

3.2. Presence of Chlorhexidine

Coatings loaded with 3mM of Chlorhexidine added in the electrolyte were analyzed by Raman spectroscopy. For both coated surfaces, the incorporation of CHX was confirmed by the presence of a sharp peak at 1597 cm⁻¹ in the Raman spectrum due to the C=C stretching of aromatic ring (Fig.7a) [52]. Raman spectra also confirmed the presence of OCP (958cm⁻¹, 967cm⁻¹) for both coating conditions and DCPD (986cm⁻¹) for PP60 [53]. Moreover, loaded CHX has no significant effect on the phase composition of the coatings (Fig 7b and 7c).

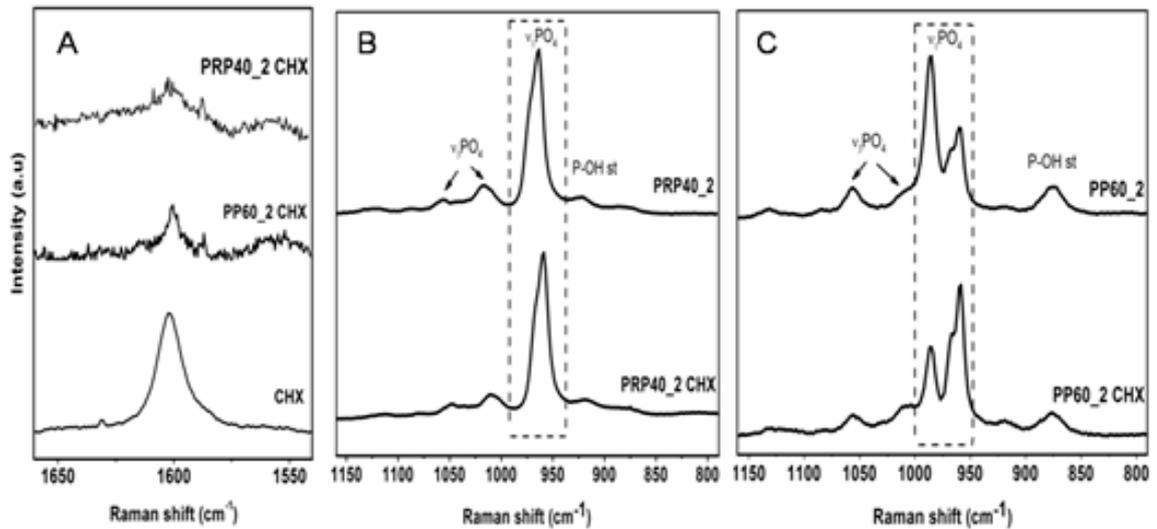


Fig. 7: Raman spectra in different wavenumber domains of CHX and CHX-loaded coatings: a) CHX in PRP40_2CHX, PP60_2CHX and 20% w/v CHX b) PRP40_2 and PRP40_2CHX and c) PP60_2 and PP60_2CHX.

3.3. Biological assays

3.3.1. Cell adhesion

Cell adhesion was studied for PRP40_2 and PP60_2 conditions in order to evaluate the cell attachment on coated surfaces without CHX (Fig. 8). Both coating procedures enhance cells attachment to the surface after 6h of incubation. A significant difference was observed in cells attached on PP60_2 and PRP40_2 surfaces compared to titanium control. Topography and surface roughness were shown to affect osteoblast-like cell adhesion (Fig. 8a). In this regard, PP60_2 had the highest surface roughness ($R_a = 3.32 \pm 0.39 \mu\text{m}$) compared with that of PRP40_2 sample ($R_a = 2.07 \pm 0.48 \mu\text{m}$). In addition, both results contrasted with the roughness of raw titanium samples ($R_a = 38.3 \pm 0.45 \text{nm}$) (Fig. 9). The increase of the average surface roughness for CaP-coated titanium may contribute to favor cell attachment [54]. Supernatant medium in contact with coated samples revealed a lower concentration of calcium ions compared with the initial medium and the medium after contact with Ti samples (Fig. 8b). However, phosphate concentration is quite stable, which could indicate that a process of dissolution and reprecipitation is taking place (Fig. 8c).

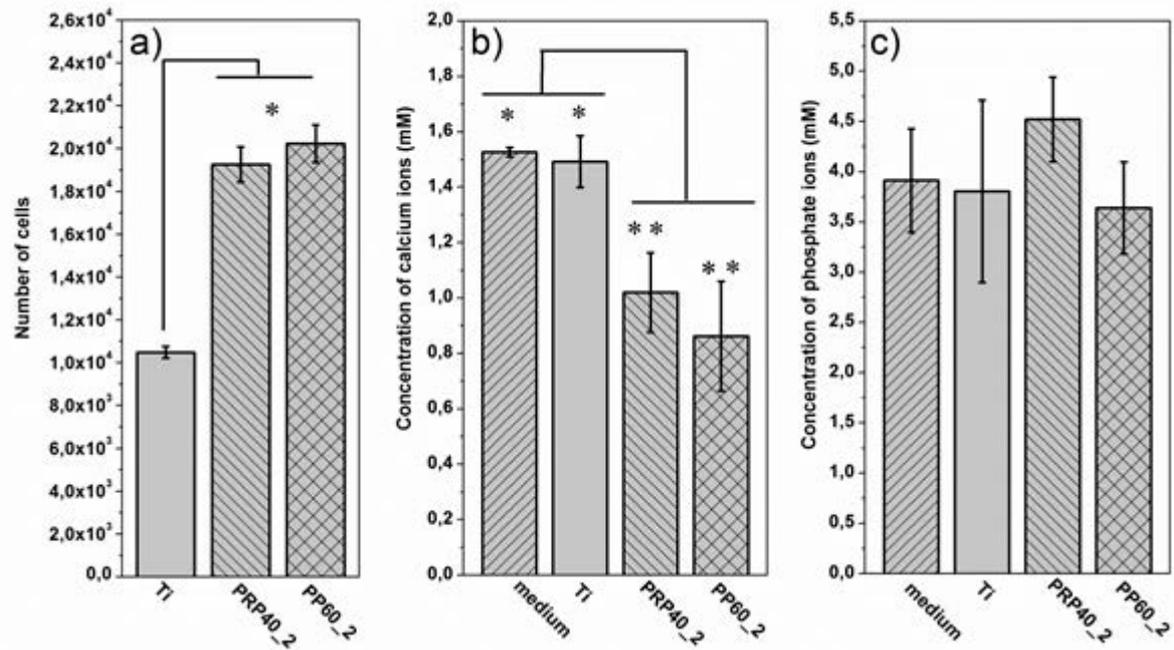


Fig. 8: a) Cell adhesion of SaOS-2 cells after 6h of incubation. Statistically significant differences versus control samples are indicated with an asterisk. Evolution of ionic concentration in the cell culture medium b) calcium ions and c) phosphate ions. Symbols indicate samples with statistically significant differences ($p < 0.05$).

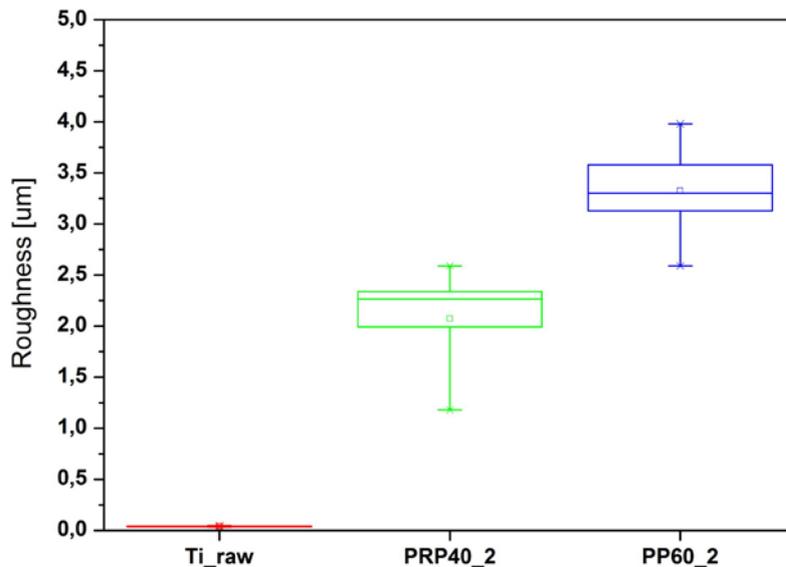


Fig. 9: Box plot of roughness measurements.

3.3.2. Bacteria growth curves

In order to adjust the CHX concentration that should be added to the electrolyte solution, bacteria growth curves were studied in presence of increased CHX concentrations (Fig. 10). For PP60_2CHX, CHX concentrations in the electrolyte above 0.6mM for *S.aureus* and 3mM for *E.coli* were needed to inhibit bacteria growth. In contrast, PRP40_2CHX required a lower concentration of CHX to prevent bacteria proliferation. These results allowed determining that 3mM was the minimal CHX concentration in the electrolyte needed to avoid bacteria growth.

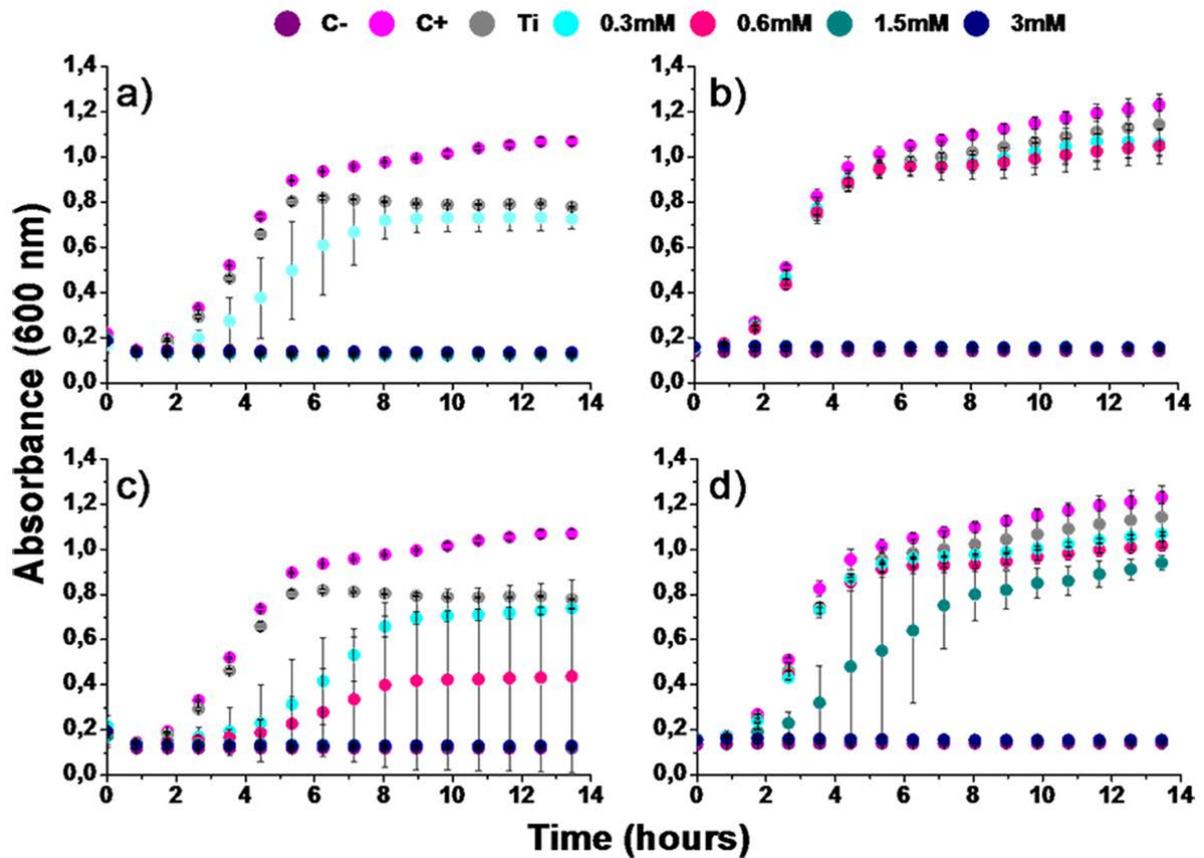


Fig. 10: Bacteria growth curves a) PRP40_2CHX with *S.aureus*, b) PRP40_2CHX with *E.coli*, c) PP60_2CHX with *S.aureus* and d) PP60_2CHX with *E.coli*.

3.3.3. Agar diffusion test

In vitro antibacterial activity of coated titanium discs with co-deposited CHX was evaluated by measuring the width of the inhibition zone around the samples (Fig. 11). All coated samples with CHX concentrations in the electrolyte above 3mM displayed antibacterial activity for both bacteria strains. These findings are in accordance with results obtained for the bacteria growth curves assay. Results also revealed that CHX was more active against Gram-positive bacteria than Gram-negative bacteria which is in conformity with literature [55]. Compared with Gram-positive bacteria, Gram-negative bacteria have an outer cell wall membrane that should probably increase its resistance to physical disruption and reduce susceptibility to CHX [30]. In line with the obtained results, the CHX concentration that should be incorporated in the electrolyte solution was chosen equal to 3mM.

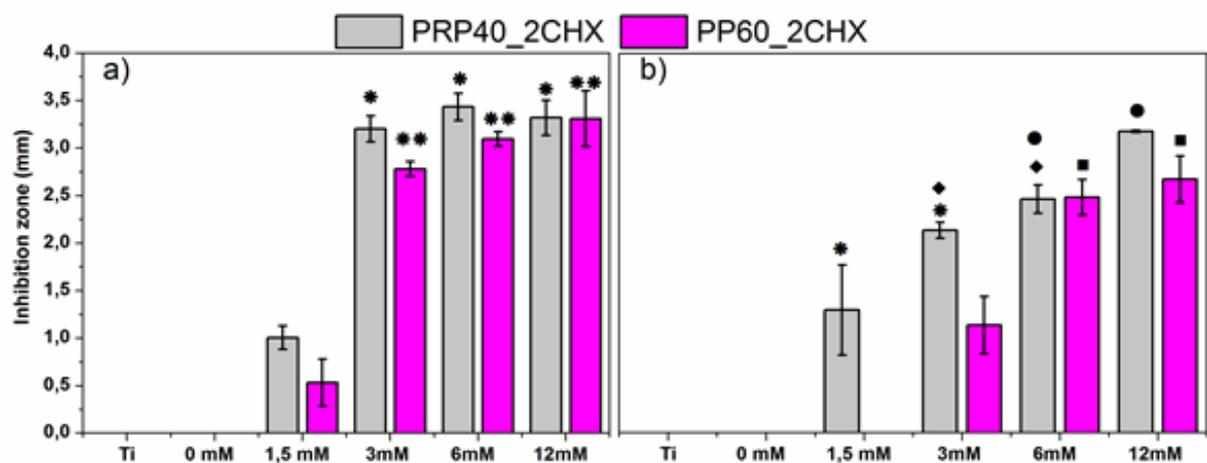


Fig. 11: Agar diffusion test of PRP40_2CHX and PP60_2CHX samples against a) *S.aureus* and b) *E.coli*. Symbols indicate significant differences ($p < 0.05$).

3.4. *In vitro* drug release

Even if the CHX concentration added to the electrolyte was the same for both conditions (3mM), the total amount of CHX co-deposited was found to be higher for PRP40_2CHX samples ($45 \pm 19 \mu\text{g/mL}$) compared to that for PP60_2CHX condition ($14 \pm 4 \mu\text{g/mL}$). This difference could be probably due to the effect of the reverse pulses which may present a

higher increase of the pH at the vicinity of the cathode. For that reason, PRP40_2CHX condition may reduce the solubility of CHX which will result in a higher concentration of CHX in the coating [32]. These results are in accordance with the major antibacterial activity observed by PRP40_2CHX condition, which is 13% greater against *S.aureus* and 47% for *E.coli* (Fig. 11).

Cumulative release of CHX from the coated specimens was studied (Fig. 12). PP60_2CHX presented a burst release of CHX and showed the fastest release for the first 48h, during which $61\pm 7\%$ of the drug loaded was released. The stationary state was reached after 7 days. The drug released by PRP40_2CHX also presented a burst release for the first 8h, although less pronounced than for PP60_2CHX. At this time point, the amount of CHX released was $28\pm 4\%$. After 3-4 days, the PP60_2CHX profile presented a less pronounced increase compared with PRP40_2CHX. These drug delivery systems provided a CHX sustained release compared with antibiotic loaded by conventional dipping method, since in the last case more than 80-90% of the antibiotics are released from calcium phosphate coatings within the first hour [56].

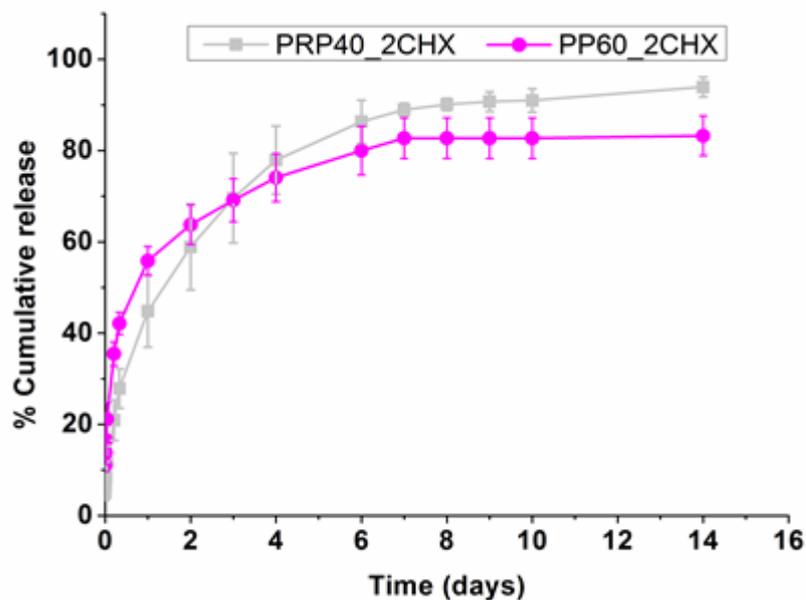


Fig. 12: Release of CHX from PRP40_2CHX (reversed pulses at 40°C and 2mA/cm²) and PP60_2CHX (pulses at 60°C and 2mA/cm²).

To characterize the release mechanism, the amount of drug released from each coating group was fitted with the different model equations (Table 3). Resulting squared multiple correlation coefficient R^2 showed that all studied models provided a better goodness of fit for PRP40_2CHX condition. For KP model, the value of n lower than 0.5, especially for PP60_2CHX showed that pseudo-Fickian diffusional mechanism controlled the release of drug from coating [57].

Considering the dissolution of the coating observed by SEM at the end of the release studies (Fig 13b), it was necessary to deepen the investigations and understanding of the mechanisms of drug release using other models as those proposed by Higuchi and Kopcha.

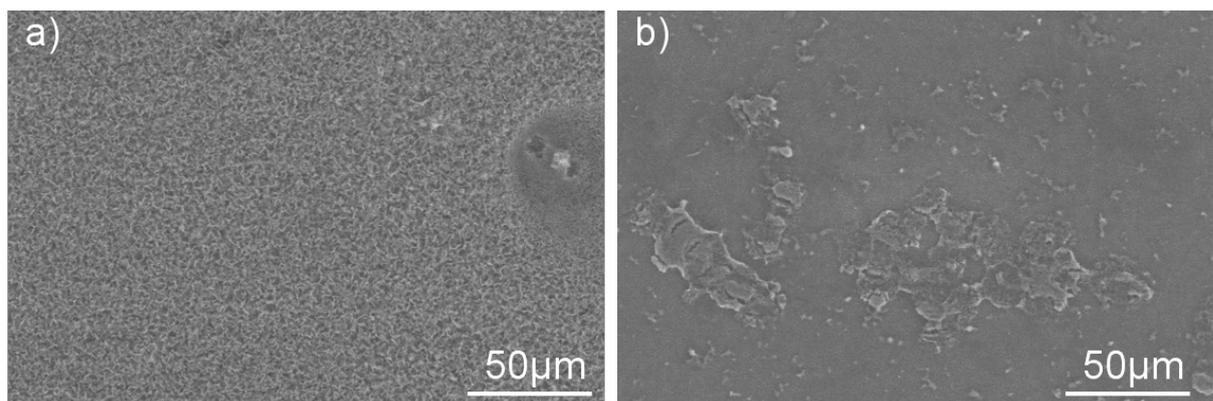


Fig. 13: SEM micrographs of PRP40_CHX coating a) before and b) after 15 days of release test in TRIS buffer.

The A/B ratio obtained in the Kopcha model showed that if erosion phenomena exist, it is the diffusion mechanisms that prevail and lead to the release of chlorhexidine [58]. This information is confirmed by the results obtained with the Higuchi model. This model also showed that by ignoring the first hour of release (burst effect), the coefficient of Higuchi is higher for PRP40_2CHX than for PP60_2CHX showing a faster release for PRP40_2CHX.

Table 3: Parameters obtained from Korsmeyer-Peppas, Higuchi and Kopcha modelling of PRP40_2CHX and PP60_2CHX release curves.

	Korsmeyer-Peppas model		Higuchi model		Kopcha model	
	n	R ²	a	R ²	A/B	R ²
PRP40_2CHX	0.422	0.998	0.074	0.996	>>1	0.997
PP60_2CHX	0.250	0.991	0.056	0.949	>>1	0.951

Despite the differences in the release kinetic profiles of PRP40_2CHX and PP60_2CHX, the statistical factors f_1 and f_2 , showed that the two kinetic profiles are statistically similar since $f_1 < 15$ and $f_2 > 50$ (Table 4).

Table 4: Factors of difference and similarity of PRP40_2CHX and PP60_2CHX conditions.

	PRP40_2CHX/PP60_2CHX	Specifications
f_1	14.5	0-15
f_2	53	50-100

4. Conclusions

In this work, adherent calcium phosphate coatings loaded with CHX have been obtained by a one-step electrodeposition process on titanium substrates. The presence of DCPD and OCP was confirmed by XRD and Raman analyses. In addition, the presence of different phases in the coating can allow tuning its stability and resorption properties. Moreover, the amount of loaded-CHX can be modulated by adjusting the coating conditions without altering the release kinetics. Although erosion of the coating was observed after 14 days in a buffered solution, CHX is predominantly released by diffusion mechanism. This study also showed that CHX co-deposited with CaP did not alter the antimicrobial agent since both coatings exhibited a noteworthy *in vitro* antibacterial activity against *S.aureus* and *E.coli*.

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