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# Light coupling into the Whispering Gallery Modes of a fiber array thin film solar cell for fixed partial Sun tracking

SUBJECT AREAS:  
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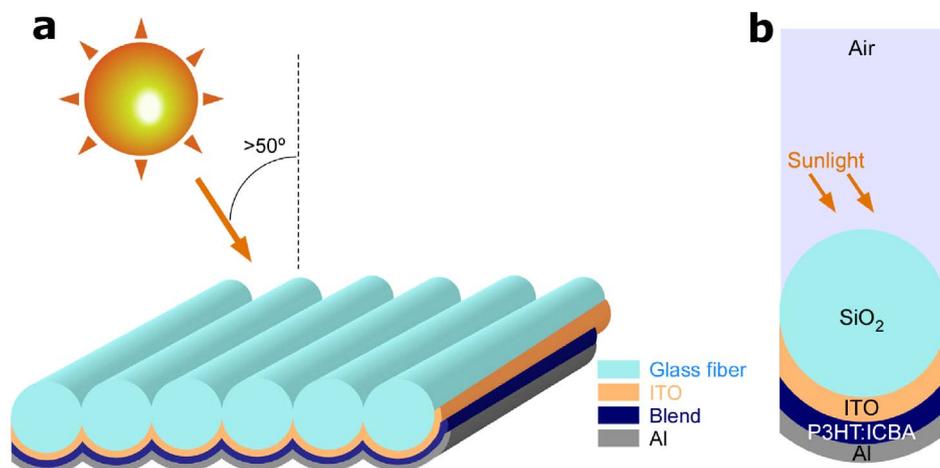
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We propose the use of whispering gallery mode coupling in a novel configuration based on implementing a thin film cell on the backside of an array of parallel fibers. We performed numerical calculations using the parameters of a thin film organic cell which demonstrate that light coupling becomes more effective as the angle for the incident light relative to the fiber array normal increases up to an optimal angle close to 55 deg. At this angle the power conversion efficiency of the fiber array solar cell we propose becomes 30% times larger than the one from an equivalent planar cell configuration. We demonstrate that the micro fiber array solar cell we propose may perform an effective partial tracking of the sun movement for over 100 degrees without any mechanical help. In addition, in the event that such fiber array cell would be installed with the adequate orientation on a vertical façade, an optimal photon-to-charge conversion would be reached for sunlight incident at 55 deg with respect to the horizon line, very close to the yearly average position for the sun at Latitude of 40 deg.

In thin film devices that use light as the energy source, it is of the utmost importance to implement an adequate material or structure configuration to obtain an optimal light absorption. In organic solar cells where the thickness of the active material is, typically, about one hundred nanometers, several approaches have been implemented, recently, to increase the effective light path<sup>1–4</sup>. Using the light scattered by plasmonic nanoparticles to achieve a 20% enhancement in the light absorption, single junction organic cells with a power conversion efficiency above 8% were demonstrated<sup>5</sup>. A disordered multilayer architecture with similar properties to one-dimensional photonic crystals has been used to enhance near infrared and near UV light absorption in semi-transparent organic cells which exhibited a power conversion efficiency above 5%<sup>6</sup>. Structured substrates forming an array of micropillars<sup>7</sup> or a curved surface such as the one obtained when spheres are laid over a planar device have also been considered to enhance light harvesting. A configuration where spheres stood in the proximity to a high-index photovoltaic absorber layer from a thin film cell was proposed to couple light into such high-index material and to obtain an enhanced light absorption. The authors claimed that the more effective coupling originated from whispering gallery modes (WGM) inside the spheres<sup>8</sup>. An alternative approach to improve absorption considered forming whispering-gallery resonant modes inside a low quality-factor spherical nanoshell structure that facilitated the coupling of light into the resonant modes and substantially enhanced the light path in the active material<sup>9</sup>. Coupling into high quality factor WGM has been extensively considered and has produced very encouraging results for the generation of laser light<sup>10–14</sup>, nonlinear light<sup>15–21</sup> or sensing<sup>22–26</sup>.

In the current work, we propose the use of WG coupling but in a drastically different configuration based on implementing an organic cell on the back side of an array of parallel fused silica fibers. In such an array, light can be coupled into low quality factor WG resonant modes of the fibers. Such coupling becomes more effective as the angle for the incident light relative to the normal of the fiber array increases up to 55 deg. In any case, as we will show below, light absorption at the active layer is at all angles larger for the fiber array configuration when compared to the standard planar configuration. In addition, the specific angular dependence of the light absorption in the configuration under study may provide an optimal solution to mimic sun-tracking systems or to enhance light harvesting for vertical PV installations.

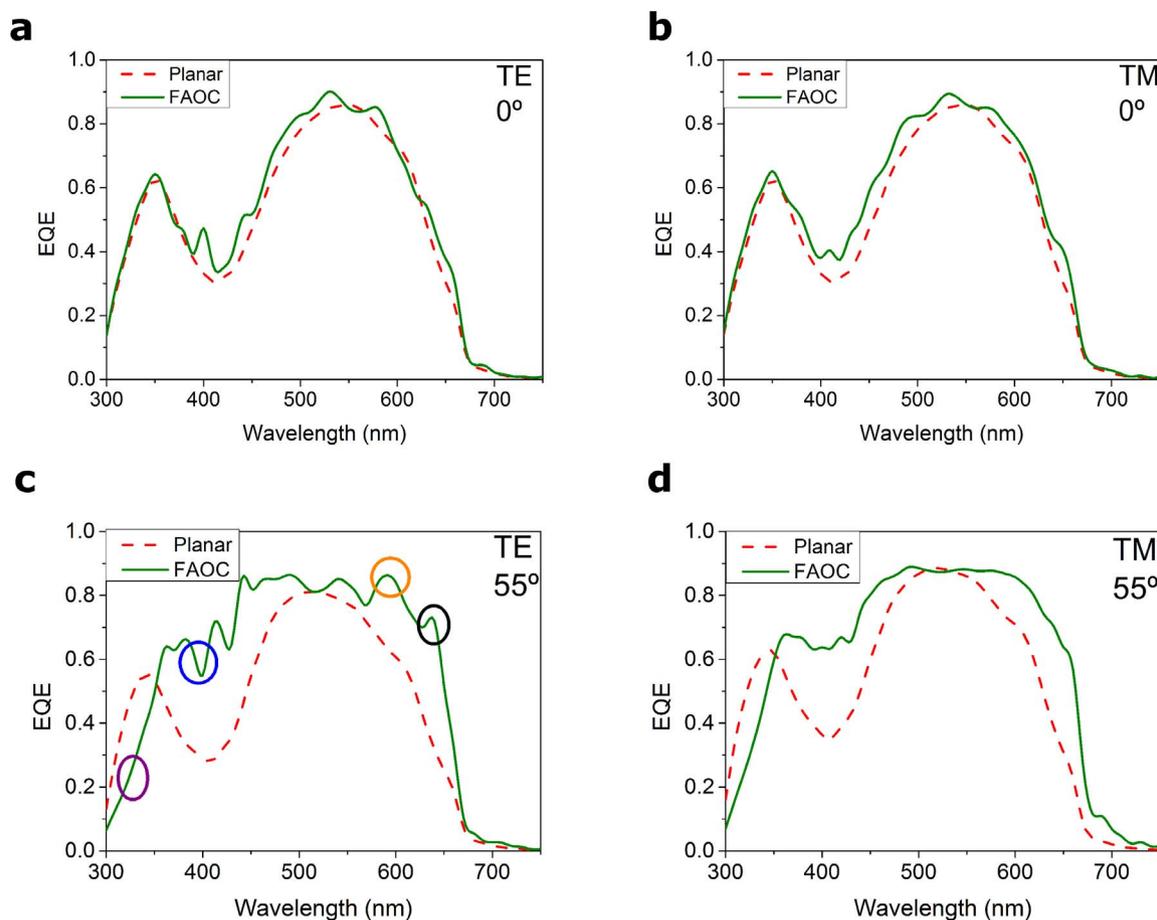


**Figure 1 | Schematic view of the FAOC.** a) The fiber array is the substrate where the solar cell device is deposited. The performance of the solar device is studied as a function of the angle of incidence ( $\theta$ ) of the Sunlight relative to the normal to the fiber array. b) Enlarged view of the cross section of one silica fiber from the array shown in a).

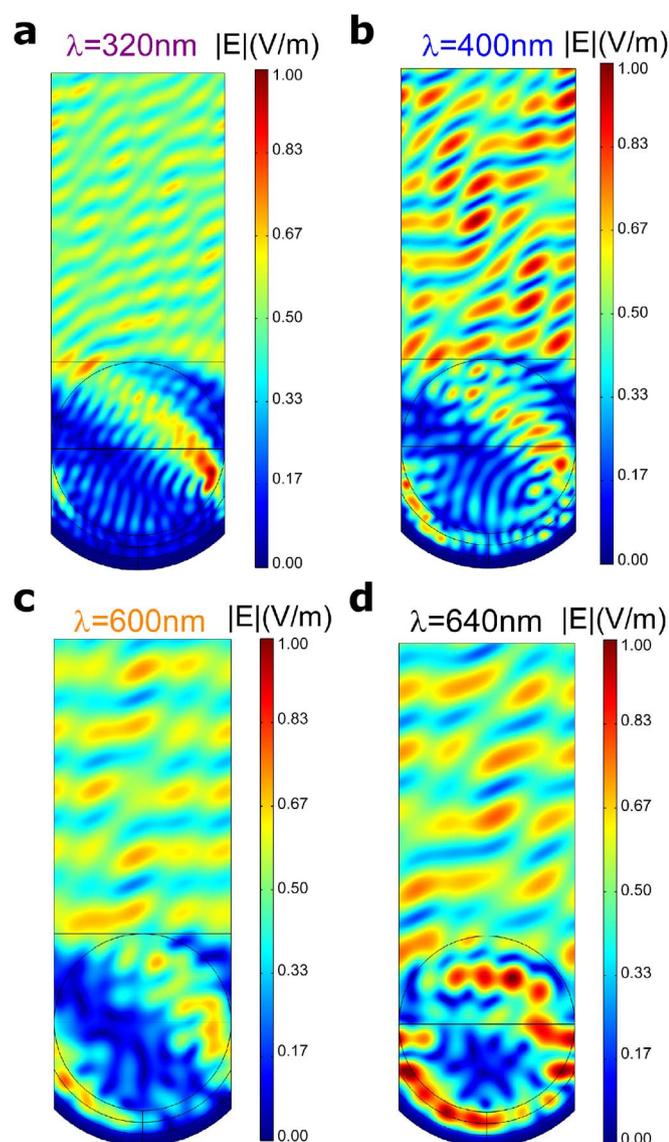
## Results

A schematic view of the solar cell device considered in here can be seen in Figure 1a. The device may consist of a number of fibers stuck together forming an array of parallel fibers that serve as the substrate for an organic solar cell device. The different layers of the cell architecture are deposited on the back side of the array relative to the

incoming sunlight incident on the front side of the array. A detailed cross section of a single cell fiber from the array is shown in Figure 1b. For the numerical study we present below, we consider silica as the substrate material. The back side of this substrate is coated with a three layer organic cell composed of a layer of Indium Tin Oxide (ITO) as transparent electrode, an active layer made of a



**Figure 2 | External quantum efficiencies of a 1.5  $\mu\text{m}$  diameter fiber FAOC (solid green) and an equivalent planar cell (dashed red).** The simulated EQEs are shown at normal incidence (0 deg) for a) TE and b) TM polarizations and at 55 deg for c) TE and d) TM polarizations. Note that at 55 deg incidence the increase in EQE for the fiber array relative to the planar cell is apparent at almost all wavelengths. The TE field intensity distributions at 320 nm (violet circle), 400 nm (blue circle), 600 nm (orange circle), and 640 nm (black circle) are shown in Figure 3.



**Figure 3** | Cross section of the spatial distribution TE field norm. Fiber diameter of the FAOC is 1.5  $\mu\text{m}$  and light is incident at 55 deg, and the wavelength tuned at a) 320 nm, b) 400 nm, c) 600 nm and d) 640 nm. All figures are normalized to 1 V/m and the same color coding is used for all of them.

Poly(3-hexylthiophene-2,5-diyl) blended with Indene-C60 Bisadduct (P3HT:ICBA), which extinction coefficient is shown in Figure SI2b, and an Aluminum (Al) metallic contact. Extremely thin layers that must be included in an experimental realization of the majority of organic cells, as noted in the supplementary information file, were omitted in our numerical calculations given their negligible effect in the re-distribution of the optical field intensity.

The convolution of the P3HT:ICBA extinction coefficient with the sun photon flux leaves a wavelength window for PV operation ranging from 300 nm to 750 nm. At each wavelength, the total power dissipation over the active layer area is integrated to extract the photon absorption in this layer or, equivalently, the External Quantum Efficiency (EQE). Provided that the scope of the work is to compare the performance of such fiber array organic cell (FAOC) relative to the planar configuration, the wavelength independent factor to account for losses in the collection of charges relative to the absorbed photons, is taken to be equal to unity. To validate the reliability of the numerical model used, the experimentally measured EQE from a fabricated planar cell is compared to the numerically

calculated one in figures SI1 from the supplementary information file. The predicted EQEs at normal incidence (0 deg) for the FAOC and planar cells at, both, TE and TM polarizations are shown in Figure 2a and 2b, respectively. Although the performance of the FAOC is slightly better than the planar one, no significantly different features are observed when comparing both EQEs. This is not the case, when the light is incident at 55 deg. In that event, the EQE for the FAOC, shown for the TE and TM polarizations in Figures 2c and 2d, respectively, is largely improved at almost the entire wavelength range. In the wavelength range spanning from 430 to 600 nm, the EQE is almost saturated to its maximum possible value. The EQE of the planar cell at 400 nm and surrounding wavelengths exhibits very low values reaching a local minimum of 0.25 for the TE polarization and 0.35 for the TM polarization due to the combined effect of a destructive interference and a local minimum of the P3HT:ICBA extinction coefficient (cf. Figure SI2b). On the contrary, in the same wavelength region the EQE for the FAOC is always higher than 0.5 for both polarizations.

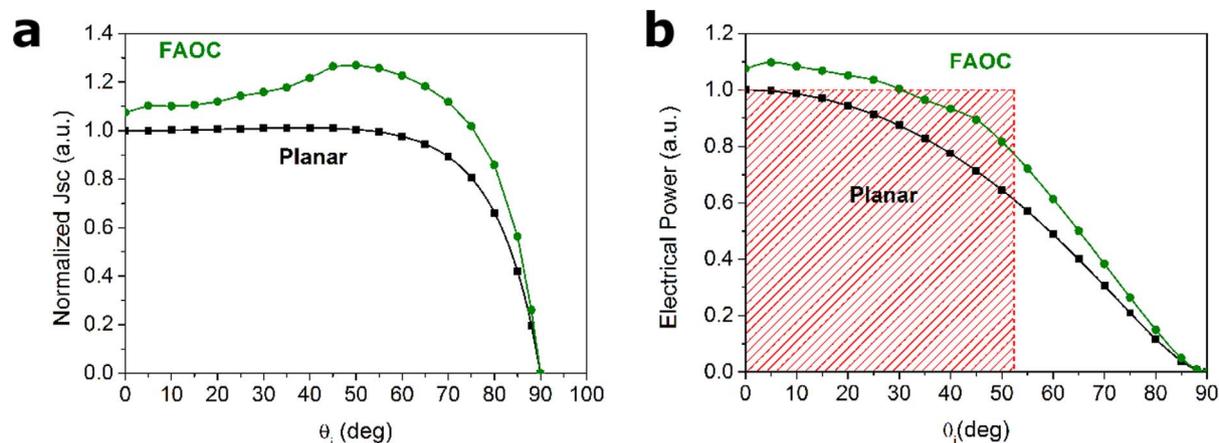
To better understand what causes the increase in EQE at 55 deg incidence, we numerically computed the spatial electric field norm distribution at 320, 400, 600 and 640 nm, shown in Figure 3 for the TE polarization. Such field distribution seems to indicate that for the last three cases photon trapping in the active layer occurs all along the half coated fiber perimeter. Incidence at 55 deg induces a partial excitation of a WGM, which leads to light trapping at the inner boundary of the spherical interface separating the transparent electrode and blend from the metal electrode. The excitation of WGMs is particularly apparent at 640 nm when the extinction coefficient is small. The TE field distribution, shown in Figure 3d, exhibits high intensity lobes in a large part of the half perimeter of the cylinder occupied by the ITO electrode and active layer. Therefore, we may attribute the 2.3 times enhancement observed in the EQE to an increased absorption path for the light within the active layer. At 320 nm coupling to the WGM is aborted by the higher extinction coefficient of ITO at that wavelength. Consequently, as seen in Figure 2, no gain in the EQE can be obtained at that wavelength region where absorption is dominated by the ITO extinction coefficient. We have also considered the case where the fiber array is finite and limited to a total number of five fibers surrounded by air. In that case the field distribution obtained was computed and, as shown in Figure SI4 in the supplementary information file, similar field distribution lobes as the ones from Figure 3 were observed. In accordance, the EQE of such finite FAOC is similar to the one from the periodic FAOC, as shown in Figure SI5 from the supplementary information file. These results confirm the validity of the periodic boundary conditions applied to model light harvesting in the FAOCs.

To estimate the short circuit current of the FAOC and compare it to the one from the standard planar, we computed the short circuit current ( $J_{sc}$ ) obtained at each angle of incidence, shown in Figure 4a. This current was calculated integrating the EQE multiplied by the solar photon flux and the electron charge  $q$  over all wavelengths  $\lambda$ , as in the equation

$$J_{sc} = \int EQE(\lambda) \frac{I(\lambda)\lambda}{hc} q d\lambda \quad (1)$$

where  $I(\lambda)$  indicates the standard AM1.5G spectral irradiance of the Sun. At normal incidence, the  $J_{sc}$  for the FAOC is 6% higher than the planar cell. When the angle of incidence increases the planar cell's  $J_{sc}$  stays almost constant up to 40 deg, whereas for the FAOC one increases with angle as the light gets coupled more effectively into the WGM. The  $J_{sc}$  exhibits a maximum at 55 deg being 30% larger than the planar. At higher angles, as expected, the  $J_{sc}$  for, both, FAOC and planar cells decays rapidly but the one for the FAOC remains always larger.

As the angle of incidence increases, the electrical power generated for both cells would decrease by a  $\cos(\theta)$  factor accounting for the



**Figure 4** | Normalized electrical response of FAOC compared to a planar cell. a) Normalized  $J_{sc}$  for the planar cell (black squares) and for a 1.5  $\mu\text{m}$  fiber diameter FAOC (green dots) as a function of the sunlight angle of incidence. b) Electrical power in arbitrary units as a function of the incidence angle provided by the planar device (black squares) and by the 1.5  $\mu\text{m}$  fiber diameter FAOC (green dots). The area of the red rectangle would be proportional to the energy collected by a planar cell tracking the movement of the sun up to 52 deg. Up to this angle the area under the FAOC curve is the same. Currents and powers are normalized to the response of the planar device at 0 deg. The black and green lines are only a guide for the eye.

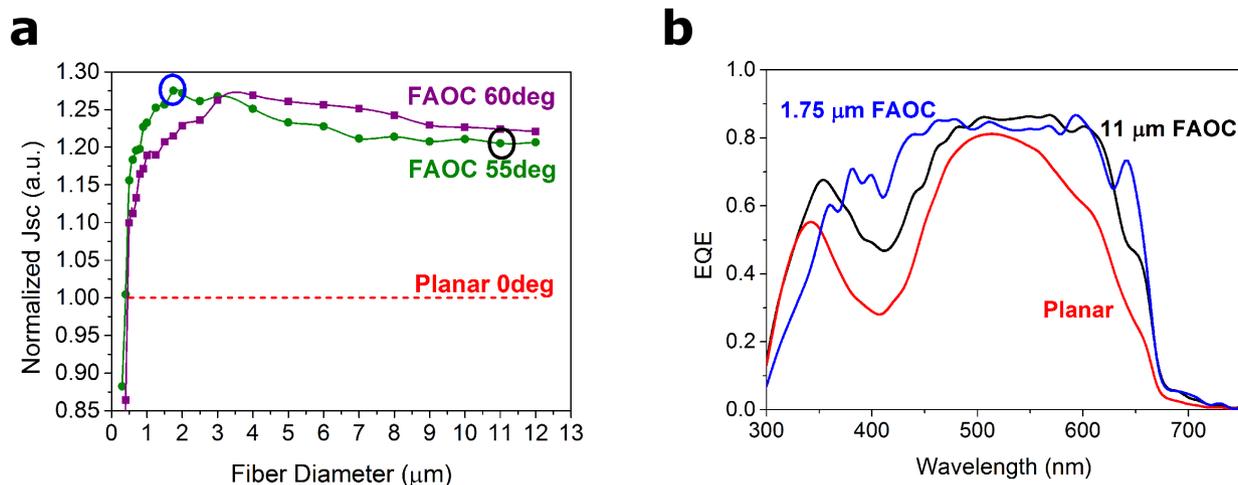
projected area to a surface normal to the direction of the incident light. As shown in Figure 4b, this reduction in electrical power can be partially compensated by the FAOC due to a photocurrent generation that is maximized at 55 deg rather than at normal incidence. For a solar cell placed in a horizontal plane, energy collected from sunrise to sunset would be proportional to two times the area underneath the curves shown in Figure 4b. This area is 17% times larger for the FAOC than for the planar case. As shown in Figure 4b too, the energy collected by the FAOC from 0 to 52 deg would be equivalent to the energy collected by a planar cell maintained, at all times, perpendicular to the sun in that angular range.

At an incidence of 55 deg we studied the  $J_{sc}$  dependence with the fiber diameter, keeping the other geometrical parameters fixed. At diameters below 400 nm, when light confinement at the perimeter of the fiber close to the back metal contact is ineffective, the  $J_{sc}$  for the FAOC is not better than for the planar configuration. As seen in Figure 5a, this situation is reversed as the diameter is increased, and the  $J_{sc}$  reaches a maximum at a fiber diameter of 1.75  $\mu\text{m}$ . At such fiber dimensions the EQE, shown in Figure 5b, is very close to the optimal for a large wavelength interval spanning from 375 to

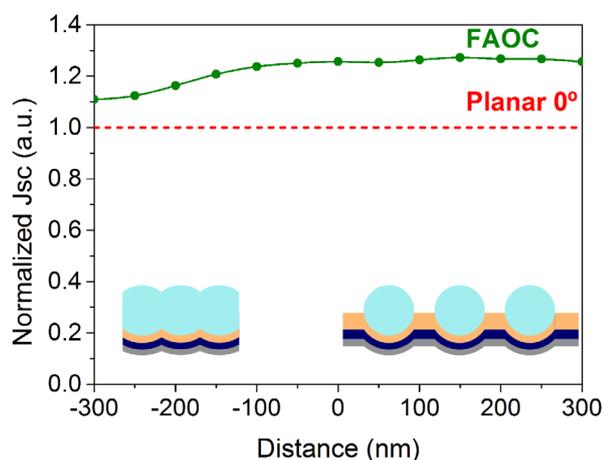
650 nm. This indicates an optimal coupling to the WGM for such entire wavelength range. As the fiber diameter is increased further, the  $J_{sc}$  decreases while the EQE for the FAOC resembles more the one for the planar cell, as shown in Figure 5b. This indicates a less effective coupling to the WGM at certain wavelengths when the fiber diameter increases. When the incidence angle is set at 60 deg we observe that the maximum  $J_{sc}$ , shown in Figure 5a, shifts slightly towards larger fiber diameters. However, the general trend is very similar to the one seen when the angle is set to 55 deg. Finally, we considered the performance for the FAOC as the separation between adjacent fibers was varied. The  $J_{sc}$  shown in Figure 6, varies little as the fiber separation is increased up to 300 nm, while it shows a mildly pronounced drop as adjacent fibers get closer to progressively overlap and eventually causing the final FAOC configuration to resemble a planar device. Such drop in  $J_{sc}$  occurs mostly in between  $-100$  and  $-200$  nm.

## Discussion

We have demonstrated that an array of fibers can be used as a substrate material to significantly improve light harvesting capacity for



**Figure 5** | Maximum response of the FAOC as function of fiber diameters. a) Normalized  $J_{sc}$  at and incidence of 55 deg (circular dots) and 60 deg (square dots) for different fiber diameters of the FAOC. Normalized  $J_{sc}$  for the planar cell (red dashed line). The green and purple lines are only a guide for the eye. The normalization is to the planar cell at 0 deg incidence. b) EQE at an incidence of 55 deg for the FAOC when the fiber diameter is 1.75  $\mu\text{m}$  (blue), when the fiber diameter is 11  $\mu\text{m}$  (black), and for the planar cell (red).



**Figure 6 | Electrical response as a function of fiber separation.**

Normalized  $J_{sc}$  at 55 deg incidence for a 1.5  $\mu\text{m}$  fiber diameter FAOC (green dots) when the separation between two adjacent fibers is varied. A negative separation corresponds to a fiber overlap (left inset), and a positive separation is for the case when adjacent fibers are connected by a planar cell (right inset). The green line is only a guide for the eye.

organic solar cells when compared to the standard planar device configuration. The incident light is coupled to some low-Q whispering gallery modes of the fibers. Such coupling is effective for a broad range of wavelengths as required when converting light into electricity from a wideband source like the sun. Our numerical study shows that the number of absorbed photons per unit area increases as the sun inclination relative to the cell normal increases from 0 to 55 deg. At a Latitude close to 40 deg if one tilts the PV plane by 35 deg relative to the surface of the Earth, the Sunlight will be incident on the PV at approximately 90 deg with respect to the PV plane or, in other words, the Sun would be 55 deg above the horizon line<sup>27</sup>. This is why at 40 deg latitude the slope of a fixed PV installation on a rooftop or solar filed is, typically, 35 deg. On the other hand, the plane of any kind of standard vertical PV installation integrated on a building façade would be 55 deg of such optimal orientation. However, for the FAOC we propose a maximum efficiency would be obtained at 55 deg, ensuring an optimal light harvesting for vertical installations. On the other hand, for mechanically fixed photovoltaic (PV) installations the lack of sun tracking leads to a rather inefficient energy harvesting. Indeed, at a Latitude of 40 deg up to 38% more energy could be harvested by maintaining the plane of the PV installation perpendicular to the sun at all times. In the event that the longitudinal axis of the FAOC would be oriented in the meridian direction, the angular increase in power conversion efficiency would provide, over the course of one day, an energy harvesting capacity 17% times larger, equivalent to a “half” tracking of the Sun movement. In a future fabrication of the FAOC practical issues such as uniformity, fiber surface roughness, or an increase in the ITO series resistance due to a larger contact area for the FAOC should be taken into account. For instance, to minimize such potential increase in the series resistance of the ITO, a transversal strip of a metal contact across the fibers should be deposited on one end of the FAOC.

## Methods

To study the performance of such FAOC we carried out numerical simulations using the finite element method numerical technique implemented in the commercial software COMSOL Multiphysics®. The electromagnetic wave equations were solved in the two-dimensional area corresponding to the transversal section of a single organic cell fiber, shown in Figure 1b. We assumed the fibers to be made of fused silica and in the numerical modeling the optical parameters for such material were used. The diameter of the fiber was set to 1.5  $\mu\text{m}$ , except for the cases in which is stated otherwise, while the thicknesses of ITO, P3HT:ICBA, and Al were set each of them to 100 nm, corresponding to the approximate parameters for an optimized performance for the equivalent planar cell<sup>28</sup>. The refractive indices of all materials were taken from

our experimental measurements except for the fused silica which was taken from the literature. We imposed periodic conditions (Floquet periodicity) on both lateral sides of the single device to simulate the effect of the array. Such periodic boundary conditions are well justified provided the largest fiber diameter considered in this work is 40 times smaller than the transversal coherence of visible sunlight<sup>29</sup>. Multiple absorbing ports were defined in the upper air boundary for each possible diffraction angle of the periodic structure. This avoided non-physical reflections at the upper boundary coming back to the system fiber plus cell. For the same reason, we kept at least one wavelength distance from the upper boundary to the silica fiber in order to avoid near fields that may not be absorbed by the ports. In-plane (TM) and out-of-plane (TE) polarizations were simulated separately with a power excitation corresponding to one sun. A perfect electric conductor boundary condition was imposed to the lower boundary although its effect is negligible since light is very effectively reflected by the 100 nm back metal contact. For comparison, a planar OPV was also simulated and the same boundary conditions were applied. In the latter case, light was incident from a fused silica glass substrate and the power of the incident wave was corrected by the corresponding Fresnel coefficient for the air-glass refraction.

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## Author contributions

M.M. and F.J.R. designed the experiment. M.M. carried out the numerical simulations and drew all the figures. P.R.G. and G.K. assisted in data analysis. J.M. and M.M. wrote the manuscript and all authors discussed the results and reviewed the manuscript.

## Additional information

**Supplementary information** accompanies this paper at <http://www.nature.com/scientificreports>

**Competing financial interests:** The authors declare no competing financial interests.

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